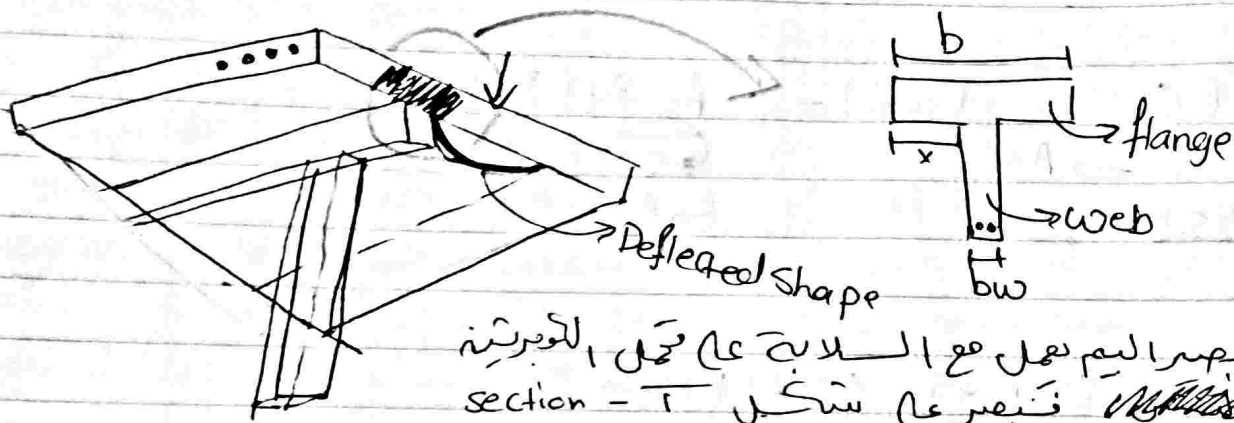


• What are T-section Beams:-

Beams + slabs  $\rightarrow$  Continuous  $\rightarrow$  monolithic construction

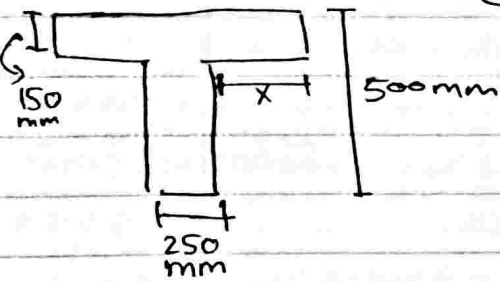


• بهر الیم عمل مع الالابه على قنل العبرینه  
 section - T

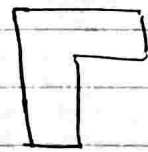
$\rightarrow$  ACI - code Table 6.3.2.1

• Example:  $l_n = 4m, s_w = 3m$

flange location		effective width (b)
Each side of web	least of	$8h$ $s_w/2$ $l_n/8$
one side of web	least of	$6h$ $s_w/2$ $l_n/12$



$$x = \begin{cases} 8h = 8 \times 150 = 1200 \text{ mm} \\ s_w/2 = 3/2 = 1500 \text{ mm} \\ l_n/8 = 4/8 = 500 \text{ mm} \checkmark \end{cases}$$



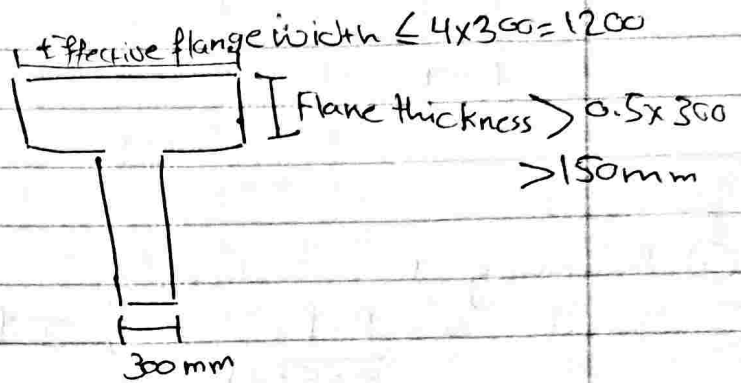
$\rightarrow b_e = 500 + 500 + 250 = 1250 \text{ mm}$

Section (T) أحياناً الكهنة يصمم على أساس (Compression area) كمنطقة ضغط.

• Condition :-

- Flange thickness  $\geq 0.5bw$
- Effective flange width  $\leq 4bw$

• Example :

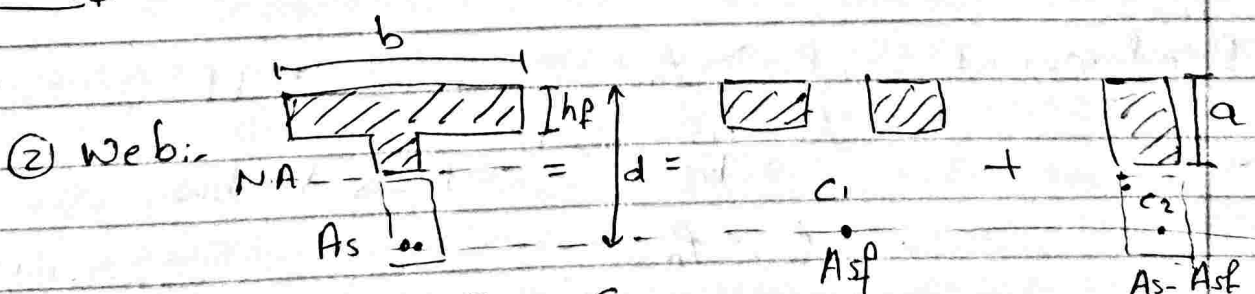
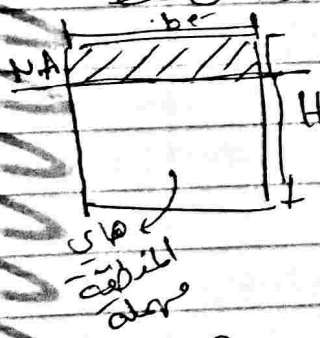


⇒ Analysis of T-sections :-

• N.A ⇒ تتغير موقعه، وعمقه، وموقعه على أبعاد أكثر، ومضائقه، كانه وكيفية السيل.

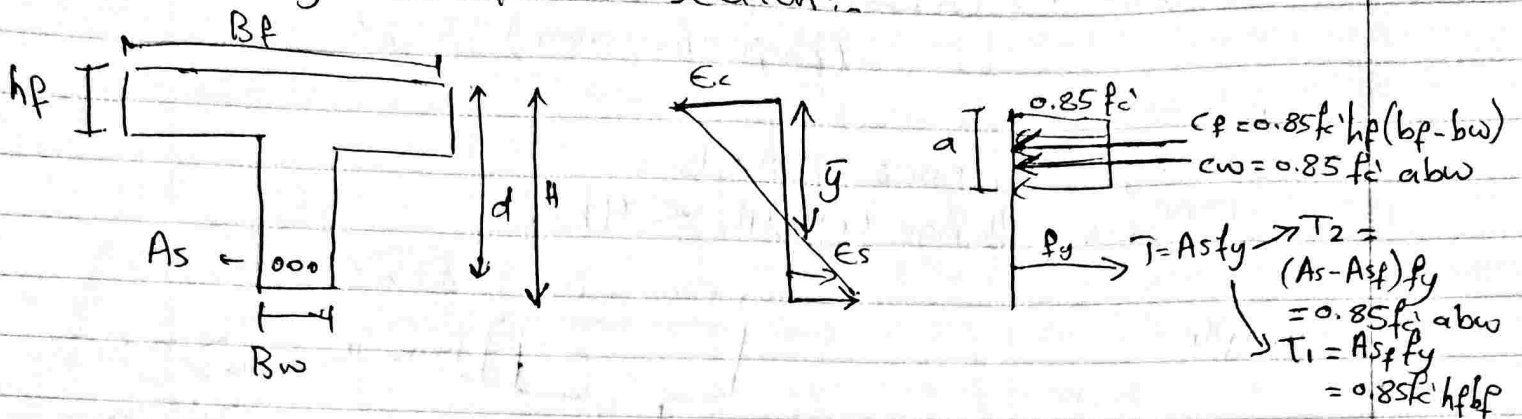
• If N.A lies in :-

① Flang :- نقتدر تغير المسكنه لأنه ربما يتغير الموقع الذي يتغير أنه ينتقل مسكناً، لياطون لمن يكون (T)، والانه الذي ينتقل السيل منها يتقبل (bw) فيتقبل عدد ليزر أكثر من السيل.



Total capacity =  $C_1 + C_2$

## \* Analysis of T-section:



① Assuming rect. section

② Check  $a = \frac{As f_y}{0.85 f_c' b}$ , If  $a \leq$ :

①  $a \leq h_f$

\* Analysis as rectangular section

\*  $T = c \Rightarrow As f_y = 0.85 f_c' a b_f$

\*  $\phi M_n = \phi As f_y (d - \frac{a}{2}) \Rightarrow$  Check width =  $B_w$

②  $a > h_f$

+ Analysis as T-section

①  $T_1 = c_f \Rightarrow As_f f_y = 0.85 f_c' h_f (b_f - b_w)$   
 $\Rightarrow \phi M_{nf} = \phi As_f f_y (d - \frac{h_f}{2})$

②  $T_2 = c_w \Rightarrow (As - As_f) f_y = 0.85 f_c' a b_w$   
 $\Rightarrow \phi M_{nw} = \phi (As - As_f) f_y (d - \frac{a}{2})$

③ Reinforcement  $\Rightarrow \rho_w > \rho_{min}$  rect  $\rightarrow b = b_f$

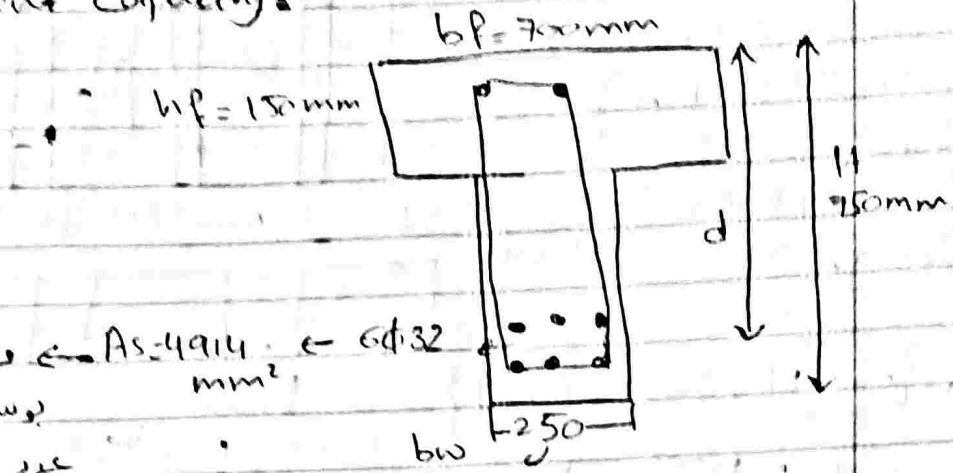
$\rho_w = \frac{As}{bd} \rightarrow b'$  T  $\rightarrow b = b_w$

$\Rightarrow \rho_w < \rho_{max}$

$\epsilon_s = \epsilon_u \frac{d - \bar{y}}{y} > 0.004$

إذا ما تكففت  
 سابتأ للديني  
 أو بتغير الأبعاد

• Example:  $f_y = 420 \text{ MPa}$ ,  $f'_c = 21 \text{ MPa}$   
 calculate the moment Capacity

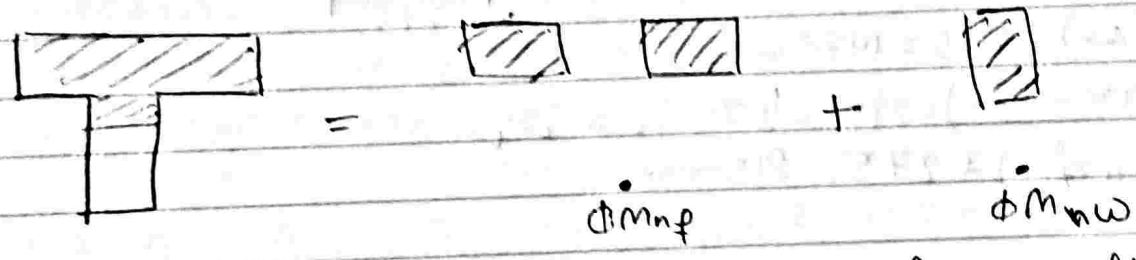


250 mm spacing between bars  
 3 bars in each layer  
 $A_s = 4914 \text{ mm}^2 = 6 \phi 32$

$$d = H - 40 - 10 - 32 - 32 - 32/2 = 620 \text{ mm}$$

• Assume rect:  $T = C \Rightarrow 0.85 f'_c a b = A_s f_y$   
 $a = 165.18 \text{ mm} > h_f$

• T-section design:



• For the flange:  $T_1 = C_f \Rightarrow A_{sf} f_y = 0.85 f'_c h_f (b_f - b_w)$   
 $A_{sf} \times 420 = 0.85 \times 21 \times 150 (700 - 250)$   
 $A_{sf} = 2869 \text{ mm}^2$   
 $A_{sw} = A_s - A_{sf} = 2045 \text{ mm}^2$

$\alpha_1$

$$\Rightarrow \phi M_{nf} = \phi A_{sf} f_y \left( d - \frac{h_f}{2} \right) = 591 \text{ kN.m}$$

• For the web:  $T_2 = C_w \Rightarrow A_{sw} f_y = 0.85 f'_c b_w a$   
 $a = 192.5 \text{ mm}$

$$\Rightarrow \phi M_{nw} = \phi A_{sw} f_y \left( d - \frac{a}{2} \right) = 404.9 \text{ kN.m}$$

• Check  $\phi \rightarrow \epsilon_s \Rightarrow \bar{y} = \frac{a}{\beta_1} \rightarrow \epsilon_s = 0.0052 > 0.005 \Rightarrow \phi = 0.9$

$$\phi M_n = \phi M_{nf} + \phi M_{nw} = 995.9 \text{ kN.m}$$

Example:  $l_n = 7.5\text{m}$

$S = 1.2\text{m}$

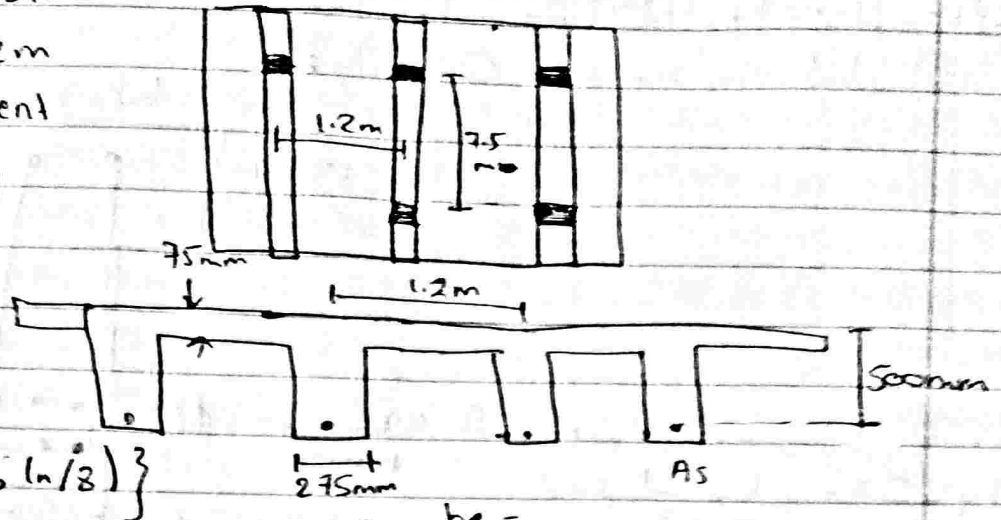
Web  $\rightarrow$  (-) moment

positive ( $M_u = 750\text{ kNm}$ )

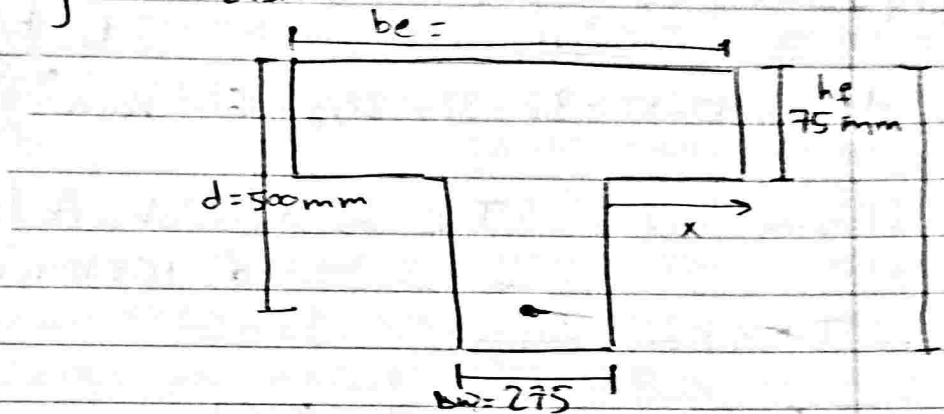
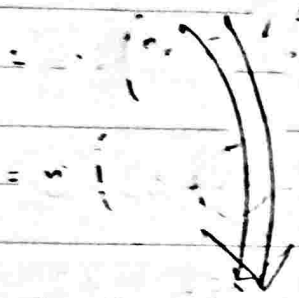
$f_y = 420\text{ MPa}$

$f_c = 21\text{ MPa}$

• Design?



$$X = \{ \min(8h, S_w/2, l_n/8) \}$$



$$b_e = \min \begin{cases} 2(600) + 275 = 1475\text{ mm} \\ 2\left(\frac{1200 - 275}{2}\right) + 275 = \boxed{1200}\text{ mm} \checkmark \checkmark \\ 2(437.5) + 275 = 2150\text{ mm} \end{cases}$$

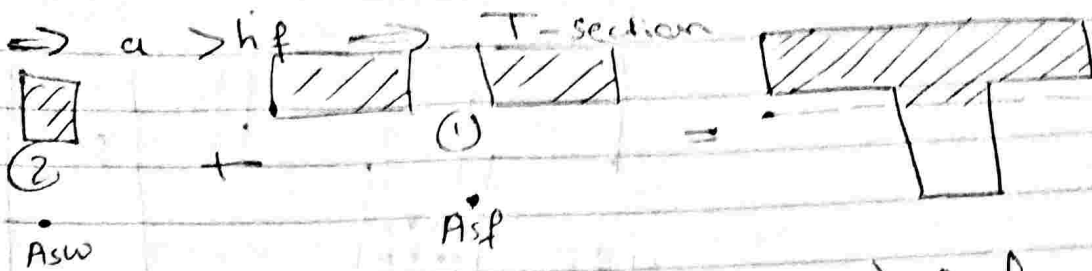
• Assume  $a < h_f \Rightarrow d = 500\text{ mm}, b = 1200\text{ mm}$

$$\Rightarrow R = \frac{M_u}{dbd^2} = \frac{750 \times 10^6}{0.9 \times 1200 \times 500^2} = 2.78\text{ MPa}$$

$\Rightarrow \rho = 0.00723 \rightarrow$  from table

$$\Rightarrow A_s = \rho b d = 4338\text{ mm}^2$$

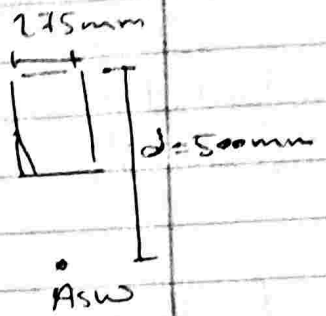
$$\Rightarrow \text{check } a = \frac{A_s f_y}{0.85 f_c b} \Rightarrow a = 85$$



①  $\phi m_n f \Rightarrow C_f = T_f \Rightarrow 0.85 f_c h_f (b_f - b_w) = A_s f_y$   
 $\Rightarrow A_s f = 2993 \text{ mm}^2$

$\phi m_n f = \phi A_s f_y (d - h_f/2) = 521.6 \text{ kN.m}$

②  $\phi m_n w = 750 - 521.6 = 228.4 \text{ kN.m} \rightarrow$



method (1) :-

$\phi m_n w = \phi A_s w f_y (d - \frac{a}{2})$

itr  
 (a)

Use :-  $a = \frac{A_s w f_y}{0.85 f_c b w}$  (unknown)

method (2) :-  $\Rightarrow \frac{R_u M_u}{\phi b d^2} = \frac{228.4 \times 10^6}{0.9 \times 275 \times 500^2} = 3.69$

$\Rightarrow$  Table  $p = 0.0099$ ,  $A_s = p b d = 1367 \text{ mm}^2$

$\Rightarrow A_s = A_s f + A_s w = 4315 \text{ mm}^2$

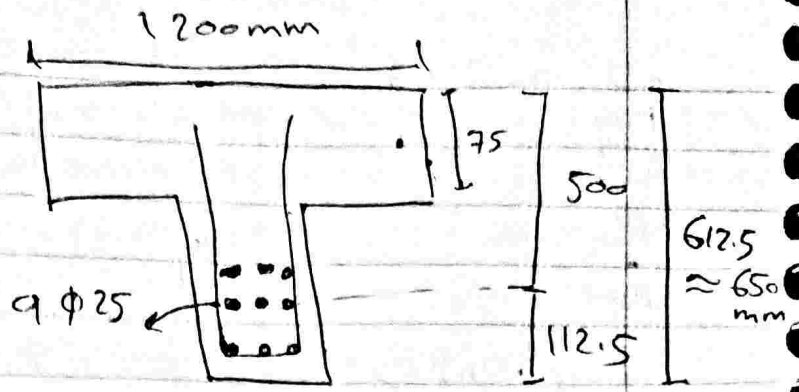
$\Rightarrow a = 117 \text{ mm}$ ,  $\bar{y} = 137.6 \text{ mm}$ ,  $E_s = 0.0079 > 0.005$   
 $\phi = 0.9$

- ④  $A_s = 4315 \Rightarrow 7 \phi 29 \rightarrow A_s = 4515 \text{ mm}^2$
  - or ②  $9 \phi 25 \rightarrow A_s = 4590 \text{ mm}^2$
  - ③  $3 \phi 43 \rightarrow A_s = 4365 \text{ mm}^2$
  - ④  $6 \phi 32 \rightarrow 4914$
- } check Spacing,  $\phi$  etc

In case ③  $\Rightarrow b_w = 2(40) + 2(10) + 3(43) + 2s' \Rightarrow s' = 23 \text{ X}$

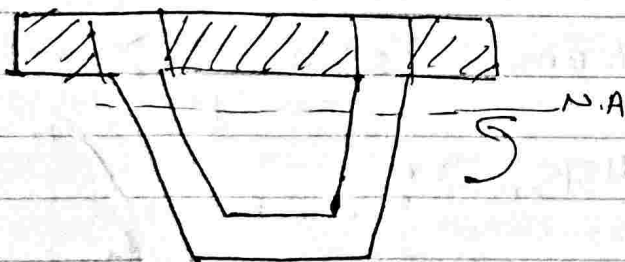
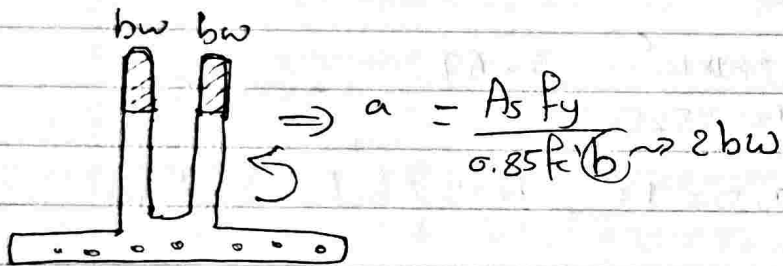
In case  $9 \phi 25 \Rightarrow 3 \text{ layers} \Rightarrow b_w = 2(40) + 2(10) + 3(25) + 2s' \Rightarrow s' = 62.5$

Choose  $9 \phi 25 \Rightarrow 3 \text{ layers}$ .



تغيرت (d) ← بعد التزايين ، به  
 زادت  $\mu$   
 فمعنى اصلا  
 بال safe side

• Arbitrary cross-section



• فقدرها انه تقسم بطريقة  
 مناسبة لكل عملية  
 التزايين .

