

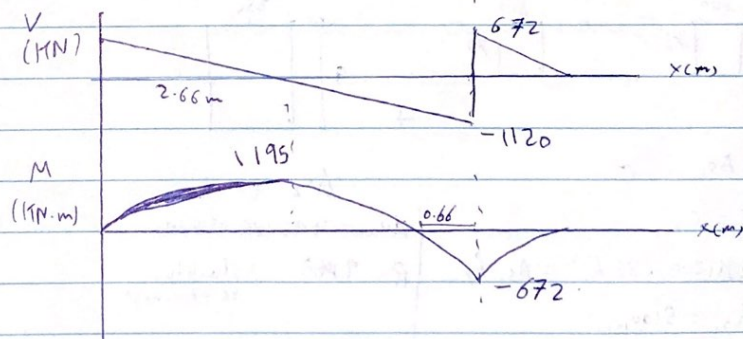
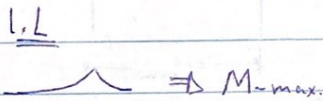
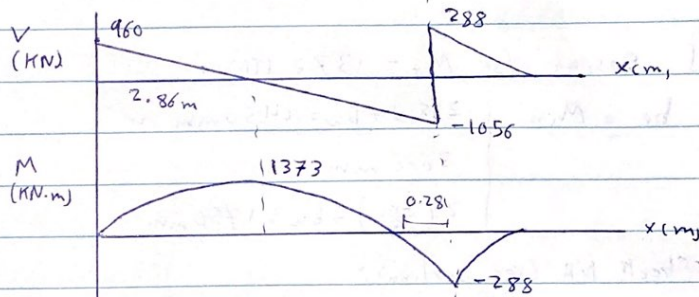
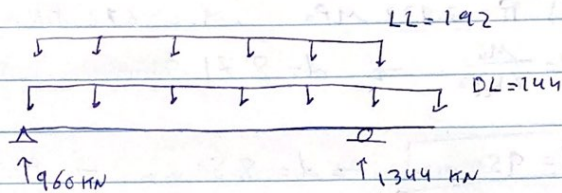
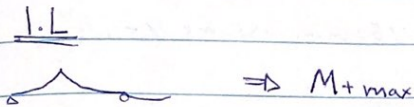
Homework assignment #4

ENCE 335

Mohamad Moayad Shannak

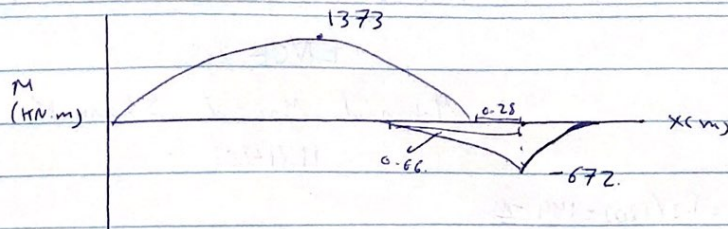
- 1181401 -

-B1: $\left\{ \begin{array}{l} DL = 1.2(120) = 144 \frac{kN}{m} \\ LL = 1.6(120) = 192 \frac{kN}{m} \end{array} \right.$



- Envelope:

B.M.



[2] [A.4] $\rho_{max} = 0.0206$

Take $\rho = 0.5 \rho_{max} = 0.0103$

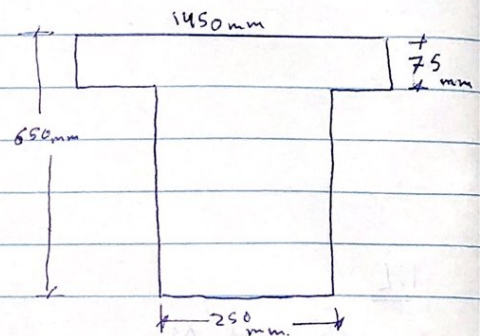
[A.5] $R = 2.932 \text{ MPa}$, $M_u = -672 \text{ kN.m}$, $b = 250 \text{ mm}$. assume $\phi = 0.9$.

$R = \frac{M_u}{\phi b d^2} \Rightarrow d = 871.5 \text{ mm}$.

[H = 950 mm] $\rightarrow d = 880 \text{ mm} \rightarrow R = 3.857 \text{ MPa} \rightarrow \rho < \rho_{0.005}$
 $\therefore \phi = 0.9$.

[3] Design for $M_u = 1373 \text{ kN.m}$

$b_e = \text{Min} \left\{ \begin{array}{l} 2(8h) + b_w = 1450 \text{ mm} \checkmark \\ 3000 \text{ mm} \\ 2\left(\frac{L_n}{8}\right) + b_w = 1750 \text{ mm} \end{array} \right.$



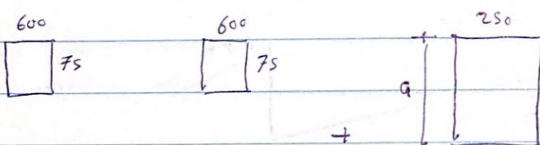
- Check NA (rec. section):

assume $\phi = 0.9$, 3 layers $\phi 43$, $d = 492.5 \text{ mm}$.

$R = \frac{M_u}{\phi b d^2} = 4.338 \text{ MPa} \rightarrow$ [A.5] $\rho = 0.0115$

$\rightarrow A_s = \rho b d = 8212 \text{ mm}^2 \rightarrow T = C \rightarrow a = \frac{f_y A_s}{0.85 f_c'} \rightarrow a = 100 \text{ mm} > 75 \text{ mm}$

\therefore T-section design



A_{s1}

A_{s2}

$T_1 = C_1$

$(75)(1200)(0.85 f_c') = A_{s1} f_y$

$A_{s1} = 5100 \text{ mm}^2$

$\phi M_{n1} = \phi A_{s1} f_y (d - \frac{75}{2})$

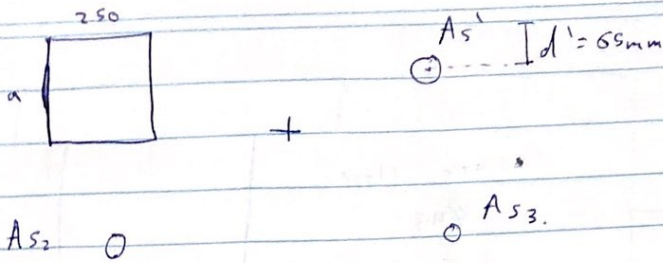
$\phi M_{n1} = 877.15 \text{ kN.m}$

$\phi M_{n2} = 1373 - \phi M_{n1}$

$= 495.85 \text{ kN.m}$

$\phi M_{n2} = 495.85 \text{ kN.m}$

$R = 9 \text{ MPa}$. \therefore doubly reinforcement.



Take $\rho = 0.018 \rightarrow \boxed{A_{s2} = 2216 \text{ mm}^2}$

[A.1] $R = 6.36 \text{ MPa}$, assume $\phi = 0.9$, $d' = 65 \text{ mm}$

$\rightarrow M_{n2} = R \phi b d^2 = 347 \text{ KN.m}$

$M_{n1} = 148.85 \text{ KN.m}$

$\rightarrow a = \frac{A_s f_y}{0.85 f_c' b} = 156 \text{ mm} \rightarrow \bar{y} = 184 \text{ mm} \rightarrow \epsilon_s = 0.00503 \rightarrow \epsilon_s' = 0.00194$ not yield
 $\rightarrow f_s' = 388 \text{ MPa}$

$M_{n1} = A_s' f_c' (d - d') \Rightarrow \boxed{A_s' = 897 \text{ mm}^2}$

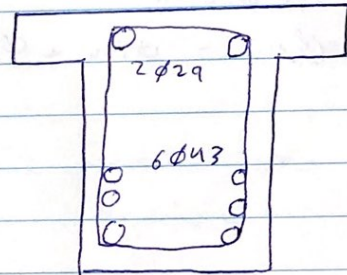
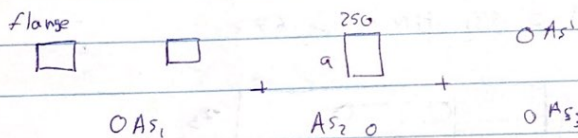
$T_2 = C_2 \Rightarrow A_s' f_s' = A_{s3} f_y \Rightarrow \boxed{A_{s3} = 829 \text{ mm}^2}$

[A.2] $A_s' = 897 \text{ mm}^2 \Rightarrow 2 \phi 29$, $\boxed{A_s' = 1290 \text{ mm}^2}$

$A_s = 5100 + 2216 + 829 = 8145 \text{ mm}^2$ [A.2] $6 \phi 43$, $A_s = 8712 \text{ mm}^2$
 3-layers

[A.7] 2 bars in each layer.

- Check moment Capacity:



$\phi M_{n1} = 877 \text{ KN.m}$, $A_s' = 1290 \text{ mm}^2 \rightarrow A_{s3} = 1192 \text{ mm}^2$
 $A_{s1} = 5100 \text{ mm}^2$, $a = 130.8 \text{ mm}$, $f_s' = 347 \text{ MPa}$

$T = C \Rightarrow A_s f_y = 2142000 + 0.85 f_c' a 250 + A_s' f_s'$

$f_s' = 347 \text{ MPa} \rightarrow a = 180 \text{ mm} \rightarrow \epsilon_s' = 0.0021$ Yield $\therefore f_s' = 420 \text{ MPa}$, $a = 164 \text{ mm} \rightarrow \epsilon_s' = 0.00199$

$\rightarrow f_s' = 398 \text{ MPa} \rightarrow a = 168 \text{ mm} \rightarrow \epsilon_s' = 0.002015 \rightarrow f_s' = 420 \text{ MPa}$ \therefore steel in Comp. side Yield.

$\bar{y} = 197 \text{ mm} \rightarrow \epsilon_s = 0.0045$ $\therefore \phi = 0.858$

$\phi M_n = \phi M_{n1} + \phi M_{n2} + \phi M_{n3}$

$= \phi A_{s1} f_y (d - \frac{7s}{2}) + \phi 0.85 f_c' a (250) (d - \frac{a}{2}) + \phi (A_s' f_y) (d - d')$

$= 1385.3 \text{ KN.m} > 1373 \text{ KN.m}$

- Design for $M_u = -672 \text{ kNm}$.

$$R = \frac{M}{\phi b d^2} = 10.4 \text{ MPa}$$

\therefore doubly.

Take $\rho = 0.6 \rho_{max}$

$$\rho = 0.01236 \rightarrow A_{s1} = 1655 \text{ mm}^2$$

assume 2 layer

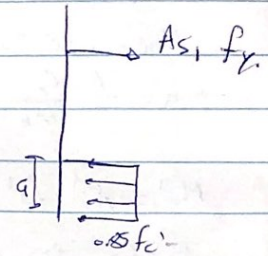
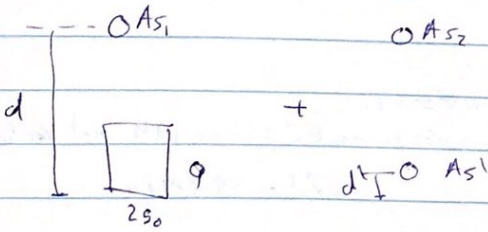
$\phi 43$

$$d = 650 - 50 - 43 - \frac{43}{2} = 535.5 \text{ mm}$$

$\phi = 0.9$

$b = 250 \text{ mm}$

$$d' = 64.5 \text{ mm}$$



$$\phi M_{u1} = \phi A_{s1} f_y (d - a/2)$$

$$a = \frac{A_{s1} f_y}{0.85 f_c'} = 117 \text{ mm} \rightarrow \epsilon_s > 0.005 \rightarrow \bar{y} = 137 \text{ mm} \rightarrow \epsilon_s' = 0.0015876 \rightarrow f_s' = 317 \text{ MPa}$$

$\therefore \phi = 0.9$

$$\phi M_{u1} = 298 \text{ kNm} \rightarrow \phi M_2 = 374 \text{ kNm} = \phi A_{s'} f_s' (d - d') \rightarrow A_{s'} = 2783 \text{ mm}^2$$

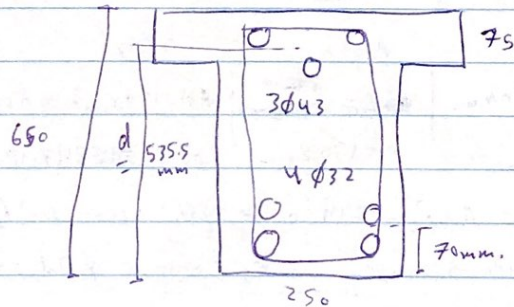
A.2 $A_s = 3756 \text{ mm}^2$, $A_{s'} = 2783 \text{ mm}^2$ $\rightarrow A_{s2} = 2100 \text{ mm}^2$

$3 \phi 43$ $A_s = 4356 \text{ mm}^2$, ~~$5 \phi 29$ $A_{s'} = 3275 \text{ mm}^2$~~

$\therefore \phi = 0.9$

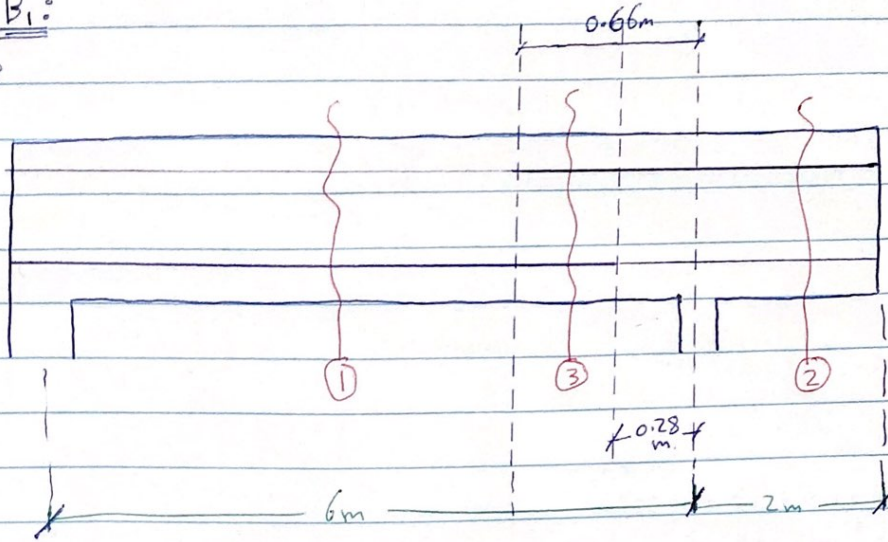
$4 \phi 32$, $A_{s'} = 3276 \text{ mm}^2$

$$\phi M_{u1} = \phi M_{u1} + \phi M_{u2} = 300 + 581 = 881 \text{ kNm} > 672$$



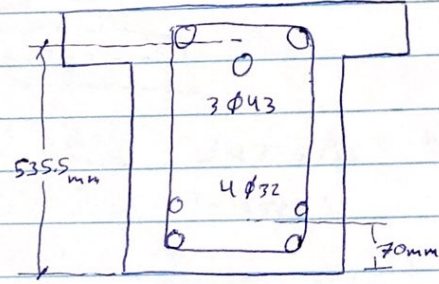
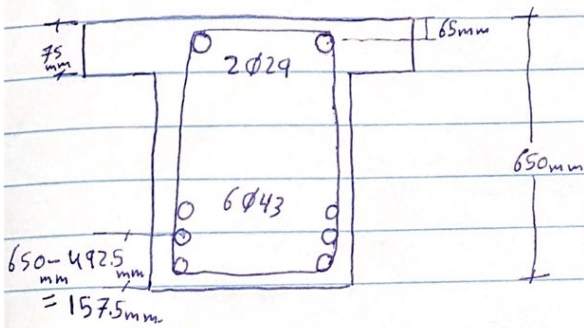
4- B_i:

Side-view:

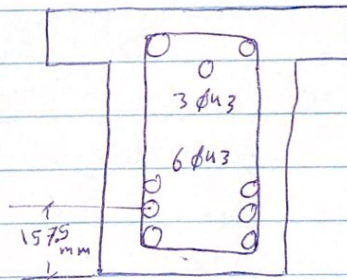


-Section 1°

-Section 2°



-Section 3°



Cover = 40mm

d_s = 10mm

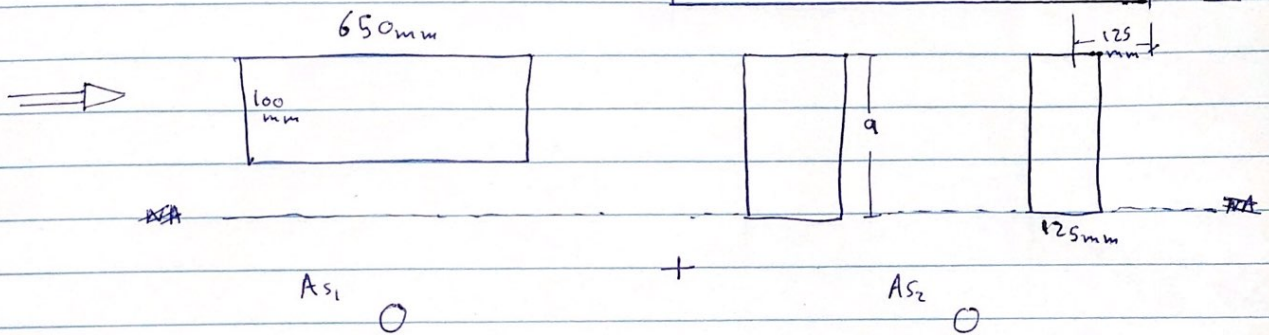
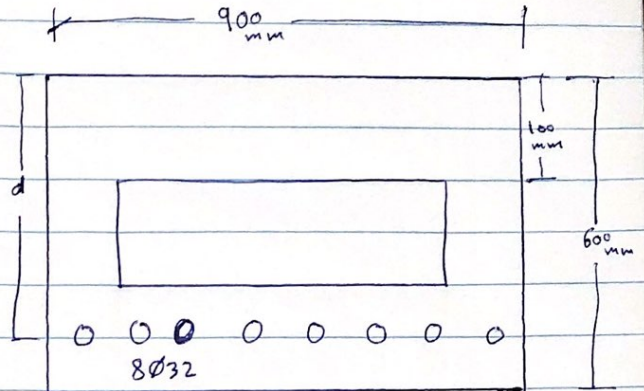
- Part 2°

$$f_c' = 28 \text{ MPa}$$

$$f_y = 420 \text{ MPa}$$

$$[A-2] A_s = 6552 \text{ mm}^2 \quad // \quad d = 534 \text{ mm}$$

$$\text{assume rect. section } a = \frac{A_s f_y}{0.85 f_c' b} = 128 \text{ mm}$$



$$T_1 = C_1 \Rightarrow A_{s1} f_y = 0.85 f_c' (650)(100)$$

$$\Rightarrow A_{s1} = 3683.33 \text{ mm}^2 \quad \Rightarrow A_{s2} = 2868.66 \text{ mm}^2$$

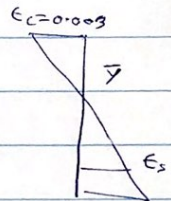
$$\phi M_n = \phi M_{n1} + \phi M_{n2}$$

$$\text{assume } \phi = 0.9 \quad // \quad \phi M_{n1} = \phi A_{s1} f_y (d - \frac{100}{2}) = 673.87 \text{ kN.m}$$

$$2 // \quad T_2 = C_2 \Rightarrow A_{s2} f_y = 0.85 f_c' (250)(a) \Rightarrow a = 202.5 \text{ mm} \quad \Rightarrow \bar{y} = 238.23 \text{ mm}$$

$$\text{assume } \phi = 0.9 \quad // \quad \phi M_{n2} = 469.255 \text{ kN.m}$$

$$\Rightarrow \epsilon_s = 0.0037246$$



Tension not controlled.

$$\phi M_n = 673.87 + 469.255 = 1143.125 \text{ kN.m}$$