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كودات البناء  
الوطني الأردني

كودة  
الأعمال  
والقوى

عمان  
تموز ٢٠٠٦



الطبعة

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(Dynamic Excitation)

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(BS 2655)

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(Gantry Girders)

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(BS 2573)

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:(Dead Loads)

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:(Imposed Loads = Live Loads)

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(Partitions)

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:(Snow Loads)

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:(Roofs)

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:(Storage Height)

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:(Wind Forces)

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.(Suction) ( ) (Pressure)

:(Earthquake Forces)

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:(Partitions) ( ) //

**(Design Requirements)** /

:(Loads Combination) //

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:(Overturning and Slipping Resistance) //

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**(Dead Loads)**

**(General)** /

( - ) ( - ) ( - ) ( - ) ( - )

**(Actual Weights)** /

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(Actual Weights) //

**(Weights of Other Materials)** /

**(Partitions)** /

(Building Frames) //

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) (Slabs )

(Beams

(Equivalent Loads)

(Floors)

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/ (Uniformly Distributed Loads)

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: (Span ) \*

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$$(2 - 1) \quad W_{e(\max)} = \frac{2W_p}{L}$$

:

$$( / ) = W_e$$

$$( / ) = W_p$$

$$.( ) ( ) = L$$

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$$(2 - 2) \quad W_{e(\min)} = \frac{1.5 W_p}{L}$$

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$$(2 - 3) \quad W_e = \frac{W_p}{e}$$

:

$$e = \frac{h_p}{1000} + 0.3L + h$$

$$e_{(\max)} = \frac{h_p}{1000} + 0.6L$$

$$e_{(\min)} = 1.0 ( )$$

$$( ) = h_p$$

$$( ) ( ) = L$$

$$.( ) (0.3 L) = h$$

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**(Weights of Tanks and Other Receptacles)**

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27.50	Aluminum	
67.00	Antimony	
35.00	Barium	
85.00	Bronze	
214.00	Platinum	
193.00	Tungsten	
45.00	Titanium	
77.00	Wrought Iron	
72.50	Cast Iron	
72.00	Zinc	
193.00	Gold	
114.00	Lead	
65.00	Zirconium	
28.00	Aluminum Alloy	
61.00	Vanadium	
105.00	Silver	
78.50	Steel	
73.00	Tin	
86.00	Cadmium	
89.00	Cobalt	
17.00	Magnesium	
72.00	Manganese	
102.00	Molybdenum	
89.60	Cast Copper	
85.20	Brass	
89.00	Nickel	
191.00	Uranium	

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<b>(Hardwood)</b> .		
7.20	Oak	
7.00	Birch	
6.60	Sycamore	
6.60	Walnut	
6.60	Poplar	
6.00	Elm & Ash	
7.20	Beech	
6.60	Teak	
6.60	Chestnut	
7.20	Mahogany	
<b>(Softwood)</b> .		
4.00	White	
5.20	Red	
3.90	Cedar	
5.30	Douglas Fir	
4.50	Yellow Pine	
4.50	Hemlock	( )
5.30	Pine	

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10.40	Acetic Acid	
15.10	Nitric Acid	
18.10	Sulfuric Acid	
8.80	Ammonia	
7.40	Naphtha	
8.60		
8.60	Benzene, Benzol	
8.50	Turpentine	
10.00	Loose Drinks	
4.60	Drinks in Bottles	
5.50	Drinks in Barrels	
8.20	Methylated Spirit	
8.00 - 7.90	Alcohol	
7.90	Paraffin (Kerosene)	
8.80	Linseed Oil	
9.81	Fresh Water	
10.05	Sea Water	
10.20	Milk	
13.70	Bitumen	
11.80	Tar, Pitch	
11.80 - 9.70	Sewage	

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5.50	Brewer's Grains (Wet)	
7.10	Flour in Bulk	
6.30	Flour in Sacks	
12.00 - 9.50	Paper	
5.50	Paper Waste (Pressed)	
9.40	Salt in Packets	
14.10	Loose Salt	
7.90	Loose Sugar	
4.40	Tea in Chests	
9.30	Rice in Sacks	
6.20	Wheat in Sacks	
7.20	Loose Wheat	
6.40	Loose Coffee	
5.30	Coffee in Sacks	
7.20	Loose Potato	
6.40	Potato in Sacks	
5.15	Butter in Barrels	
4.80	Loose Cheese	
9.30	Fats	
5.95	Canned Meats	
11.90	Fig in Boxes	
9.60	Dry Fruits in Sacks	
7.20	Fresh Fruits in Sacks	
1.30	Hay (Pressed in Bales)	

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5.50 - 2.40	Cotton in Bales	
5.30	Cotton Goods (Encased Pieces) in Bales	
4.80	Cotton Goods (Encased Pieces)	
5.60	Hemp (Cannabis) in Bales	( )
5.15	Whirled Ropes	
7.20	Silk Goods in Envelopes	
7.70	Wool Pressed in Bales	
2.10	Loose Wool	
4.35	Wool Goods (Encased Pieces)	
3.20	Leathers in Bales	
13.00 - 9.60	Rubber	
10.40	Stacking Books	
12.50 - 8.95	Loose Coal	
3.20	Furniture	
9.00	Ice	
4.80	Carpets	
10.90	Eggs in Cartoons	
26.00	Glass	
12.00	Acrylic	
5.50	Onion in Sacks	
7.00	Tinned Pickles	

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	( / )
	15.00 - 10.00
	16.00
( )	14.20
( )	16.40
( )	18.00 - 15.00
( )	13.90
( )	15.90
( )	12.40
( )	14.50
( )	12.90
( )	14.60
( )	12.90
( )	14.50
( )	15.70
( )	18.10
	15.00
	14.90 - 5.50
	30.00
	28.00
	27.00
	23.00
	11.00 - 7.00
( )	20.00
( )	10.00
( )	18.25

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	( / )
( )	14.40
( )	20.00
( ) 70	15.00
( ) 100	14.50
( ) 150	14.00
( ) 200	13.50
) 140 ( 130 =	12.00
) 180 ( 150 =	11.00
) 240 ( 180 =	10.00
) 320 ( 300 =	12.50
	25.00 - 24.00
	22.00
	23.00
(1)	24.00
(2)	25.00
(5)	26.00
( )	20.00 - 12.00
( )	16.00 - 5.00
	9.00 - 3.00

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( / )	( / )	( / )	( )		
2.320	2.880	2.440	120		
5.720	5.280	4.840	240		( )
2.100	1.660	1.220	120		
3.300	2.860	2.420	240		( )
2.610	2.170	1.730	90	9	
6.850	6.410	5.970	290	9	
3.570	3.130	2.690	140	14	
6.900	6.460	6.020	290	14	( )
4.520	4.080	3.640	190	19	
6.790	6.350	5.910	290	19	
2.140	1.700	1.260	90	9	
5.660	5.220	4.780	290	9	
3.820	3.380	2.940	190	19	
5.330	4.890	4.450	290	19	( )
5.350	4.910	4.470	290	29	
2.280	1.840	1.400	70		
2.880	2.440	2.000	100		
3.880	3.440	3.000	150		( )
4.880	4.440	4.000	200		
1.980	1.540	1.100	70		
2.380	1.940	1.500	100		
3.080	2.640	2.200	150		( )
3.680	3.240	2.800	200		
4.330	3.890	3.450	150		
5.480	5.040	4.600	200		
3.280	2.840	2.400	100		
4.480	4.040	3.600	150		
5.680	5.240	4.800	200		
-	5.450	5.010	200		
-	6.650	6.210	250		
-	7.850	7.410	300		

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**(Live Loads, Imposed Loads)**

(Structural Elements)

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(Damping)

(Natural Frequency)

(Mode Shape)

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(Spectators)

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(Uniformly Distributed Load)

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(Concentrated Load)

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(Slabs )

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(Maximum Deflection)

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(Effective Lateral Distribution)

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(Local Effect)

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(Punching)

(Crushing)

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(1)

(0.33)

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**(Forces Due to Temperature Variations)**

(20)

(30)

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$$\epsilon = \alpha \cdot \Delta t$$

:

$$= \epsilon$$

$$= \alpha$$

$$= \Delta t$$

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Foundry		Assembly Hall	
Art Gallery		Balcony	
Gymnasium		Bank Hall	
Hallway		Bed Room	
Kitchen		Billiard Room	
Landing		Boiler Room	
Laundry		Cat Walk	
Lounge		Cold Storage	
Motor		Corridor	
Museum		Dance Hall	
Reading Room		Display & Sale Hall	
Stack Room		Dormitory	( )
Stage	( )	Dressing Room	
Stairs		Drill Room	
Stationery	( )	Factory	
Theater		Fan	
		Filing Room	
		Fly Gallery	
		Foot Bridge	( )

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	/			
1.4	2.0	.(All Usages)	:	.
1.8	2.0	.	:	.
-	2.0	.		
2.7	2.0	.		
4.5	3.0	.		
4.5	3.0	.		

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	/			
4.5	7.5	.	:	.
1.5		.		
. 1.0	.(3) -	.		
		.	:	
1.8	2.0	.		
-	2.0	.	.	
2.7	2.0	.		
4.5	4.0	.		
4.5	3.0	.		

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	/			
4.5	7.5	.	:	
3.6	5.0	.		
-	4.0	.		
-	5.0	.		
1.5		.		
.	(4)			
.		.		
		.		
		.		

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	/			
7.0	4.8 .(10)	.		.
7.0	2.4 .(6.5)	.		
9.0	4	.		
4.5	5.0	.		
9.0	5.0	.		
3.6	5.0	.		
4.5	3.0	.		
2.7	3.0	.		

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	/			
2.7	3.0	.		
4.5	2.5	.		
4.5	4.0	.		
1.8	2.0	.		
4.5	2.0	.		
1.8	2.0	.		
-	4.5	.		

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	/			
4.5	4.0	.		.
4.5	7.5	.		
4.5	4.0	.		
2.7	3.0	) .(		
9.0	4	.		.
4.5	5.0	.		
-	3.0	.		
2.7	2.5	.		
4.5	4.0	.		

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	/			
4.5	4.0			
9.0	5 .(15)			
9.0	4			

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	/			
7.0	2.4	.	.	.
3.6	4.0	.	.	.
-	20.0	.	.	.
9.0	5.0	.	.	.
	.(15)	.	.	.
7.0	4.0	.	.	.
7.0	2.4	.	.	.
9.0	12.5	.	.	.
4.5	4.0	.	.	.
4.5	4.0	.	.	.
4.5	5.0	.	.	.

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	/			
9.0	5.0 .(15)			
7.0	4.8 .(15)			
9.0	4.0			
9.0	4.0			
7.0	2.4			
4.5	7.5			

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	/			
4.5	5.0			.
1.0 .(1.0)	-			
4.5	7.5		( )	.
9.0	5.0			
		. (2500)		
9.0	5.0	(2500)		

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	/			
9.0	5.0		( ) .	
4.5	4.0			
4.5	4.0			
9.0	2.5			
		(2500)		

(Other Live Loads)

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:(Parapets, Balustrades and Railings)

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:(Ceilings, Skylights and Like Structures)

(Hangers)

(Timber Joists)

(Frames)

(Ribs of Skylights)

(Access Hatches)

(1.4)

(0.9)

(1.2)

:( - )

( )	( / )	( / )	
0.25	0.50	0.36	( )
0.50	1.00	0.74	( )
		0.22	(600) ( )
0.25	0.50	0.36	( )
0.50	1.00	0.74	( )

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( )	( / )	( / )	
.			:
1.50	1.50	1.50	(530) ( )
1.50	1.50	1.50	. ( )
.			
0.50	1.00	0.74	. ( )
0.50	1.00	0.74	. ( )
.			
1.50	1.50	1.50	. (3) ( )
1.50	1.50	3.00	(3) ( )
.			. ( )

( - )

( )	( / )	( / )	
.			
1.50	1.50	1.50	{( ) ( ) } ( )
.			
1.50	1.50	1.50	( )
( / )			( )

(Reductions)

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:(Columns, Walls & Foundations)

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:(Beams)

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(Reduction) ( )	(Number of Floors)
0	1
10	2
20	3
30	4
40	10 - 5
50	10

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( )	( )
0	0
5	50
10	100
15	150
20	200
25	250

: /

(1.5) //

:

$$F = \frac{0.5m v^2}{\delta_c + \delta_b}$$

:

.( ) = m

.( / ) = v

.( ) =  $\delta_c$

.( ) =  $\delta_b$

( / / ) //  
: (2500)

$$.( ) 1500 = m$$

$$.( / ) 4.5 = v$$

$$.( ) 100 = \delta_c$$

(F) (δ<sub>b</sub>)  
. (2500) (150)

( / / ) //  
: (2500)

$$.( ) = m$$

$$.( / ) 4.5 = v$$

$$.( ) 100 = \delta_c$$

(Bumper) //  
(2500)

. (375)

( / / ) ( / / ) (F) //

(610)

( / / ) ( / / ) (F)

(610)

. (20)

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**(Imposed Loads on Roofs Except Wind Forces)**

/ /

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(Imposed Roof Load)      ( )

.(Ponds)

.( / )

\*(Movement Joints)

.(    )

:(Accessible Roofs)      (    )

(30)

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/      (1.5)

\*

(0.3x 0.3)

(1.8)

\*

( / )

:(Inaccessible Roofs)

( )

(30)

:

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\*

(0.3x 0.3)

(0.9)

\*

\*

:

(30)

/ (0.6) -

/ {0.6 [(60 -  $\alpha$ ) / 30]} -

(60)

(30)

(60)

/ ( ) -

(Fragile)

:(Small Buildings)

( )

( )

( / / )

:

(200)

\*

(10)

\*

(1.5)

\*

:

-

(35)

( )

:

(S<sub>0</sub>)

\*

(1.25) ( / / )

/ (0.75)

\*

(0.9)

\*

(60)

(30) (α)

[(60 - α)/30]

(60)

:

//

/ (0.75)

/ (1.5)

( / / ) ( / / )

( / )

:(Roof Coverings)

//

(125)

(0.9)

: //

) ( // )  
.(

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**(Occasional Loads on Roof Trusses)**

:(Industrial and Commercial Buildings) //

()

(4.5)

(Frames) ( )

(4.5)

:(Other Buildings) //

( / / )

(1.3)

:(All Buildings) //

(1.3)

(1.2)

.( / / ) ( / / )

**(Snow Loads)** /

: 1/9/3

:(Site Altitude) ( )

:S<sub>o</sub> (Site Snow Load) ( )

:(Snow Load Shape Coefficient) ( )

:S<sub>d</sub> (Snow Load on Roof) ( )

:(Redistributed Snow Load) ( )

:(Variably Distributed Load) ( ) ( )

: //

:

= h

... i = b<sub>i</sub>

= F<sub>s</sub>

... =j = h<sub>oi</sub>

... =j = l<sub>si</sub>

= S<sub>d</sub>

= S<sub>o</sub>

= α

= β

= α

... = i = μ<sub>i</sub>

: //

:

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\*

:(Specific Gravity) //

(0.4 - 0.1) ( )

(0.25)

( )

(50)

(1.0)

: (Height of Structure) //

(25)

(S<sub>o</sub>) ( - )

(1500)

( - )

( / ) (S <sub>o</sub> )	( ) (h)
0	250 > h
(h-250)/800	500 > h > 250
(h-400)/320	1500 > h > 500



( - ) ( - )

(Empirical)

( $b_1, h_{o1}, I_{s1}, b_2 \dots c_k$ )

( / )

:(Single Span Roofs) ( )

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( / / )

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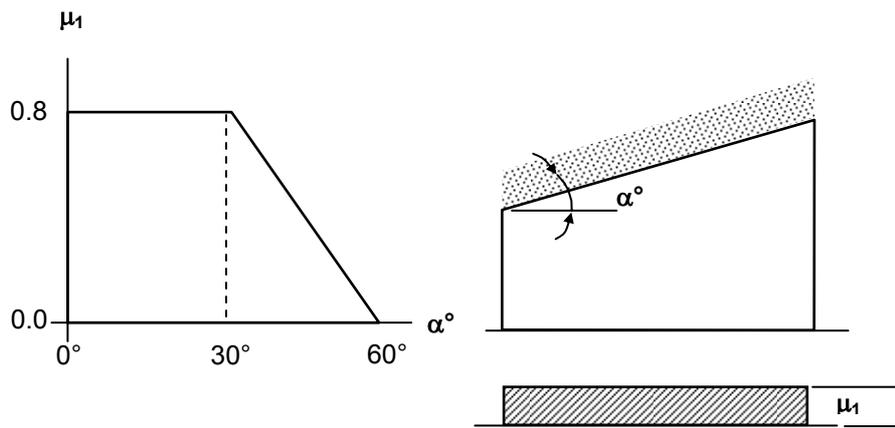
( )

( $\mu_i$ )

( - )

(α)

$60^\circ \leq \alpha^\circ$	$30^\circ < \alpha^\circ < 60^\circ$	$0^\circ \leq \alpha^\circ \leq 30$	$\alpha^\circ$
$\mu_1 = 0$	$\mu_1 = 0.8 \left[ \frac{60 - \alpha}{30} \right]$	$\mu_1 = 0.8$	$\mu_1$



( - )

: ( )

(μ<sub>i</sub>)

: \*

: -( ) \*

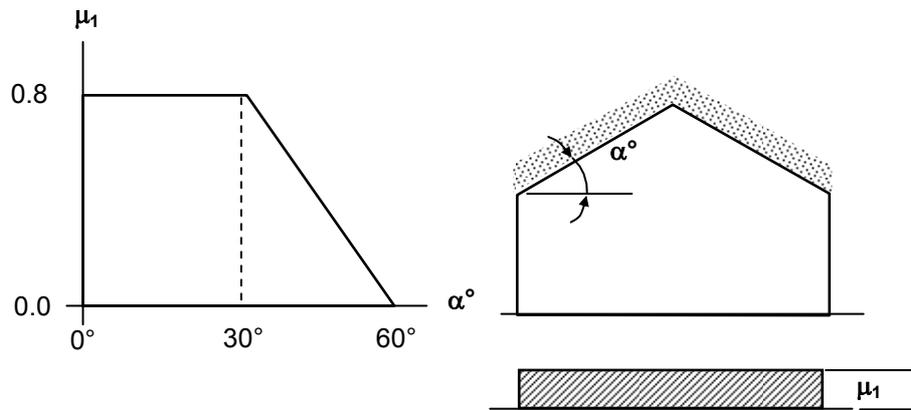
( - - )

:(asymmetric) -( ) \*

(Ridge)

( - - )

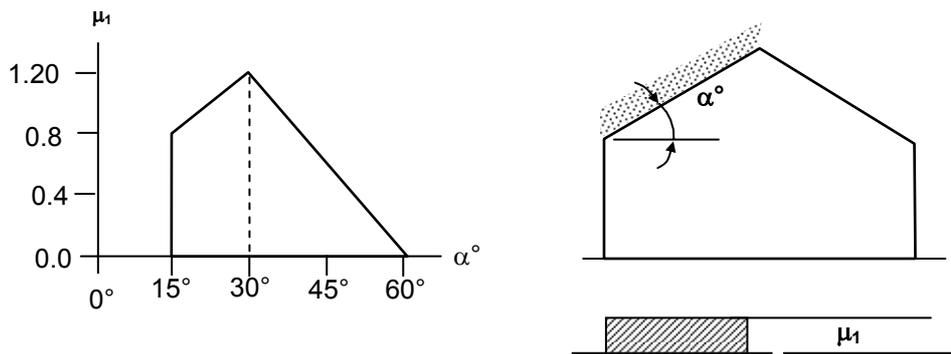
$60^\circ \leq \alpha^\circ$	$30^\circ < \alpha^\circ < 60^\circ$	$0^\circ \leq \alpha^\circ \leq 30$	$\alpha^\circ$
$\mu_1 = 0$	$\mu_1 = 0.8 \left[ \frac{60 - \alpha}{30} \right]$	$\mu_1 = 0.8$	$\mu_1$



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.( ( ) )

$60^\circ \leq \alpha^\circ$	$30^\circ < \alpha^\circ < 60^\circ$	$15^\circ < \alpha^\circ \leq 30^\circ$	$0^\circ < \alpha^\circ \leq 15^\circ$	$\alpha^\circ$
$\mu_1 = 0$	$\mu_1 = 1.2 \left[ \frac{60 - \alpha}{30} \right]$	$\mu_1 = 0.8 + 0.4 \left[ \frac{\alpha - 15}{15} \right]$	$\mu_1 = 0$	$\mu_1$



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( $\mu_i$ )

:

( $\beta$ )

: -

(60) ( $\delta$ ) (Eaves)

: -

(60)

(60)

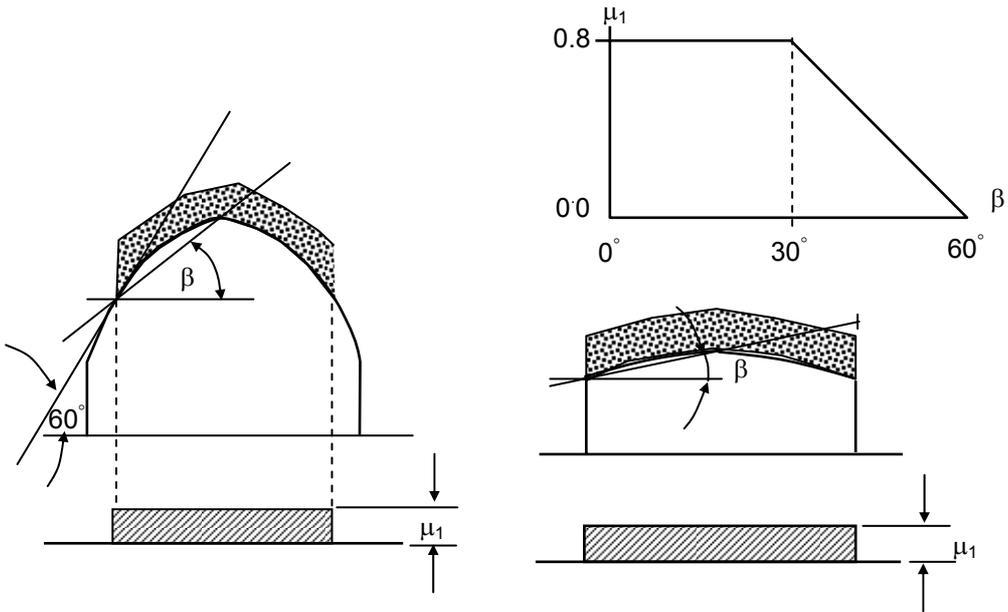
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( )

(60)

.( - - )

$\beta \geq 60^\circ$	$60^\circ > \beta > 30^\circ$	$30^\circ \geq \beta \geq 0^\circ$	$\beta$
$\mu_1 = 0$	$\mu_1 = 0.8 \left[ \frac{60 - \beta}{30} \right]$	$\mu_1 = 0.8$	$\mu_1$



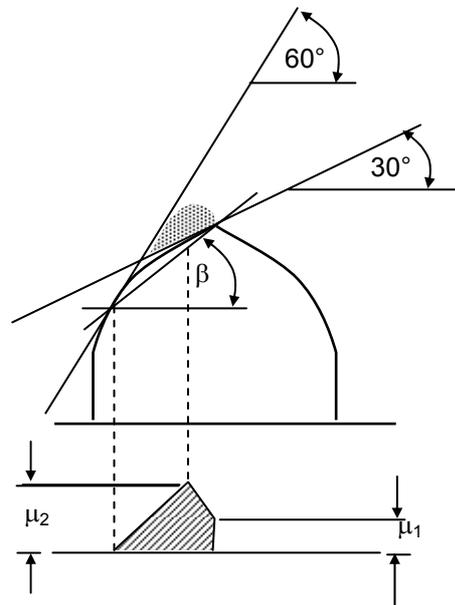
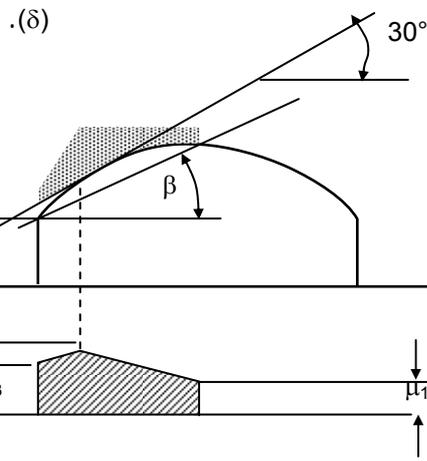
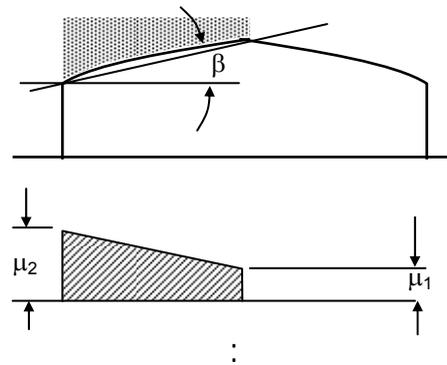
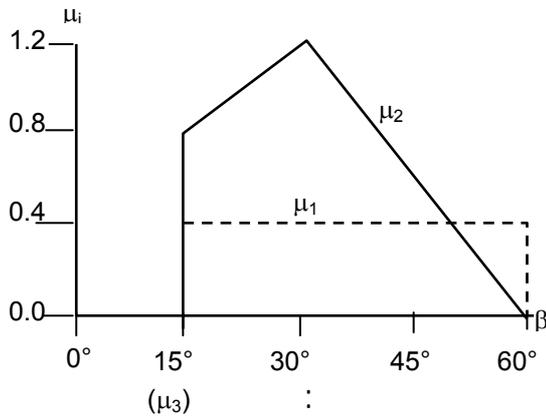
:( - - )

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$\beta \geq 60^\circ$	$60^\circ > \beta > 30^\circ$	$30^\circ \geq \beta > 15^\circ$	$15^\circ \geq \beta \geq 0^\circ$	$\beta$
$\mu_1 = 0$	$\mu_1 = 0.4$	$\mu_1 = 0.4$	$\mu_1 = 0$	
$\mu_2 = 0$	$\mu_2 = 1.2 \left[ \frac{60 - \beta}{30} \right]$	$\mu_2 = 0.8 + 0.4 \left[ \frac{\beta - 15}{15} \right]$	$\mu_2 = 0$	
$\mu_3 = 0$	$\mu_3 = \mu_2 \left[ \frac{60 - \delta}{30} \right]$	$\mu_3 = \mu_2 \left[ \frac{60 - \delta}{30} \right]$	$\mu_3 = 0$	



(60) و (30)

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:( ) ( )

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(Valley) ( )

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(Valley)

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:(Valleys of Multi- span Roofs)

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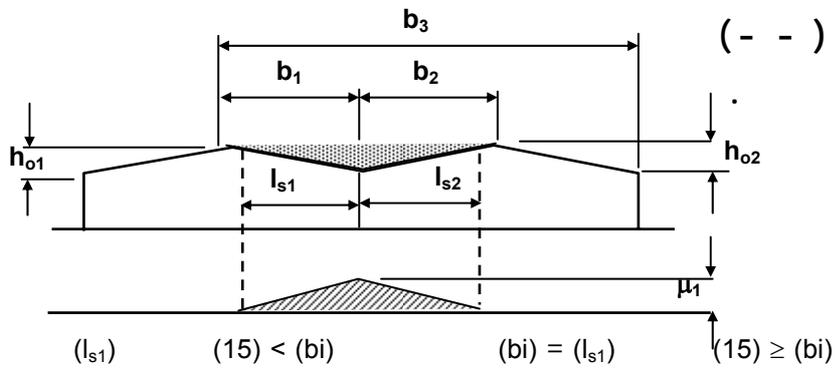
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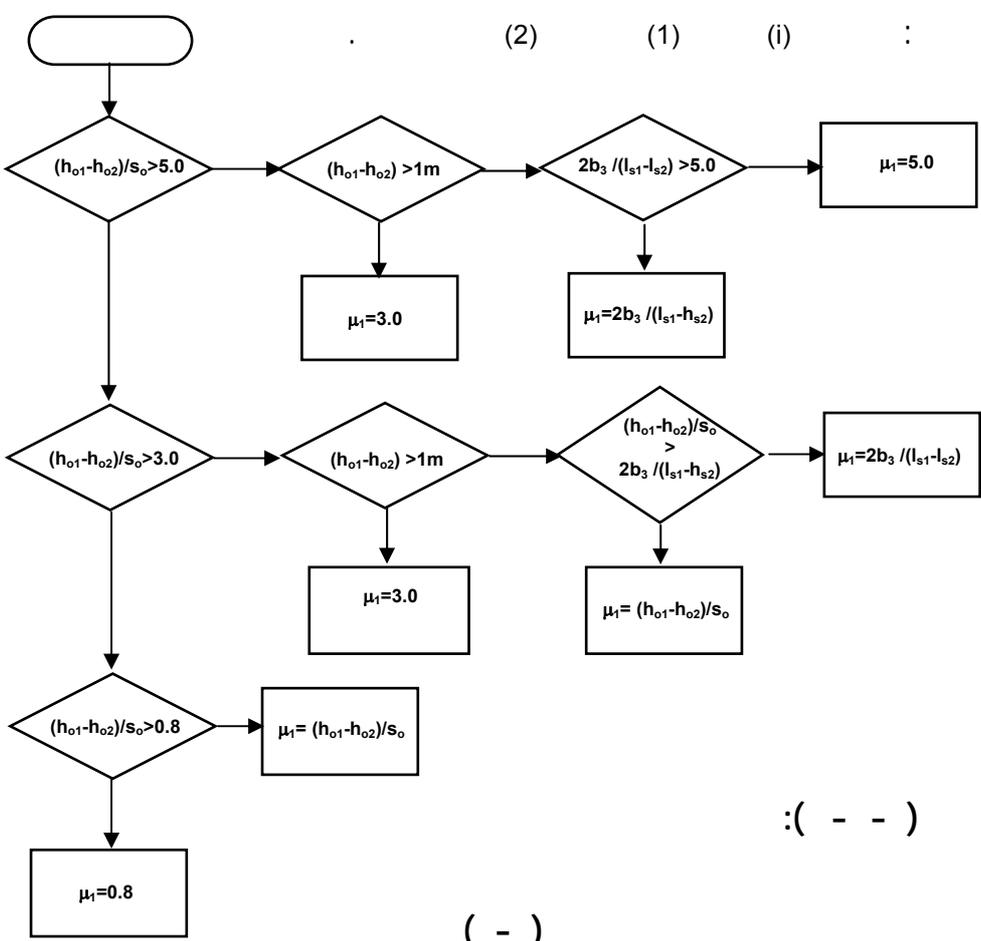
.

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(h<sub>02</sub> - h<sub>01</sub>)



(15)



:( - - )

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:(Roofs Abutting or Close to Taller Structures)

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:(T- Intersections) (T)

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:(Local Projections and Obstructions)

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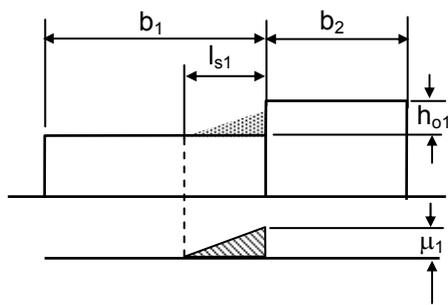
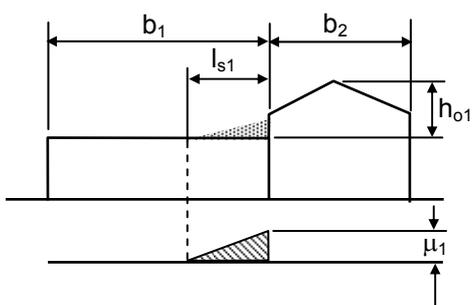
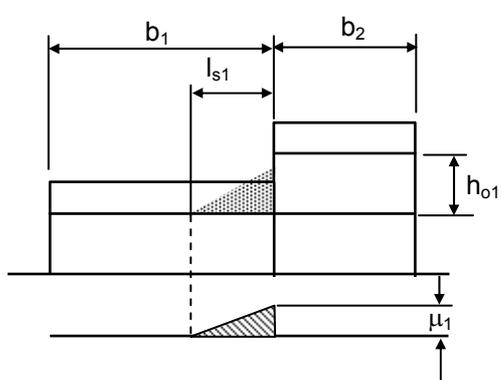
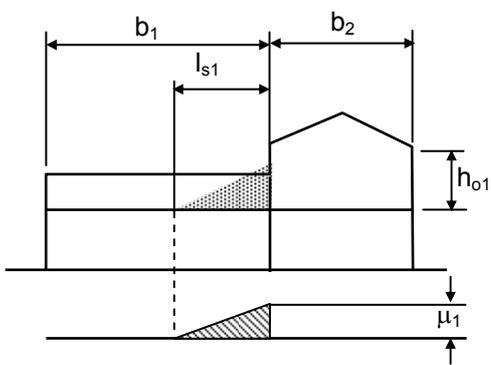
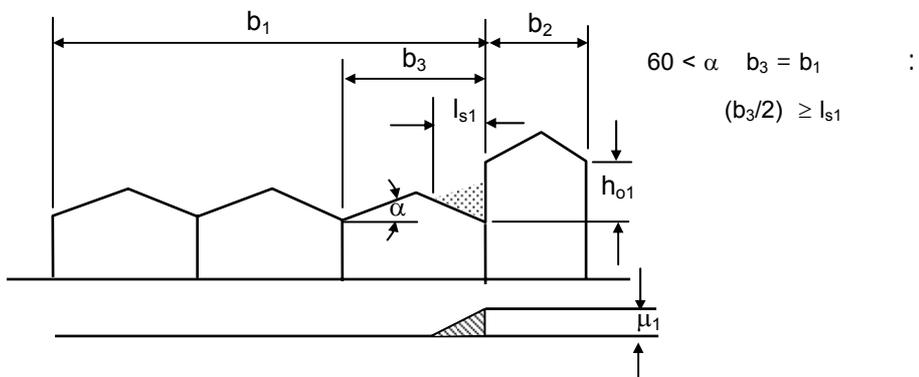
.(Over Loading Bays)

.( - )

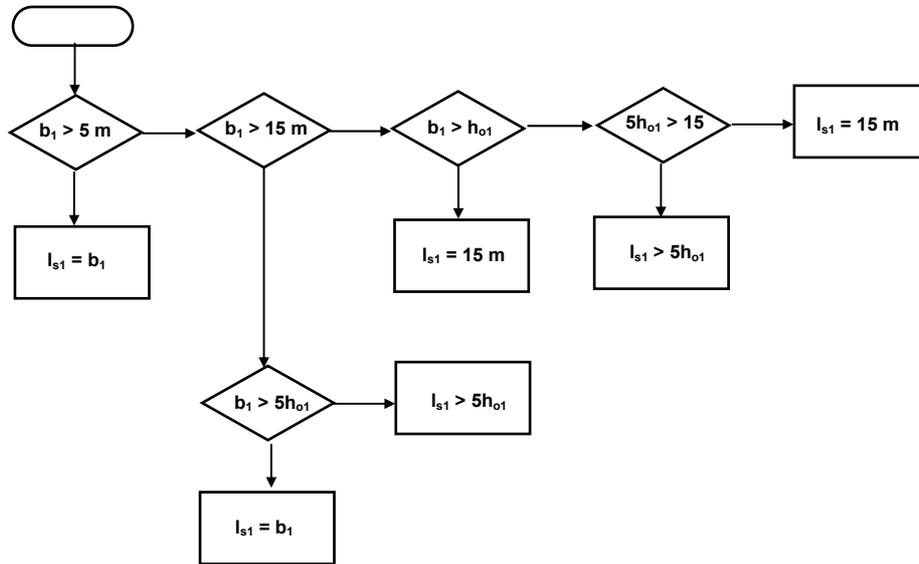
(Gable)

:

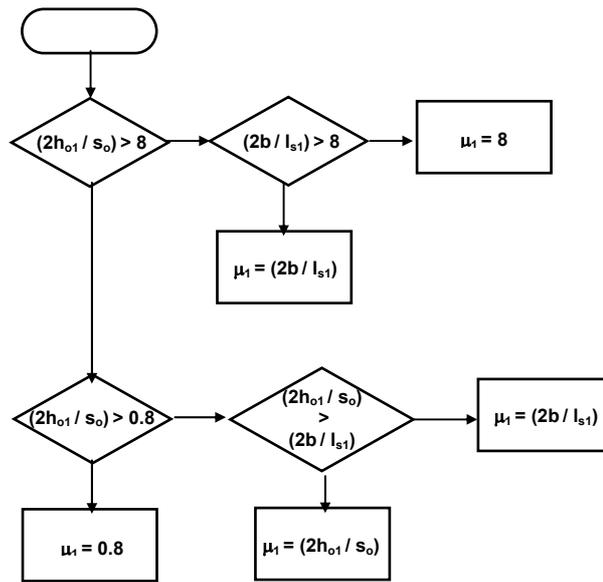
.(300)



( - )



:( - - )



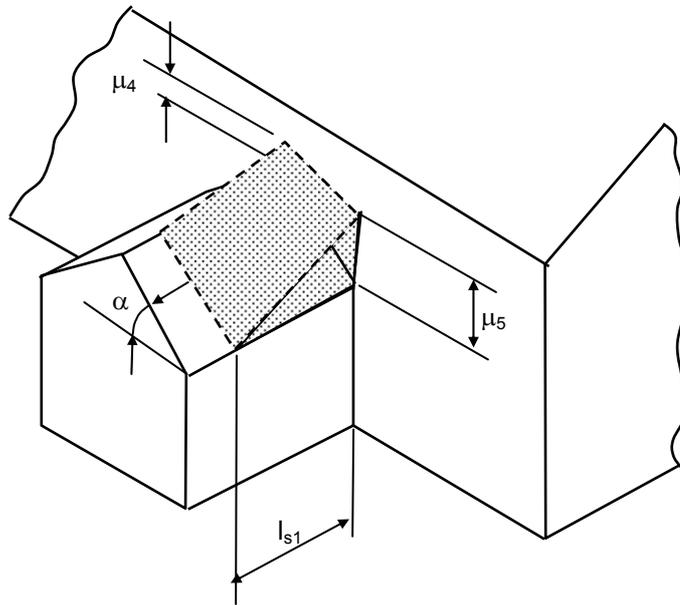
.(b<sub>2</sub>) (b<sub>1</sub>)

(b)

:

:( - - )

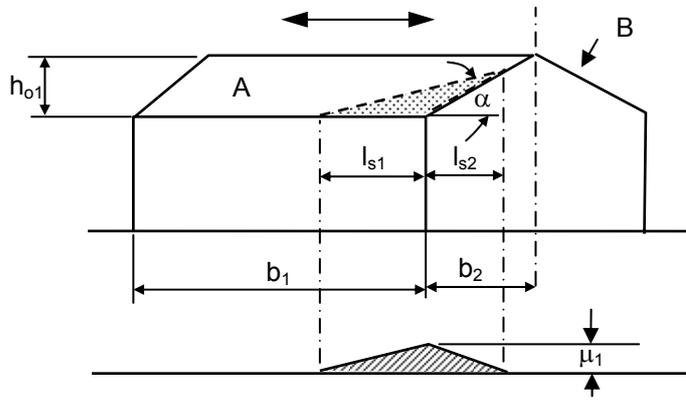
( - )



( - )  $\mu_4 = \mu_1 = \alpha$   
 $\mu_5 = \mu_4 = \mu_1$   
 $l_{s1} = \mu_1$

$60^\circ \leq \alpha$	$60^\circ > \alpha > 30^\circ$	$30^\circ \geq \alpha > 15^\circ$	$15^\circ \geq \alpha \geq 0^\circ$	( $\alpha$ )
$\mu_4 = 0^\circ$	$\mu_4 = 0^\circ$	$\mu_4 = \mu_1 [(30-\alpha)/15]$	$\mu_1 = \mu_4$	
$\mu_5 = 0^\circ$	$\mu_5 = \mu_1 [(60-\alpha)/30]$	$\mu_1 = \mu_5$	$\mu_1 = \mu_5$	

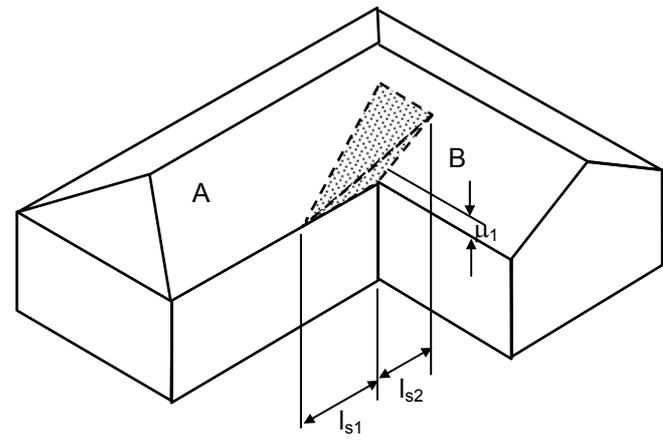
( - )



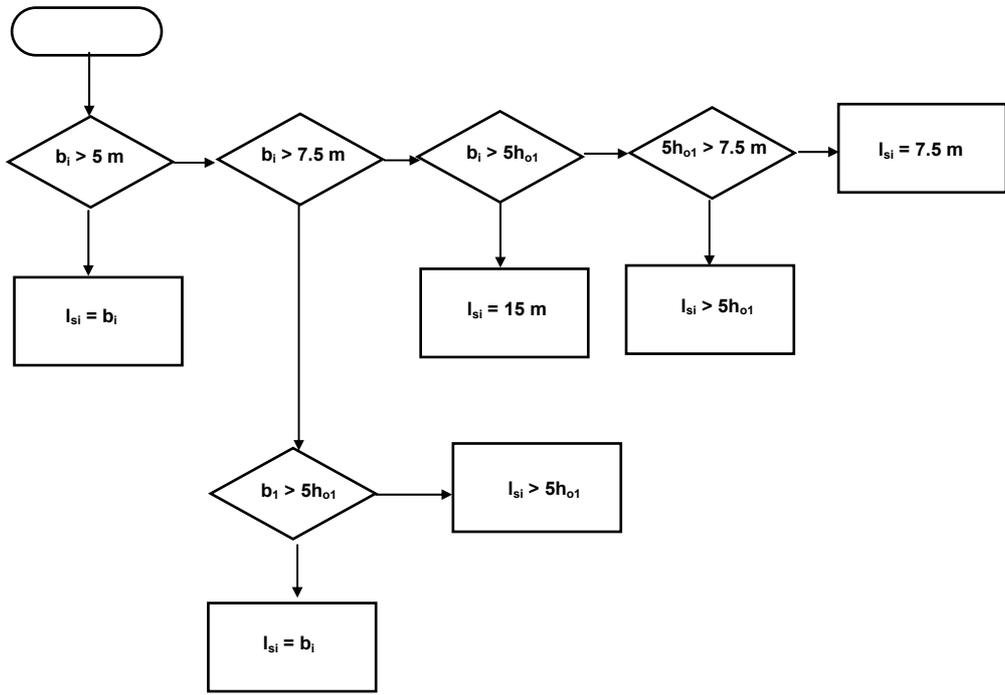
$\mu_1$  : ( )

: ( )

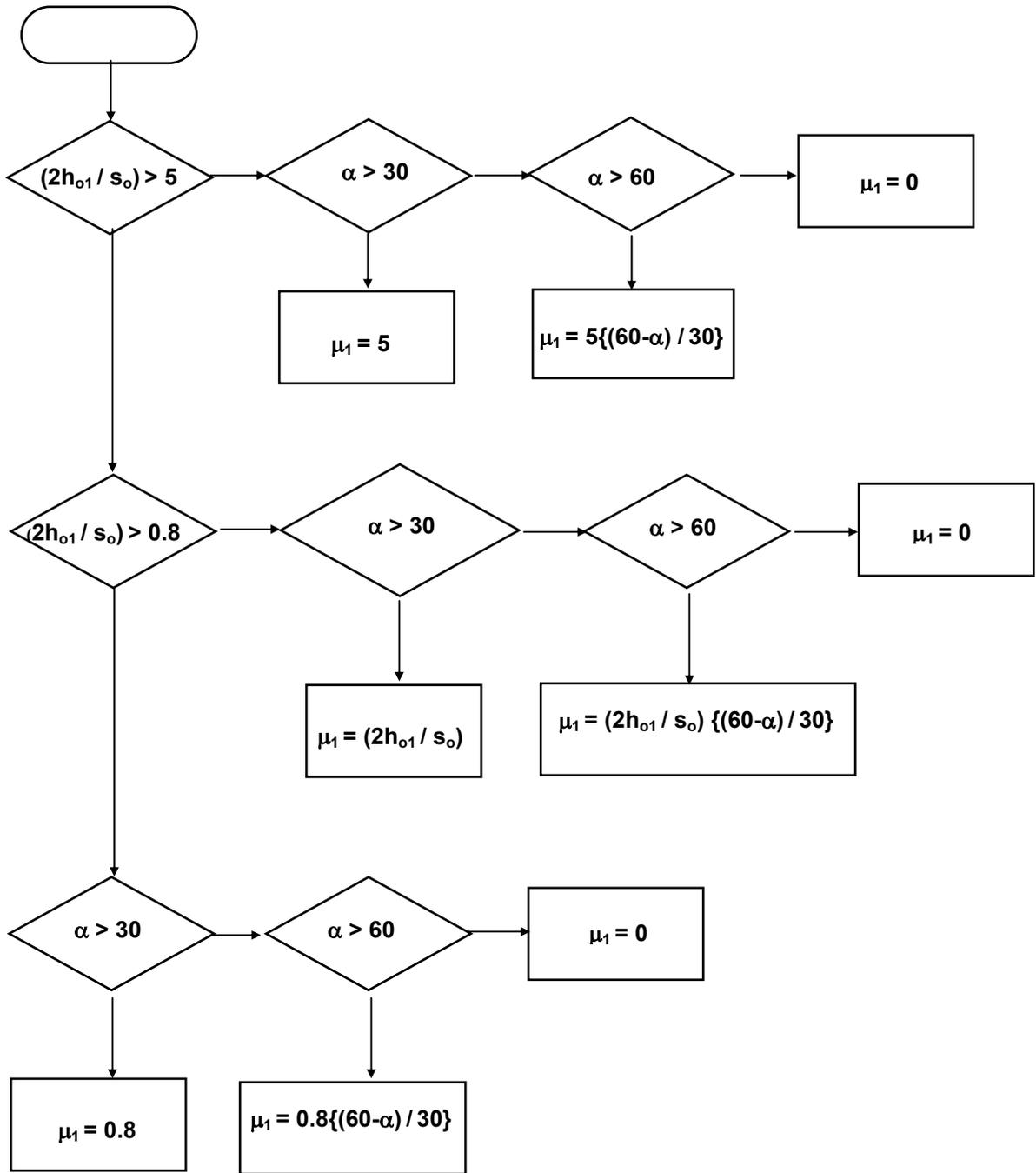
.B



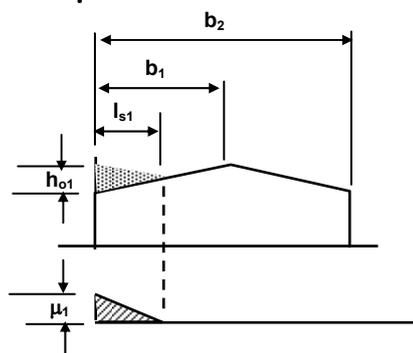
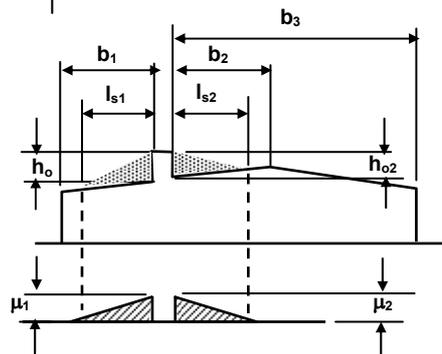
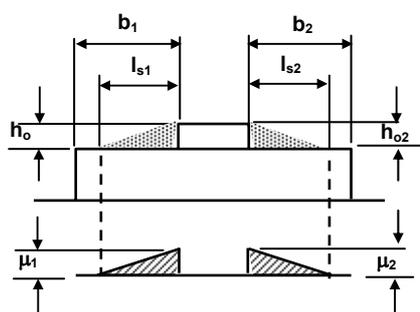
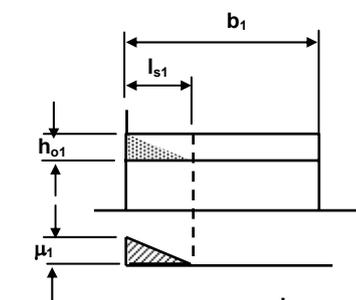
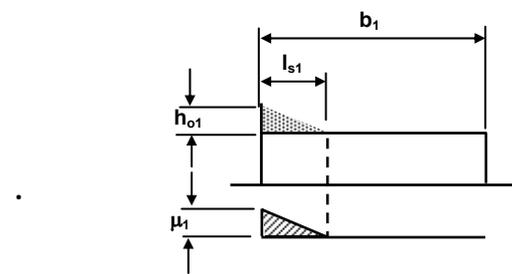
( - )



:( - - )

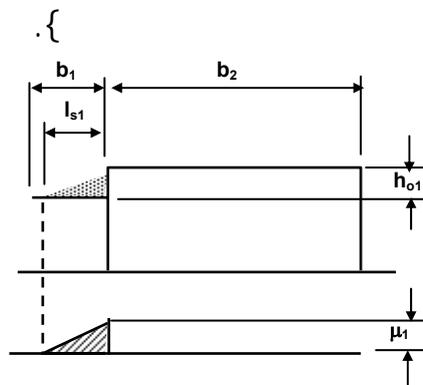


:( - - )



(b2) (b3) }

(b1) (b2) }



(b1) (b2) }

{ (b1) < (b2)

( - )

:(Snow Sliding Down Roofs)

(A)

:

(F<sub>s</sub>)

$$F_s = S_d b \sin \alpha$$

:

( / )

= S<sub>d</sub>

( )

= b

= α

(Onerous)

( / / )

S<sub>d</sub>

/

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( ... )

(100)

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: ()

(2)

(10)

(11)

.( / / )

( )  
(25)

(S<sub>a</sub>)

: ( )

( )

: ( )

: ( )

: ( )

(Potential)

: ( )

: ( )

: ( )

( )

: ( )

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: ( )

:(Altitude) ( )

( )

:( ) ( )

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:( ) ( )

:( ) ( ) ( )

: ( )

(Extent)

: ( )

(Extent)

: ( )

:(Scaling Length) ( )

:(Fetch) ( )

		:	//	
				= A
( $\Delta$ // )		( )		= A <sub>s</sub>
			( // )	
				= a
	( - )			= B
				= b
				= C <sub>a</sub>
				= C <sub>f</sub>
				= C <sub>p</sub>
				= C <sub>pe</sub>
				= C <sub>pi</sub>
				= C <sub>r</sub>
				= D
(Inset)	(eaves)	(Ridge)		= H
		(Lower Storey)		
				= H <sub>e</sub>
				= H <sub>r</sub>
				= H <sub>o</sub>
(Free-standing Wall)				= h
		(Signboard)		
				= K <sub>b</sub>
				= L
		( )		= L <sub>D</sub>
		( )		= L <sub>e</sub>

( // )

- = C<sub>l</sub>
- = d
- = F<sub>r</sub>
- = F<sub>w</sub>
- = P
- = p
- = q
- = S<sub>a</sub>
- = S<sub>b</sub>
- = S<sub>p</sub>
- = S<sub>d</sub>
- = V<sub>b</sub>
- = V<sub>s</sub>
- = W

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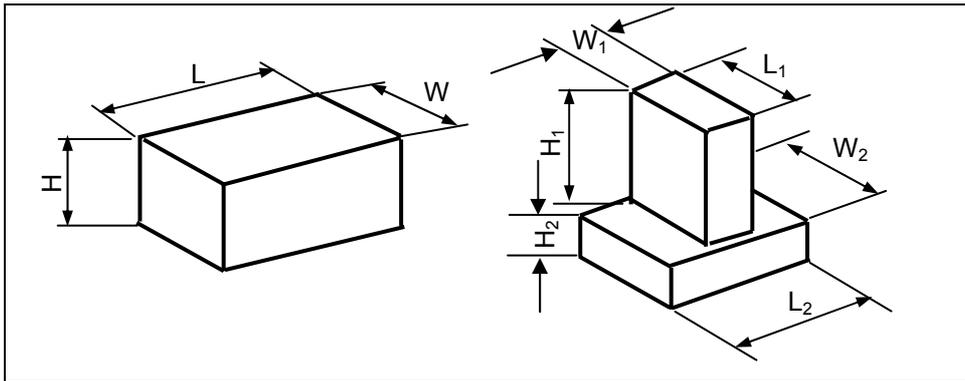
(Dynamic Excitation)

(susceptible)

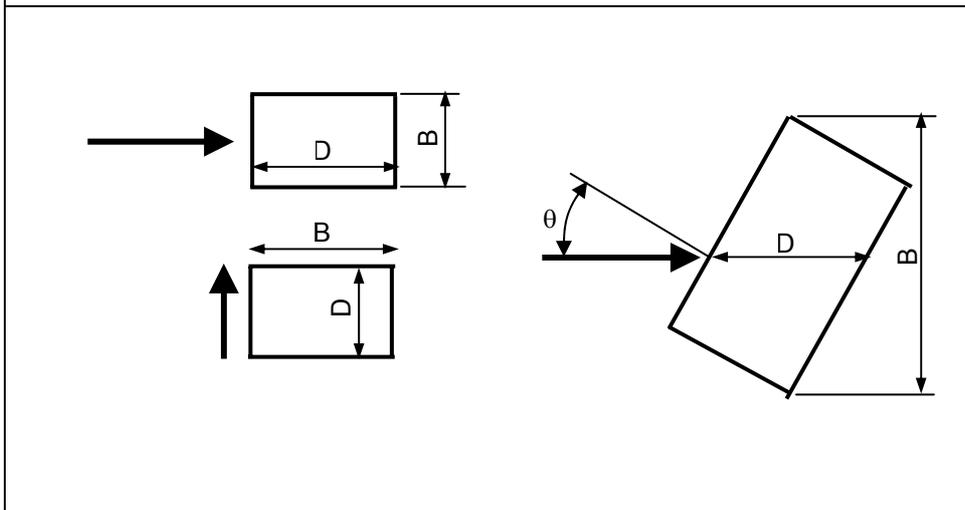
(Mildly Dynamic Structures)

. ( $C_r$ ) (Dynamic Augmentation Factor)

. ( - ) ( $K_b$ )



. : ( )

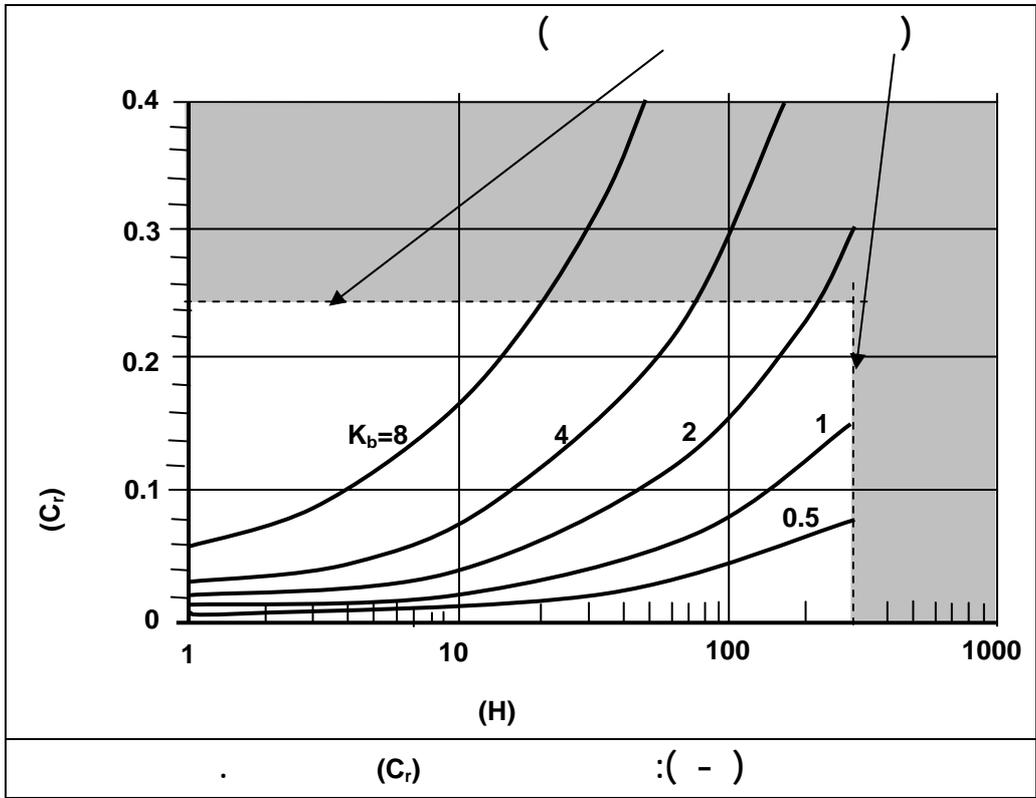


. : ( )

.	
( )	
:( - )	
(K <sub>b</sub> )	
(K <sub>b</sub> )	
8	.
4	.
2	.
1	.
0.5	.

.( - ) (C<sub>r</sub>) ( - )

---



: //  
 : ( )  
 : \*  
 : \*  
 : \*  
 (5)  
 : ( )  
 (H<sub>r</sub>) ( )  
 ( )

(H<sub>e</sub>) ( )

.(H<sub>r</sub>)

(H<sub>e</sub>) ( )

.( - )

(X) (H<sub>o</sub>)

: (H<sub>e</sub>)

<b>(H<sub>e</sub>)</b>	
(0.4H <sub>r</sub> ) (H <sub>r</sub> - 0.8H <sub>o</sub> )	2H <sub>o</sub> ≥ X
(H <sub>r</sub> )	6H <sub>o</sub> ≤ X
(0.4H <sub>r</sub> ) (H <sub>r</sub> - 1.2H <sub>o</sub> + 0.2X)	2H <sub>o</sub> < X < 6H <sub>o</sub>

( )

(H<sub>e</sub>)

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/

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.(( ) - )

()

(°45±) ( )

(°180 = θ) (°0 = θ)

: ()

: (q<sub>s</sub>) ()

(4-1)  $q_s = 0.613 V_e^2$

= q<sub>s</sub> :

.( / )

( / ) = V<sub>e</sub>

( // )

$$(q_s) \quad ( )$$

$$/ \quad (550)$$

$$: \quad ( )$$

$$: \quad ( )$$

$$: \quad (p_e)$$

$$(4-2) \quad p_e = q_s C_{pe} C_a$$

:

$$.( / )$$

$$= q_s$$

$$= C_{pe}$$

$$.( / / ) \quad ( / / )$$

$$= C_a$$

$$( )$$

$$: \quad ( )$$

$$: \quad (p_i)$$

$$(4-3) \quad p_i = q_s C_{pi} C_a$$

:

$$.( / )$$

$$= q_s$$

$$( / / )$$

$$= C_{pi}$$

$$= C_a$$

$$( )$$

$$: \quad ( )$$

$$: \quad (p)$$

$$(4-4) \quad p = p_e - p_i$$

( )

:

(4-5)  $p = q_s C_p C_a$

:

.( / )

=  $p_e$

.( / )

=  $p_i$

.( / )

=  $q_s$

=  $C_p$

( // )

( )

.( // )

=  $C_a$

( )

:

( )

(a)

( - )

.( - )

(a)

.( // )

( 5 = a )

:

( )

:

(4-6)  $P = p A$

:

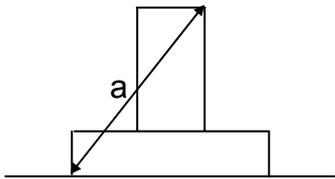
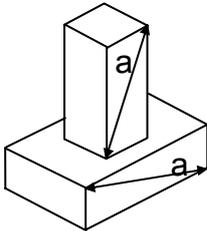
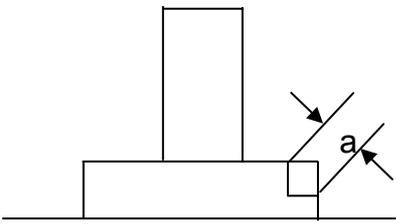
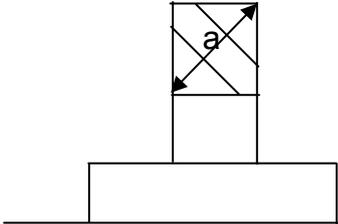
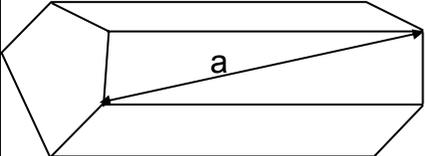
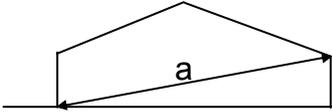
.( / )

=  $p$

.( )

=  $A$

$(C_a)$	:( - )
$(C_a)$	( ) (a)
1.0	$5 \geq$
0.95	10
0.90	20
0.85	60
0.80	125
0.75	300
0.70	400
0.65	1000

 <p>( )</p>	 <p>( )</p>
 <p>( )</p>	 <p>( )</p>
 <p>( )</p>	 <p>( )</p>
(a)	( - )

: ( )

(4 - 7) (P)

:(0.85) (ΣP<sub>front</sub> - ΣP<sub>rear</sub>)

(4 - 7) P = 0.85(ΣP<sub>front</sub> - ΣP<sub>rear</sub>)(1 + C<sub>r</sub>)

= ΣP<sub>front</sub>

= ΣP<sub>rear</sub>

= C<sub>r</sub>

.( / / )

: ( )

( )

: ( )

(60) \*

(100)

\*

(60)

: ( )

) (P<sub>f</sub>)

( )

( )

:

(4 - 8) P<sub>f</sub> = q<sub>s</sub> C<sub>f</sub> A<sub>s</sub> C<sub>a</sub>

$$\begin{aligned} & \quad \quad \quad ( \quad ) & = & A_s \\ & \quad \quad \quad \cdot ( \quad // ) ( \quad // ) \\ & \cdot ( - ) & = & C_f \end{aligned}$$

: //

: ( )

( )

$$\begin{aligned} & ) & & (V_b) \\ & \cdot & & ( \end{aligned}$$

$$\begin{aligned} & \quad \quad \quad (V_b) \\ & \quad \quad \quad / (33.33) : / (120) (V_e) \\ & / (33.33) & \cdot (10) \\ & ( - ) & (10) & (1.62 = S_b) \end{aligned}$$

(S<sub>b</sub>)

· (V<sub>e</sub>)

:(V<sub>s</sub>) ( )

: ( )

: (V<sub>s</sub>)

$$(4 - 9) \quad V_s = V_b \times S_a \times S_d \times S_s \times S_p$$

:

$$( \quad // ) \quad = \quad V_b$$

· ( // )

$$\cdot ( ) \quad = \quad S_a$$

$$\cdot ( ) \quad = \quad S_d$$

$$\cdot ( ) \quad = \quad S_s$$

$$\cdot ( ) \quad = \quad S_p$$

:(S<sub>a</sub>) ( )

(V<sub>b</sub>)

(4 - 10)

(4 - 10) S<sub>a</sub> = 1 + 0.001Δ<sub>s</sub>

:

.( )

= Δ<sub>s</sub>

.( - )

.(4 - 12) (4 - 11)

(4 - 11) S<sub>a</sub> = 1 + 0.001Δ<sub>s</sub>

(4 - 12) S<sub>a</sub> = 1 + 0.001Δ<sub>T</sub> + 1.2ψ<sub>e</sub>s

:

.( )

= Δ<sub>s</sub>

( )

= Δ<sub>T</sub>

.( )

( )

= ψ<sub>e</sub>

.(Δ)

( )

= s

( )

( - ) ( - )

:

(L<sub>e</sub>)

(ψ<sub>e</sub>)

.(L<sub>U</sub> = L<sub>e</sub>) (ψ<sub>U</sub> = ψ<sub>e</sub>) (0.30 > ψ<sub>U</sub> > 0.05)

.(  $\frac{Z}{0.3} = L_e$  ) (0.30 = ψ<sub>e</sub>) (0.30 ≤ ψ<sub>U</sub>)

.( )

(s)

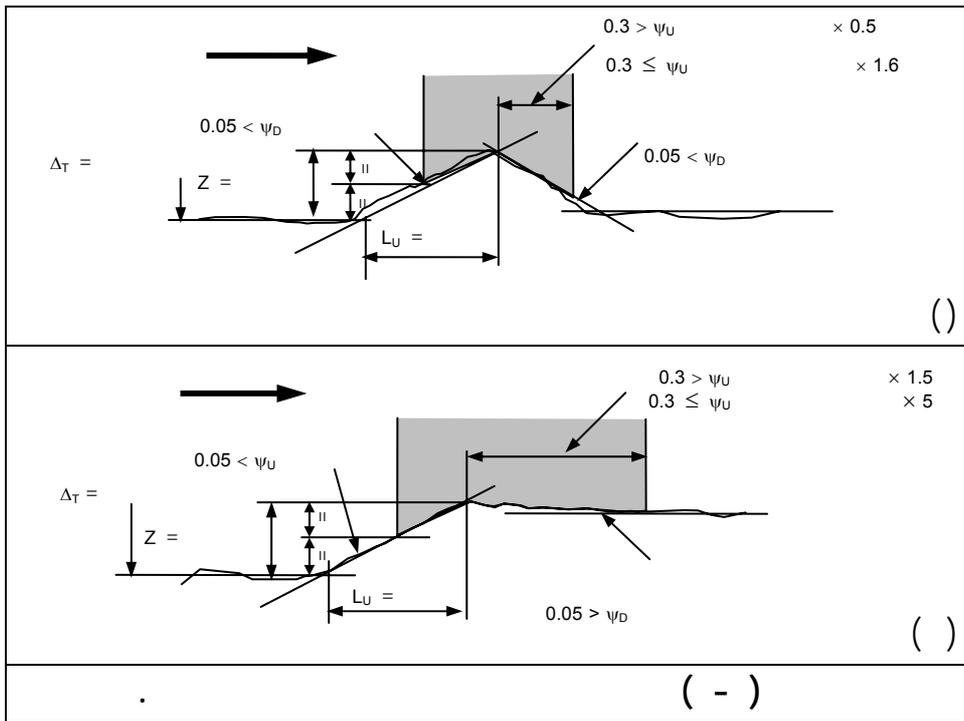
( - )

( ) ( )

(s)

: ( )

$$(1.0 = S_d)$$



: ( )

$$(S_s)$$

( )

(6)

( )

$$(1.0 = S_s)$$

$$(0.02)$$

: ( )

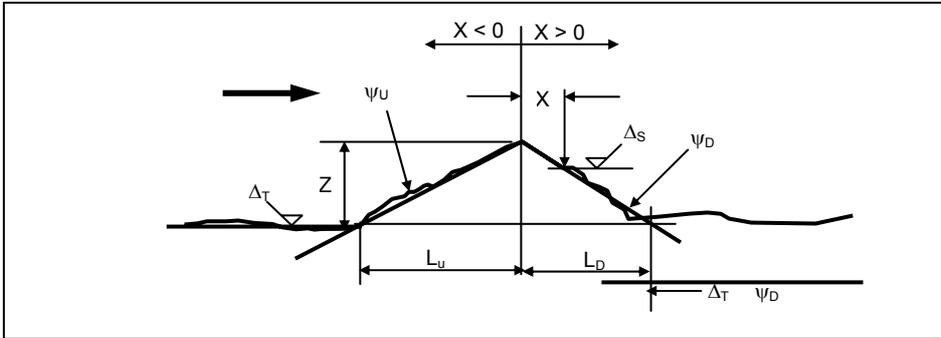
$$(S_p)$$

$$(0.02 = Q)$$

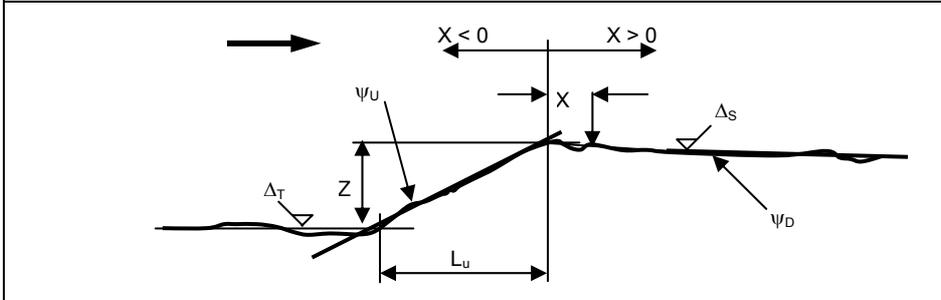
$$(1.0 = S_p)$$

. ( )

$$(0.02 = Q)$$



( )



( )

:

$\Delta_s$	$L_D$
$\Delta_T$	$L_U$
$\psi_U$	$X$
$\psi_D$	$Z$
( - )	

: ( )

: (V<sub>e</sub>) ( )

(4 - 13)  $V_e = V_s \times S_b$

:

(°45±)

= V<sub>s</sub>

( )

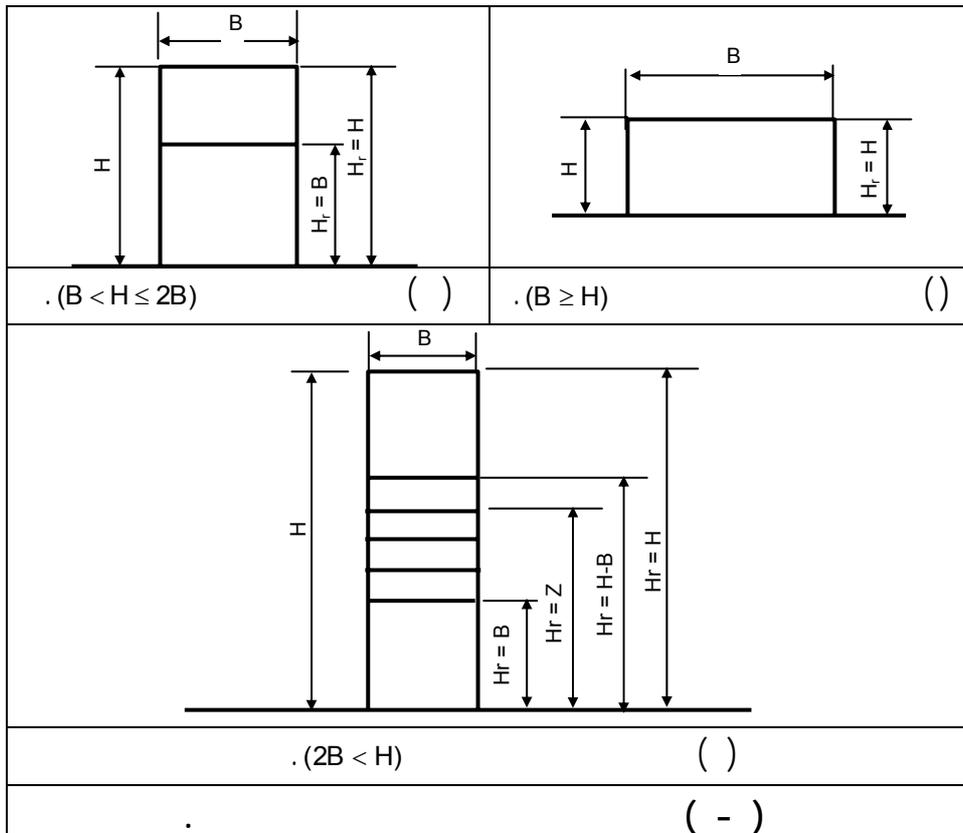
= S<sub>b</sub>

( )

( - )

(H<sub>r</sub>)

(a)



.( - ) (S<sub>b</sub>) ( )

(S <sub>b</sub> )	:( - )	
2 ≤ )		(H <sub>e</sub> )
(		
1.07	1.26	2 ≥
1.36	1.45	5
1.58	1.62	10
1.71	1.71	15
1.77	1.77	20
1.85	1.85	30
1.95	1.95	50
2.07	2.07	100
:		
		( )
.( 5 = a)		( )
( 100 < H <sub>e</sub> )		( )

: //

( // )

( // ) ( // )

: //

: ( )

(C<sub>pe</sub>) ( - ) ( )  
 .( - )

(windward)

(D)  $\left(\frac{D}{H} \geq 4\right)$   $\left(\frac{D}{H} \leq 1\right)$

(Leeward)

(H) ( - )

(°15±)

( - )

(BS 6399: Part 2:1997)

( / / / )

		$(C_{pe})$				$( - )$	
				(Span)			
				/			
				$4 \leq \frac{D}{H}$	$1 \geq \frac{D}{H}$		
1.6 -	1.3 -	(A)		0.6 +	0.8 +	)	(
0.9 -	0.8 -	(B)		0.1 -	0.3 -	)	(
0.9 -	0.4 -	(C)					
$\left(1 < \frac{D}{H} < 4\right)$						:	( / / )

( )

(b)

( - )

(B)  $(2H = b)$   $(B = b)$

(H) ( - )

( )

( )

(b)

$(C_{pe})$

:

(C<sub>pe</sub>) (b) (b/4) \*

( - )

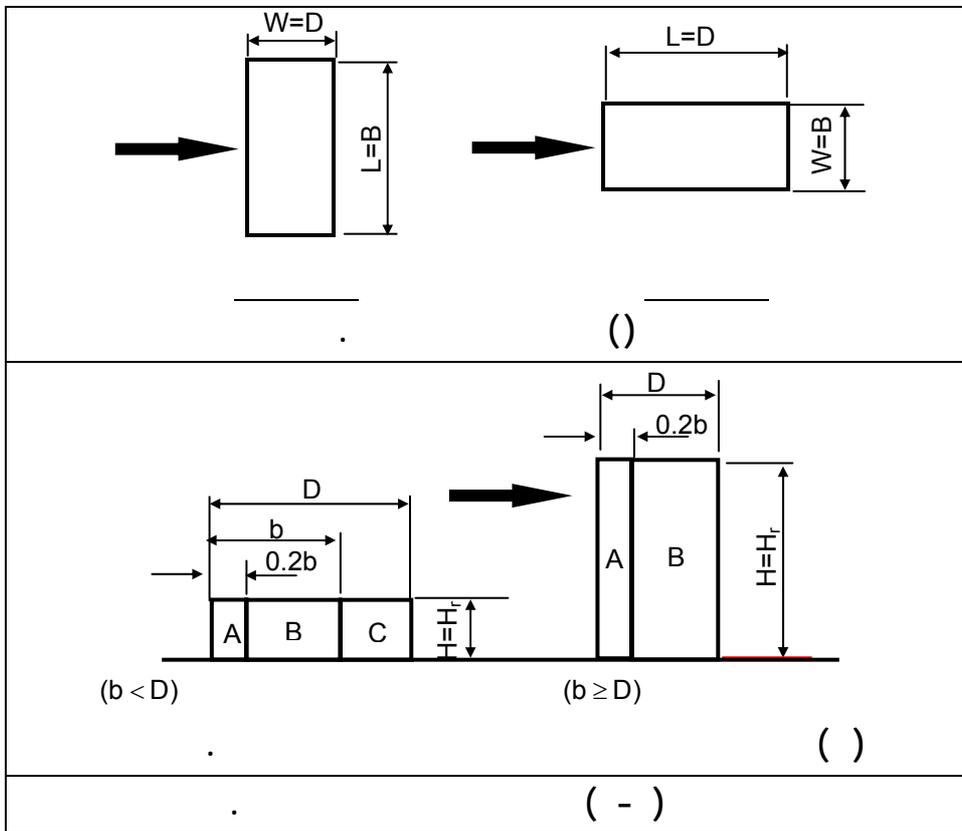
(C<sub>pe</sub>) (b) (b/4) \*

( - ) :

(b/2)

(b) (b/4) ( - )

(b) (b/2) (b/2) (b/4)



( )

( - )

( // // ) (°90 ≤

(BS 6399: Part 2:1997)

( - )

(BS 6399: Part 2:1997) ( / / / / ) (23)

:(Recessed) (Re-entrant) ( )

( - ) ( )

:( - )

\*

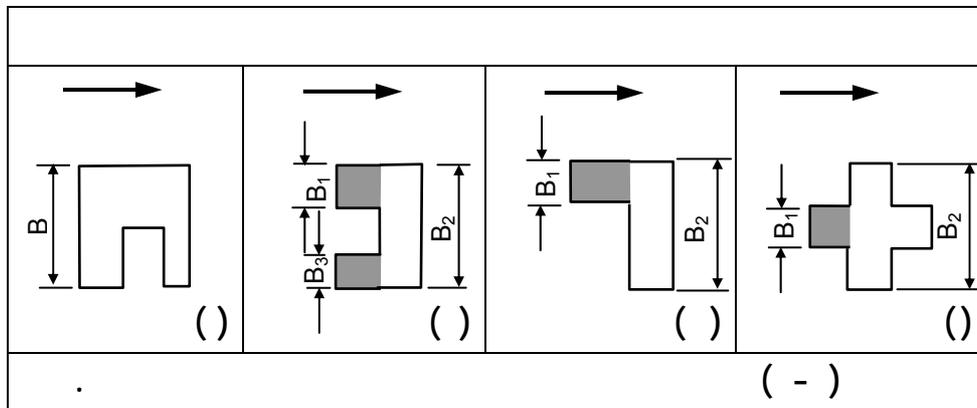
( ( ) ( ) ( ) )

(H) (B<sub>3</sub>) (B<sub>1</sub>) (B)

\*

(H) (B<sub>2</sub>) (B)

\*



) ( )

( ) ( )

:{ ( - ) } (b)

(C<sub>pe</sub>)

\*

.( / / )

(C<sub>pe</sub>)

\*

(C<sub>pe</sub>)

( ) ( ) ( )  
 {( - ) } (b)  
 ( / / / ) (C<sub>pe</sub>)

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: ( )

: ( )

)

( - ) .(

( - ) (C<sub>pe</sub>)  
 : ( )

: ( ) \*

(C) (B) (A)

.( - )

(H) ( ) (b)

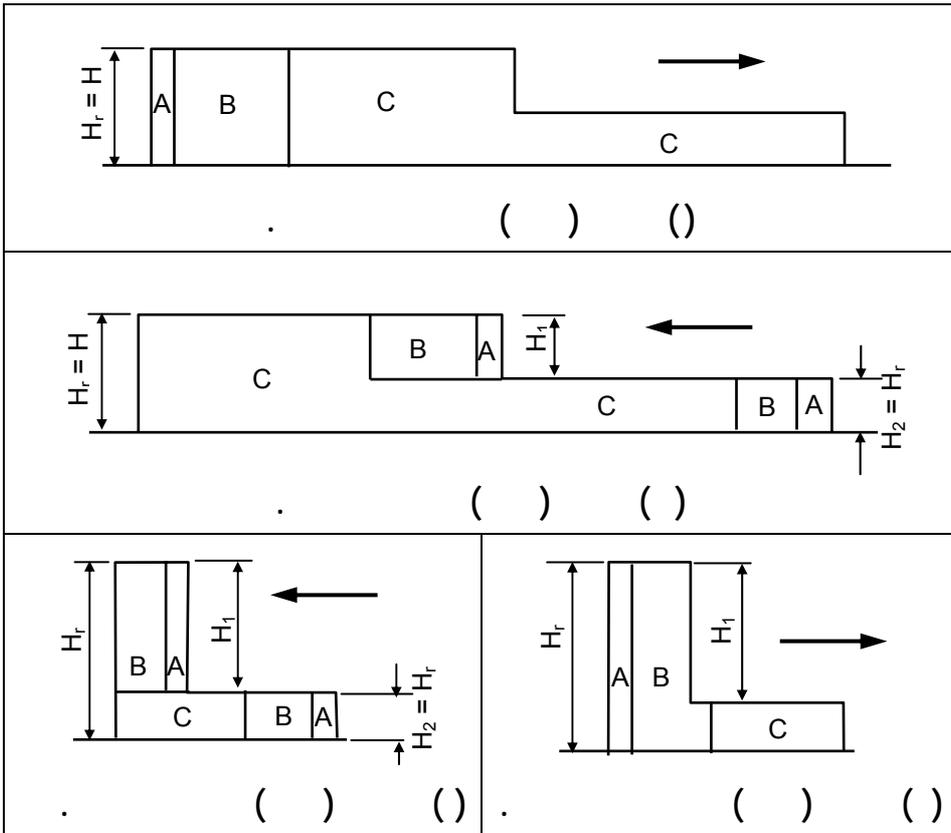
.(B)

: ( ) \*

(C) (B) (A)

.( - )

(B) (H) (b)  
 .(B<sub>2</sub>·H<sub>2</sub>) (B<sub>1</sub>·H<sub>1</sub>) ( )  
 ( ) (H<sub>r</sub>)  
 .( - )  
 .( // )



( - )

(0.2b<sub>1</sub>)

( - )

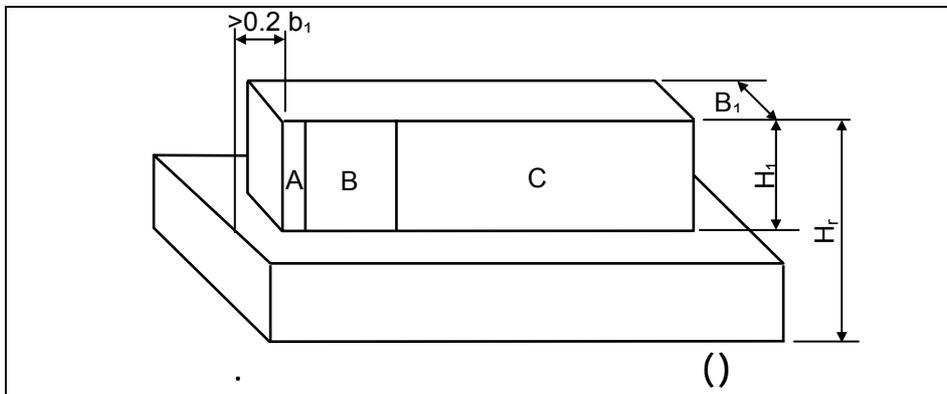
\*

(b<sub>1</sub>)

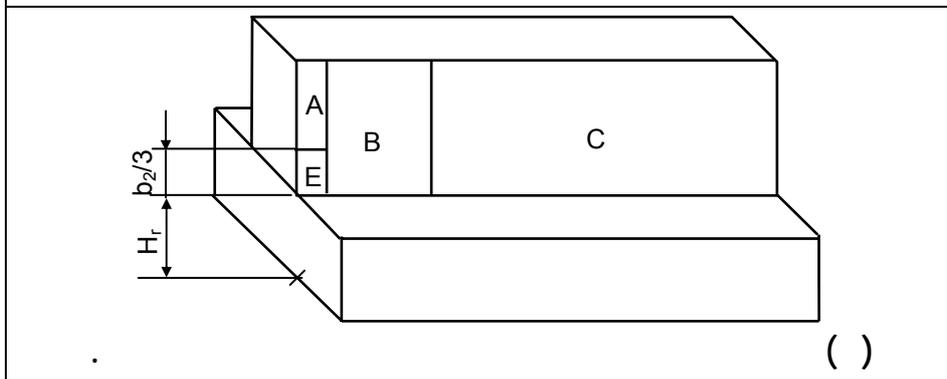
( - )

(C) (B) (A)

(C<sub>pe</sub>)



( )



( )

( - )

(0.2b<sub>1</sub>)

( - )

\*

( - )

(C) (B) (A)

(C<sub>pe</sub>)

(E)

(E)

(H<sub>r</sub>)

-

(A) (E) -  
 (b<sub>2</sub>)  $\left(\frac{b_2}{3}\right)$

(A) -

(E) (2.0 - = C<sub>pe</sub>)

(E) : ( )

( ) ( )

(C<sub>f</sub>) (b < D)

( ) ( - ) (C)  
 ( / / )

(C <sub>f</sub> )	:( - )
0.01	
0.02	
0.04	

: ( ) ( )

(C<sub>pe</sub>) ( - )  
 (°0 = θ) ( )

(°180 = θ)

(0 = C<sub>pe</sub>) (°40 = θ)

(0.7 ± = C<sub>pe</sub>)

: (C<sub>pe</sub>) / /

: ( )

: ( )

(°5)

$(45 \pm \theta)$  ( )

.( - ) ( / / ) ( )

$(C_{pe})$				$:( - )$
$2.5 \geq \frac{H}{d}$	$10 \leq \frac{H}{d}$	$2.5 \geq \frac{H}{d}$	$10 \leq \frac{H}{d}$	$(\theta)$
1.0 +	1.00 +	1.0 +	1.0 +	° 0
0.9 +	0.90 +	0.9+	0.9+	° 10
0.7 +	0.70 +	0.7+	0.7+	° 20
0.35+	0.35 +	0.4+	0.4+	° 30
0	0	0	0	° 40
0.50 -	0.70 -	0.4 -	0.5 -	° 50
1.05 -	1.20 -	0.8 -	0.95 -	° 60
1.25 -	1.40 -	1.10 -	1.25 -	° 70
1.30 -	1.45 -	1.05 -	1.20 -	° 80
1.20 -	1.40 -	0.85 -	1.00 -	° 90
0.85 -	1.10 -	0.65 -	0.80 -	° 100
0.40 -	0.60 -	0.35 -	0.50 -	° 120
0.25 -	0.35 -	0.30 -	0.40 -	° 140
0.25 -	0.35 -	0.30 -	0.40 -	° 160
0.25 -	0.35 -	0.30 -	0.40 -	° 180

: ( )

$(2H=b)$   $(B=b)$  (b) ( - )

(L) (W) (B)

.( ) ( ) (H)

:( ) ( )

( - )

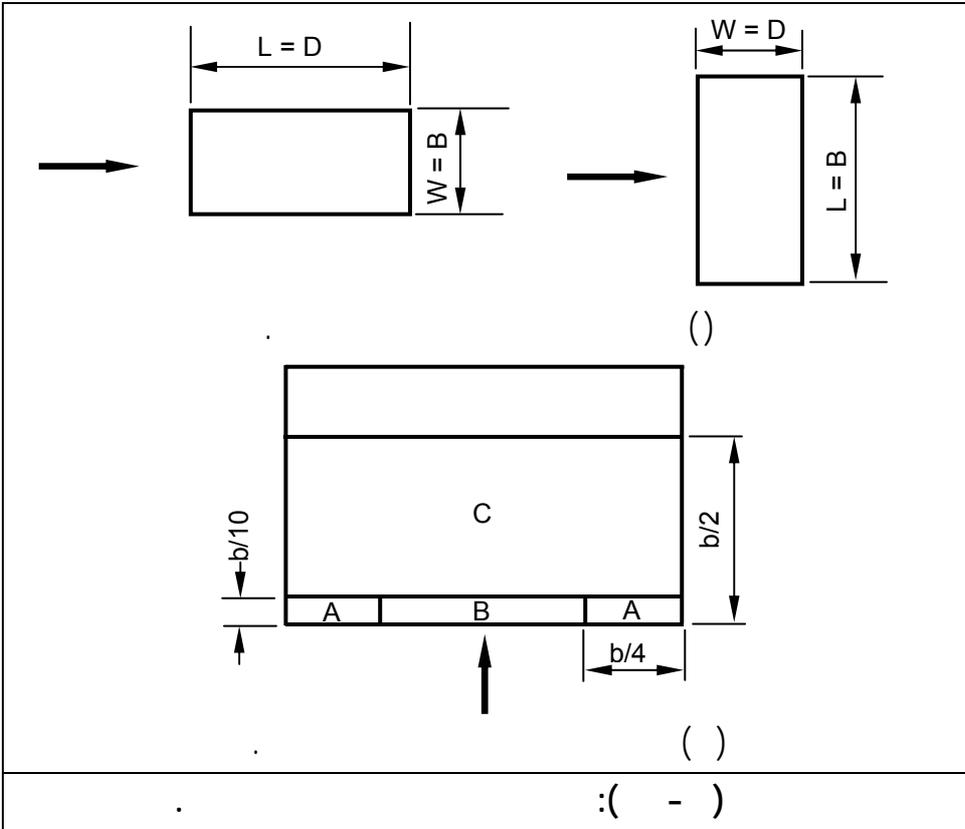
$(C_{pe})$

.( - )

( )

( / / )

.( / / )



(C <sub>pe</sub> )				:( - )	
D	C	B	A		
0.2 ±	0.7 -	1.4 -	2.0 -		
0.2 ±	0.7 -	1.25 -	1.8 -	$0.05 = \frac{h}{b}$	<b>Eave with Parapet</b>
0.2 ±	0.7 -	1.2 -	1.75 -	$0.10 = \frac{h}{b}$	
0.2 ±	0.7 -	1.0 -	1.4 -	$0.20 \leq \frac{h}{b}$	
0.2 ±	0.4 -	1.2 -	1.0 -	$0.05 = \frac{r}{b}$	<b>Curved Eave</b>
0.2 ±	0.3 -	0.8 -	0.75 -	$0.10 = \frac{r}{b}$	
0.2 ±	0.3 -	0.55 -	0.55 -	$0.20 = \frac{r}{b}$	
0.2 ±	0.3 -	1.0 -	0.95 -	$30 = \alpha$	<b>Mansard Eave</b>
0.2 ±	0.4 -	1.3 -	1.2 -	$45 = \alpha$	
0.2 ±	0.6 -	1.25 -	1.3 -	$60 = \alpha$	

:

( )

(°30 =  $\alpha$ ) ( )

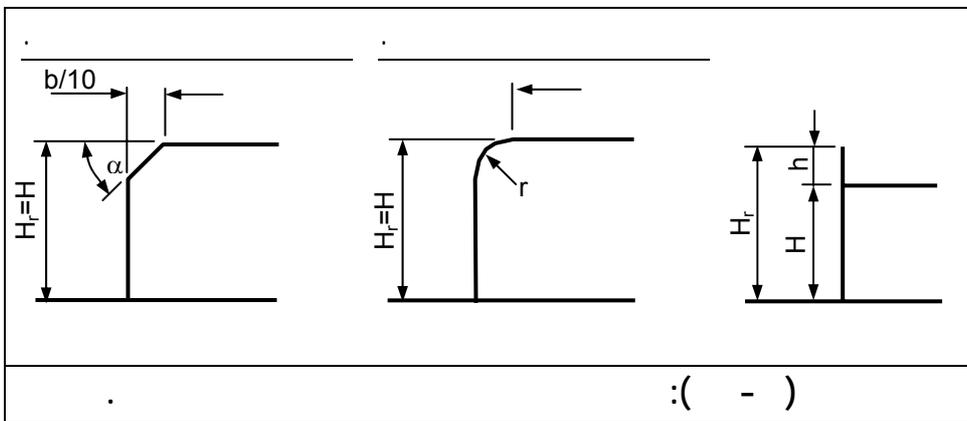
(°60 =  $\alpha$ ) (°60 =  $\alpha$ )

(°60 <  $\alpha$ )

(D) ( )

( / / ) ( )

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:

( )

( $C_{pe}$ )

( - )

\*

(H<sub>r</sub>) ( / / ) ( )

(H)

(b)

:

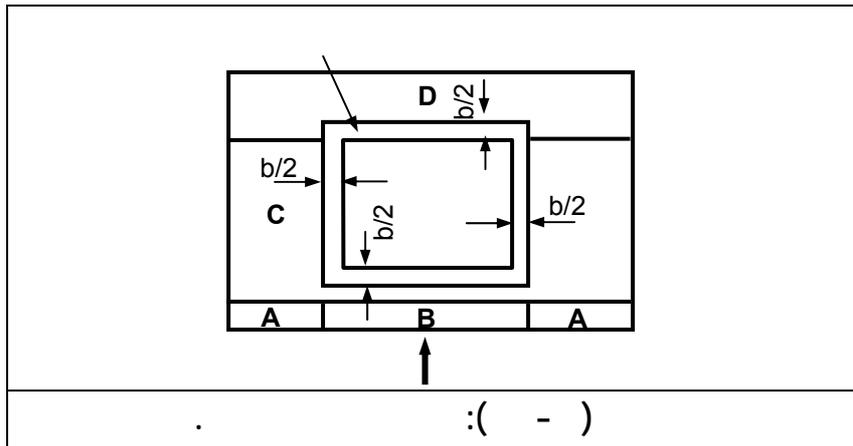
\*

(H<sub>r</sub>)

(b) (b/2)

(C<sub>pe</sub>)

.( / / )



:( - )

: ( )

: ( )

( )

( - ) ( - )

(2H W = b<sub>w</sub>)  
(H)

(2H L = b<sub>L</sub>) (b<sub>w</sub>) (b<sub>L</sub>)  
(L) (W)

: ( )

.( - )

(C<sub>pe</sub>)

(° = θ)

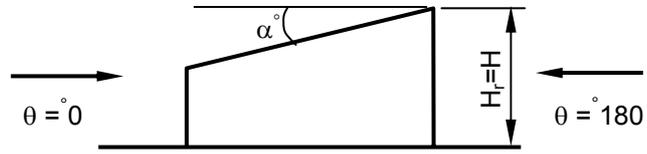
( )

( )

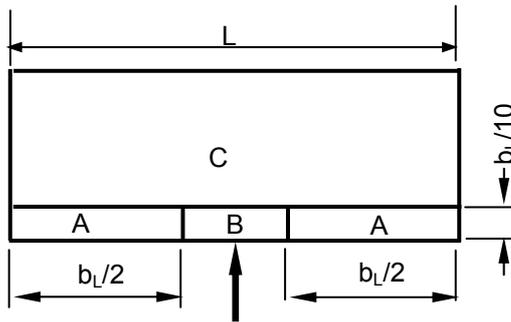
(°90 = θ)

.( - )

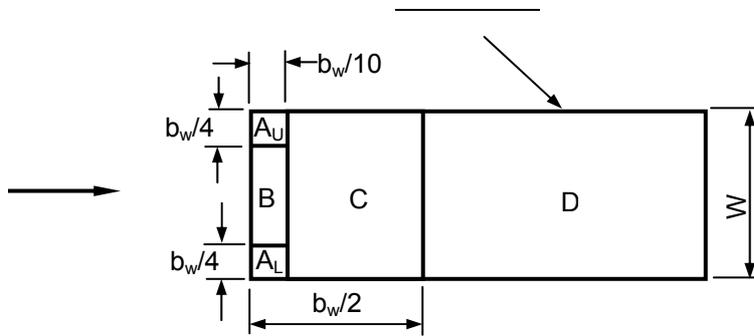
(°180 = θ)



( )



( $180 = \theta$ ) ( $0 = \theta$ ) ( )



( $90 = \theta$ ) ( )

:( - )

(C<sub>pe</sub>)

:( - )

° 180 = θ			° 90 = θ				° 0 = θ			(α)	
C	B	A	D	C	B	A <sub>L</sub>	A <sub>U</sub>	C	B	A	
0.8 -	1.2 -	2.3 -	0.5 -	0.6 -	1.7 -	2.1 -	2.2 -	0.6 -	1.2 -	1.8 -	° 5
0.9 -	1.0 -	2.6 -	0.7 -	0.8 -	1.6 -	1.6 -	2.8 -	0.3 -	0.8 -	1.3 -	° 15
								0.2 +	0.2 +	0.2 +	
0.8 -	1.2 -	2.3 -	0.8 -	1.0 -	1.2 -	1.3 -	1.7 -	0.2 -	0.5 -	1.1 -	° 30
								0.4 +	0.5 +	0.8 +	
0.8 -	1.0 -	1.3 -	0.9 -	1.0 -	1.2 -	1.3 -	1.5 -	0.7 +	0.3 -	1.1 -	° 45
									0.6 +	0.8 +	
0.7 -	0.7 -	1.0 -	0.4 -	0.4 -	1.2 -	1.2 -	1.2 -	0.8 +	0.8 +	0.8 +	° 60
				0.4 +							
0.7 -	0.7 -	1.1 -	0.2 -	0.4 -	1.2 -	1.2 -	1.2 -	0.8 +	0.8 +	0.8 +	° 75
			0.4 +	0.5 +							
:											
° 0 = θ											( )
° 30 > α > ° 15											
° 90 = θ											
° 75 > α > ° 60											( )
(α)											( )
.( )											( )

: ( )

.( - )

(C<sub>pe</sub>)

\*

(° 0 = θ)

( )

.(° 90 = θ)

.( - )

( - )

[5]

(5)

$(b_L > W) \quad (\gamma > \alpha)$

$(\theta = 0)$

\*

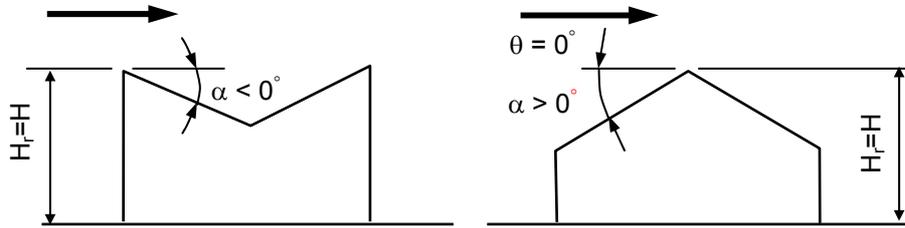
$\left(\frac{b_L}{2}\right) \quad (C)$

(G)

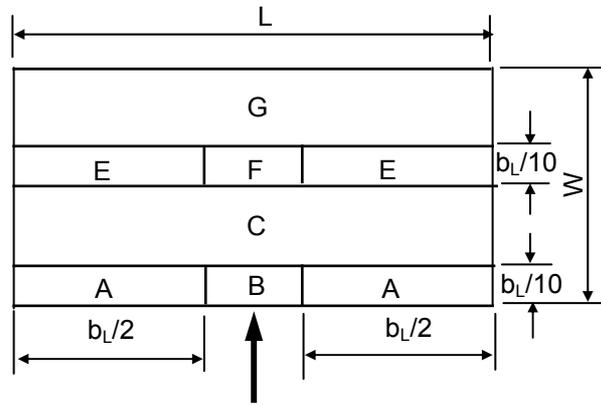
(F) (E)

$(C_{pe})$										$:( - )$
$(\theta = 90^\circ)$				$(\theta = 0^\circ)$						$(\alpha)$
D	C	B	A	G	F	E	C	B	A	
0.2 -	1.0 -	1.3 -	1.5 -	0.7 -	0.7 -	1.0 -	0.8 -	1.0 -	1.0 -	$45^\circ -$
0.2 -	1.0 -	1.3 -	1.7 -	0.7 -	0.7 -	0.9 -	0.8 -	1.2 -	1.2 -	$30^\circ -$
0.3 -	0.8 -	1.4 -	2.7 -	0.5 -	0.5 -	0.7 -	0.9 -	1.0 -	2.6 -	$15^\circ -$
0.4 -	0.7 -	1.5 -	2.2 -	0.3 -	0.3 -	0.3 -	0.8 -	1.2 -	2.3 -	$5^\circ -$
0.4 -	0.6 -	1.1 -	2.0 -	0.3 -	0.3 -	0.5 -	0.6 -	1.2 -	1.8 -	$5^\circ +$
0.3 -	0.6 -	1.5 -	1.6 -	0.5 -	0.9 -	1.1 -	0.3 -	0.8 -	1.3 -	$15^\circ +$
							0.2+	0.2+	0.2+	
0.2 -	0.6 -	1.1 -	1.2 -	0.4 -	0.4 -	0.7 -	0.2 -	0.5 -	1.1 -	$30^\circ +$
							0.4+	0.5+	0.8+	
0.2 -	0.6 -	1.2 -	1.2 -	0.3 -	0.3 -	0.4 -	0.7+	0.3 -	1.1 -	$45^\circ +$
								0.6+	0.8+	
0.2 -	0.7 -	1.2 -	1.2 -	0.3 -	0.7 -	0.7 -	0.8+	0.8+	0.8+	$60^\circ +$
0.2 -	0.7 -	1.2 -	1.2 -	0.3 -	0.7 -	0.7 -	0.8+	0.8+	0.8+	$75^\circ +$
:										
$(\theta = 0^\circ)$										$( )$
$(\alpha > 30^\circ > 15^\circ)$										
(a)									$( )$	

$(C_{pe})$									$:( - )$
$(\overset{\circ}{90} = \theta) \quad (\overset{\circ}{0} = \theta)$									$(\alpha)$
J	I	H	G	F	E	C	B	A	
0.2 -	0.8 -	0.8 -	0.7 -	0.7 -	0.7 -	0.8 -	0.6 -	1.3 -	$\overset{\circ}{45} -$
0.2 -	0.8 -	0.8 -	0.7 -	0.7 -	0.7 -	0.8 -	0.8 -	2.3 -	$\overset{\circ}{30} -$
0.3 -	0.6 -	0.6 -	0.5 -	0.5 -	0.5 -	0.9 -	1.0 -	2.6 -	$\overset{\circ}{15} -$
0.4 -	0.6 -	0.6 -	0.3 -	0.3 -	0.3 -	0.8 -	1.2 -	2.3 -	$\overset{\circ}{5} -$
0.4 -	0.6 -	1.2 -	0.3 -	0.6 -	0.6 -	0.6 -	1.2 -	1.8 -	$\overset{\circ}{5} +$
0.3 -	0.6 -	1.4 -	0.5 -	1.2 -	1.0 -	0.3 -	0.8 -	1.3 -	$\overset{\circ}{15} +$
						0.2+	0.2+	0.2+	
0.2 -	0.8 -	1.4 -	0.4 -	0.5 -	0.7 -	0.2 -	0.5 -	1.1 -	$\overset{\circ}{30} +$
						0.4+	0.5+	0.8+	
0.2 -	0.8 -	1.3 -	0.3 -	0.3 -	0.6 -	0.7+	0.3 -	1.1 -	$\overset{\circ}{45} +$
							0.6+	0.8+	
0.2 -	0.4 -	1.2 -	0.3 -	0.3 -	0.6 -	0.8+	0.8+	0.8+	$\overset{\circ}{60} +$
0.2 -	0.4 -	1.2 -	0.3 -	0.3 -	0.6 -	0.8+	0.8+	0.8+	$\overset{\circ}{75} +$
:									
$(\overset{\circ}{0} = \theta)$									$( )$
$(\overset{\circ}{30} + > \alpha > \overset{\circ}{15} +)$									
$(\alpha)$									$( )$

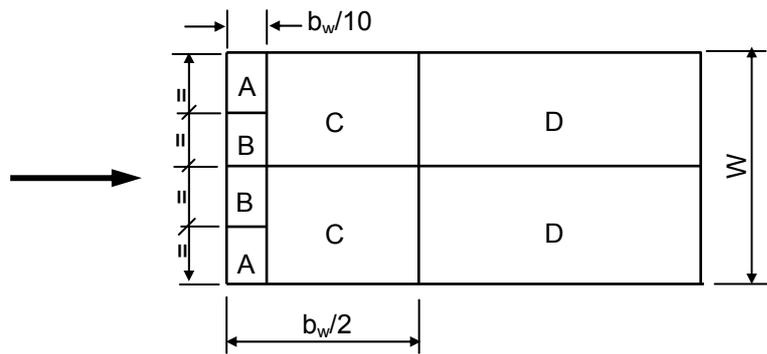


( )



( $0 = \theta$ )

( )



( $90 = \theta$ )

( )

:( - )

: ( )

( - )  
( - )

(  
.(°75 + ← α → - °45)

( )

.( - )

[5]

(Skewed)

:( ) ( )

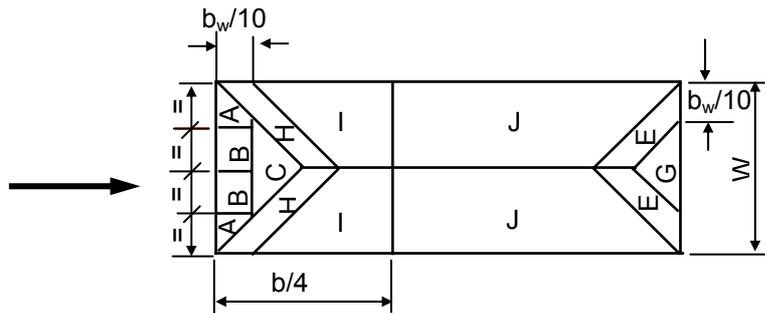
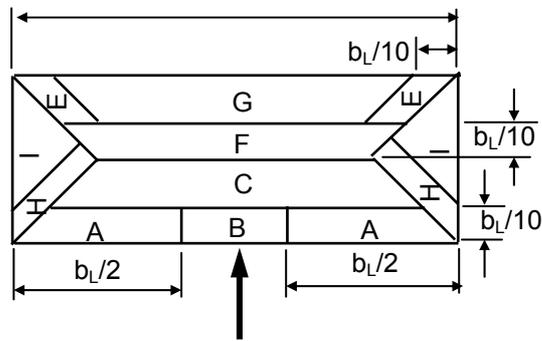
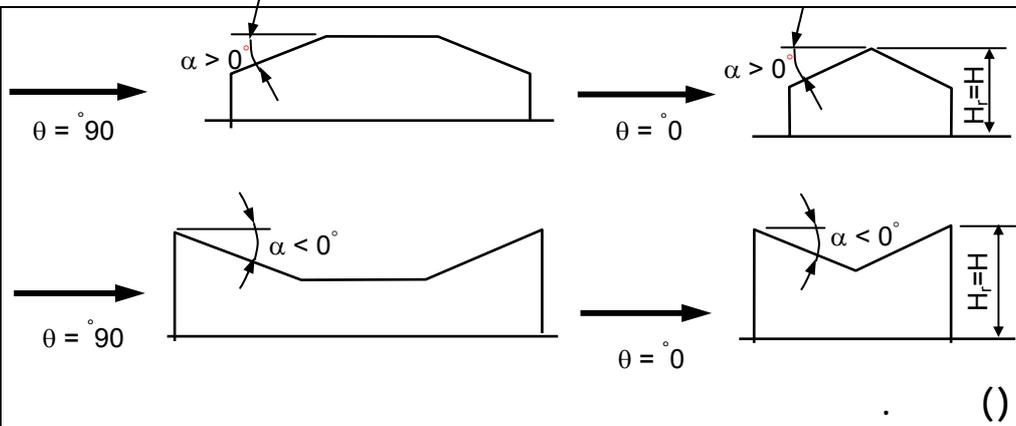
( )

( // )

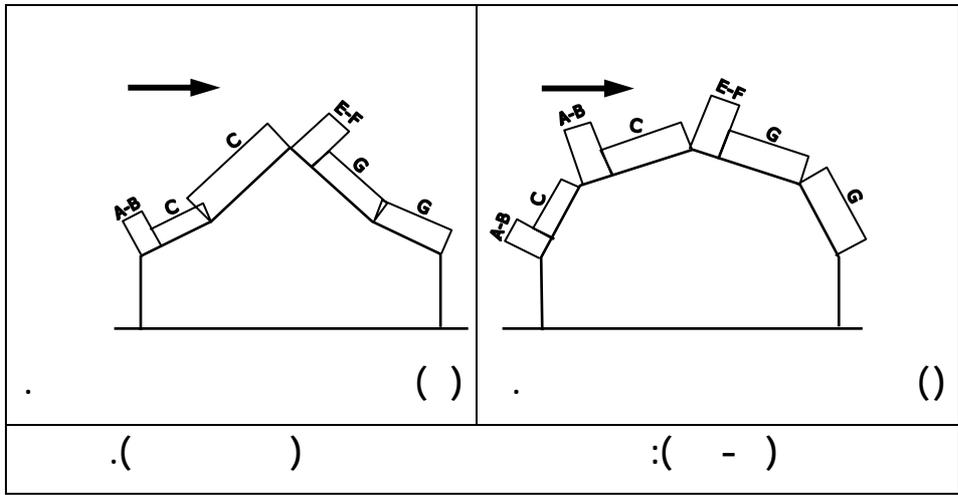
( )

( // )

.( - )



: ( - )



.( )

:( - )

: (Δ)

( - ) ( - ) (C<sub>pe</sub>)  
 ( - )

:

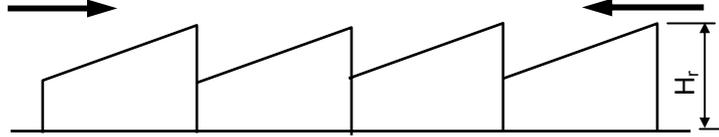
( - ) \*  
 ( - )

.(0.4 - = C<sub>pe</sub>) \*

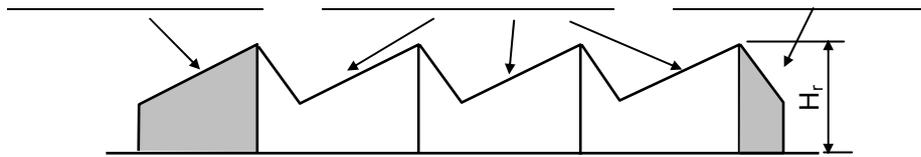
( - ) ( )

.(10) (α)

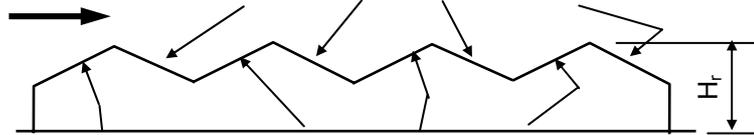
$0^\circ = \theta$



( )



( )



( )



( )

:( - )

$$( \quad - ) ( \quad - )$$

\*

:

$$(0.6) \quad :(\overset{\circ}{180} = \theta) \quad (\overset{\circ}{0} = \theta)$$

(0.8)

: ( )

( // )

.( $\Delta$  // ) ( // )

: ( )

( )

( $\overset{\circ}{30} > \alpha$ )

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( // // )

: ( )

$\left(\frac{b}{10} \leq\right)$  ( )

( // )

.( $\Delta$  // ) ( // )

( // )

: ( ) ( )

: ( )

( - )

( $C_p$ )

\*

$(C_p)$   $( - ) ( - )$   
 $( )$   $( )$   
 $(C_p)$  \*  
 $(\zeta)$   $( )$   
 $(h_1)$   $(h_2)$   
 $(0 = \zeta)$   $(1 = \zeta)$   
 $(0 = \zeta)$   $(1 = \zeta)$   
 $(1 = \zeta)$   
 $(0 = \zeta)$  \*  
 $( )$  \*  
 $(0.3 W)$   
 $( )$   $(Fascia)$   $( )$  \*  
 $( )$   $( )$   
 $(1.3+ = C_p)$   $(0.6 - = C_p)$   
 $( )$

$(C_p)$ : ( - )						
<b>C</b>	<b>B</b>	<b>A</b>		( $\zeta$ )	(+) (-)	( $\alpha$ )
1.1+ 1.4 - 2.2 -	1.8+ 1.3 - 1.8 -	0.5+ 0.6 - 1.3 -	0.2+ 0.5 - 1.2 -	( $\zeta$ ) (0 = $\zeta$ ) (1 = $\zeta$ )		$^{\circ}0$
1.3+ 1.8 - (2.1 -) 2.6 -	2.1+ 1.7 - 2.6 -	0.8+ 1.1 - (1.2 -) 1.4 -	0.4+ 0.7 - (1.2 -) 1.4 -	( $\zeta$ ) 0 = $\zeta$ 1 = $\zeta$		$^{\circ}5$
1.6+ 2.1 - (1.8 -) 2.7 -	2.4+ 2.0 - 2.6 -	1.2 + 1.5 - (1.1 -) 1.4 -	0.5+ 0.9 - (1.1 -) 1.4 -	$\zeta$ 0 = $\zeta$ 1 = $\zeta$		$^{\circ}10$
1.8+ 2.5 - (1.6 -) 2.8 -	2.7+ 2.4 - 2.9 -	1.4+ 1.8 - (1.0 -) 1.5 -	0.7+ 1.1 - (1.0 -) 1.5 -	$\zeta$ 0 = $\zeta$ 1 = $\zeta$		$^{\circ}15$
2.1+ 2.9 - (1.5 -) 2.7 -	2.9+ 2.8 - 2.9 -	1.7+ 2.2 - (0.9 -) 1.5 -	0.8+ 1.3 - (0.9 -) 1.5 -	$\zeta$ 0 = $\zeta$ 1 = $\zeta$		$^{\circ}20$
2.3+ 3.2 - (1.4 -) 2.5 -	3.1+ 3.2 - 2.5 -	2.0+ 2.6 - (0.8 -) 1.4 -	1.0+ 1.6 - (0.8 -) 1.4 -	$\zeta$ 0 = $\zeta$ 1 = $\zeta$		$^{\circ}25$
2.4+ 3.6 - (1.2 -) 2.3 -	3.2+ 3.8 - 2.0 -	2.2+ 3.0 - (0.8 -) 1.4 -	1.2+ 1.8 - (0.8 -) 1.4 -	$\zeta$ 0 = $\zeta$ 1 = $\zeta$		$^{\circ}30$
:						
.(1 > $\zeta$ > 0)						( )
						( )

: ( )

[5]

: ( )

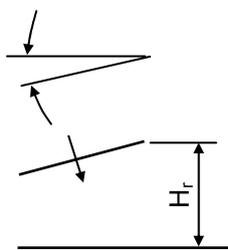
.( - )

: ( ) ( )

( / / ) ( / / )

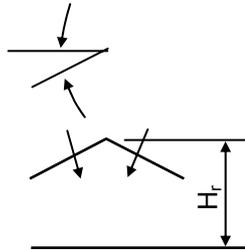
( / / )

(a)



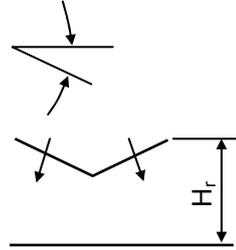
$C_p > 0$

(a)



$C_p > 0$

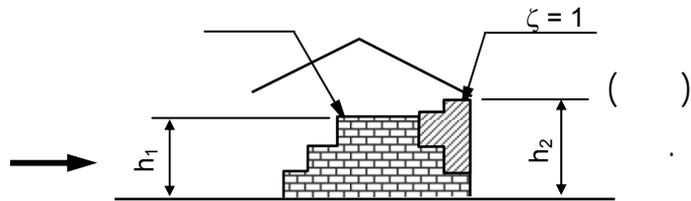
(a)



$C_p > 0$

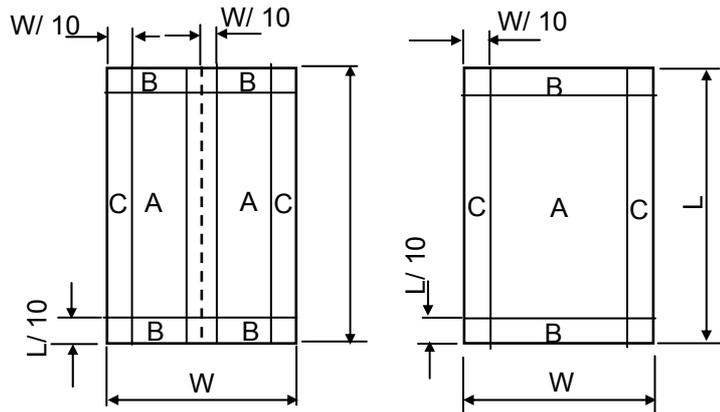
( )

$$\zeta = h_1 / h_2$$



/ ) ( / ) ( )

.....(



( )

.( ) :(- )

$(C_p)$					:( - )		
D	C	B	A		( $\zeta$ )	(+) (-)	( $\alpha$ )
1.7 +	0.6 +	1.6 +	0.8 +	0.7 +	( $\zeta$ )		°20 -
0.6 -	1.6 -	1.3 -	0.9 -	0.7 -	0 = $\zeta$		
1.2 -	2.4 -	2.4 -	1.5 -	1.5 -	1 = $\zeta$		
1.4 +	0.7 +	1.5 +	0.6 +	0.5 +	( $\zeta$ )		°15 -
0.6 -	1.6 -	1.3 -	0.8 -	0.6 -	0 = $\zeta$		
1.2 -	2.6 -	2.7 -	1.5 -	1.5 -	1 = $\zeta$		
1.1 +	0.8 +	1.4 +	0.6 +	0.4 +	( $\zeta$ )		°10 -
0.6 -	1.5 -	1.3 -	0.8 -	0.6 -	0 = $\zeta$		
1.2 -	2.5 -	2.5 -	1.4 -	1.4 -	1 = $\zeta$		
0.8 +	0.8 +	1.5 +	0.5 +	0.3 +	( $\zeta$ )		°5 -
0.6 -	1.6 -	1.3 -	0.7 -	0.5 -	0 = $\zeta$		
1.2 -	2.4 -	2.3 -	1.4 -	1.4 -	1 = $\zeta$		
0.4 +	1.3 +	1.8 +	0.6 +	0.3 +	( $\zeta$ )		°5 +
1.1 -	1.4 -	1.4 -	0.6 -	0.6 -	0 = $\zeta$		
1.5 -	1.8 -	2.0 -	1.2 -	1.2 -	1 = $\zeta$		
0.4 +	1.4 +	1.8 +	0.7 +	0.4 +	( $\zeta$ )		°10 +
1.4 -	1.4 -	1.5 -	0.7 -	0.7 -	0 = $\zeta$		
1.6 -	1.6 -	1.8 -	1.2 -	1.2 -	1 = $\zeta$		
0.4 +	1.4 +	1.9 +	0.9 +	0.4 +	( $\zeta$ )		°15 +
1.8 -	1.4 -	1.7 -	0.9 -	0.8 -	0 = $\zeta$		
1.7 -	1.3 -	1.6 -	1.2 -	1.2 -	1 = $\zeta$		
0.4 +	1.5 +	1.9 +	1.1 +	0.6 +	( $\zeta$ )		°20 +
2.0 -	1.4 -	1.8 -	1.2 -	0.9 -	0 = $\zeta$		
1.7 -	1.2 -	1.5 -	1.2 -	1.2 -	1 = $\zeta$		

(C <sub>p</sub> )					:( - )			
D	C	B	A		(ζ)	(+) (-)	(α)	
0.5 +	1.6 +	1.9 +	1.2 +	0.7 +	(ζ)		°25 +	
2.0 -	1.4 -	1.9 -	1.4 -	1.0 -	0 = ζ			
1.6 -	1.1 -	1.4 -	1.2 -	1.2 -	1 = ζ			
0.7 +	1.6 +	1.9 +	1.3 +	0.9 +	(ζ)		°30 +	
2.0 -	1.4 -	1.9 -	1.4 -	1.0 -	0 = ζ			
1.6 -	1.1 -	1.3 -	1.2 -	1.2 -	1 = ζ			
:(							( )	( )
.(1 > ζ > 0)							( )	( )

:( - )		
0 = ζ		
0.81	1.00	
0.64	0.87	
0.63	0.68	

:( )

:( )

( - )  
(J)

(D)  
(D)

( - ) ( - ) (°90 = θ)

.( - )  
( - )

.( // )

: ( )

(0 = ζ)

.(1 = ζ)

( - )

.( // )

: //

: ( )

( )

.( - ) (C<sub>pi</sub>)

: (a)

(4-14)

X 10 = a

( )

(5)

( )

( )

.(C<sub>p</sub>)

(0.2 - = C<sub>pi</sub>) (0.3 - = C<sub>pi</sub>)

.(0.5 = C<sub>p</sub>)

: (a)

(4-15)

X 10 = a

(C <sub>pi</sub> )	:( - )
(C <sub>pi</sub> )	( )
0.2 +	-
0.3 -	-
0.3 -	

( )

( )

: ( )

(a)

(C<sub>pi</sub>)

(C<sub>pe</sub>)

( - )

( / / ) ( / / )

(a)

(4-17) (4-16)

:

(4-16)

= a

(4-17)

× 0.2 = a

(C <sub>pi</sub> )		:( - )
(C <sub>pi</sub> )		
C <sub>pe</sub> X 0.75		2
C <sub>pe</sub> X 0.9		3

:

( )

(C<sub>pi</sub>)

( - )

( )

(a)

(° = θ)

( - )

( )

(°45 = θ)

(2.2 = C<sub>p</sub>)

[5]

(C <sub>pi</sub> ) : ( - )				
<b>5</b>	<b>4</b>	<b>3</b>	<b>2</b>	<b>1</b>
0.60 +	0.77 +	0.68 +	0.85 +	°0 = θ
0.00 -	0.38 - 0.77 +	0.40 -	0.60 -	°90 = θ
0.39 -	0.30 -	0.16 -	0.16 -	°180 = θ
:				
4 (°90 = θ) ( )				
. ( 5 ) ( )				
. ( - )				

: ( )

(C<sub>pi</sub>) ( - )  
( )

(C <sub>pi</sub> ) : ( - )	
(C <sub>pi</sub> )	$\frac{\text{الارتفاع}}{\text{القطر}}$
0.8 -	$0.3 \leq \frac{H}{d}$
0.5 -	$0.3 > \frac{H}{d}$

: //

()

.( (200) )

. (200)

:( ) ()

(C<sub>p</sub>) ( - ) ()

(C <sub>p</sub> )	:( - )
(C <sub>p</sub> )	
1.20	
2.00	

(H<sub>r</sub>) ()

(L)

(H<sub>r</sub>) (2B ≤ L)

: ()

( - )

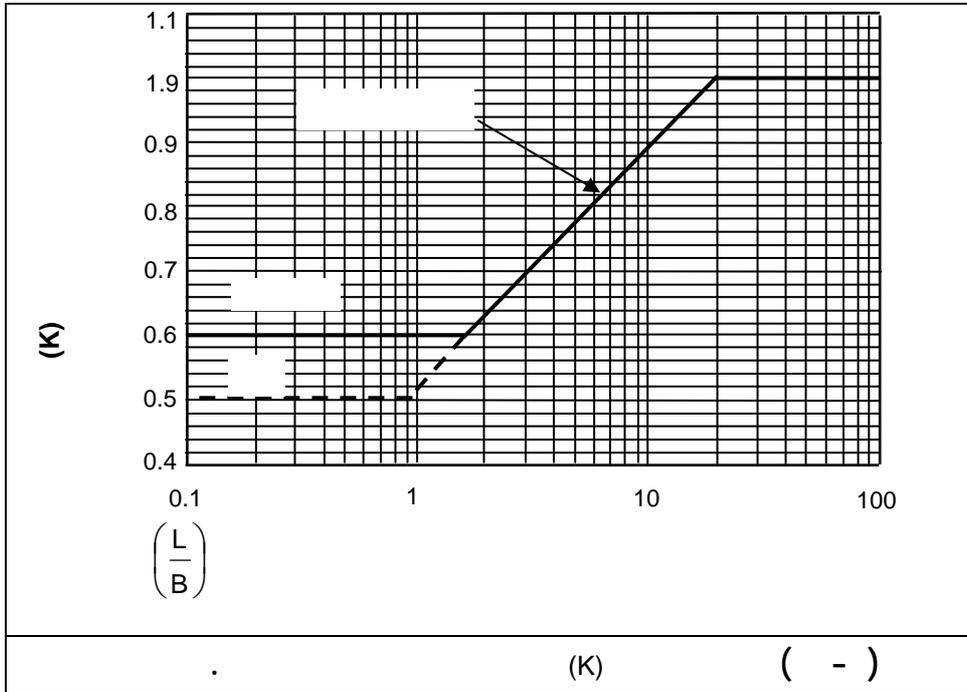
(L)

(2L)

( )

(1 = K)

(∞ = L)



:

( )

- - ( )

( )

//) ( //) ( //)

(L) .(

.( )

( )

[6] [5]

.(30 = 0)

: //

: ()

(C<sub>p</sub>) ( - ) ()

(0.8 = ζ)

(1.0 = ζ)

(20)

(80)

.( - )

(0.8 < ζ < 1)

(0.8 = ζ)

.( / / )

()

(h)

(C<sub>p</sub>)

( )

( - )

<b>(C<sub>p</sub>)</b>				<b>:( - )</b>	
<b>D</b>	<b>C</b>	<b>B</b>	<b>A</b>		
1.2	1.7	2.1	3.4		1 = ζ
1.2	1.4	1.8	2.1		
1.2	1.2	1.2	1.2		0.8 = ζ

: ()

( - )

$\left(\frac{h}{2} \leq\right)$

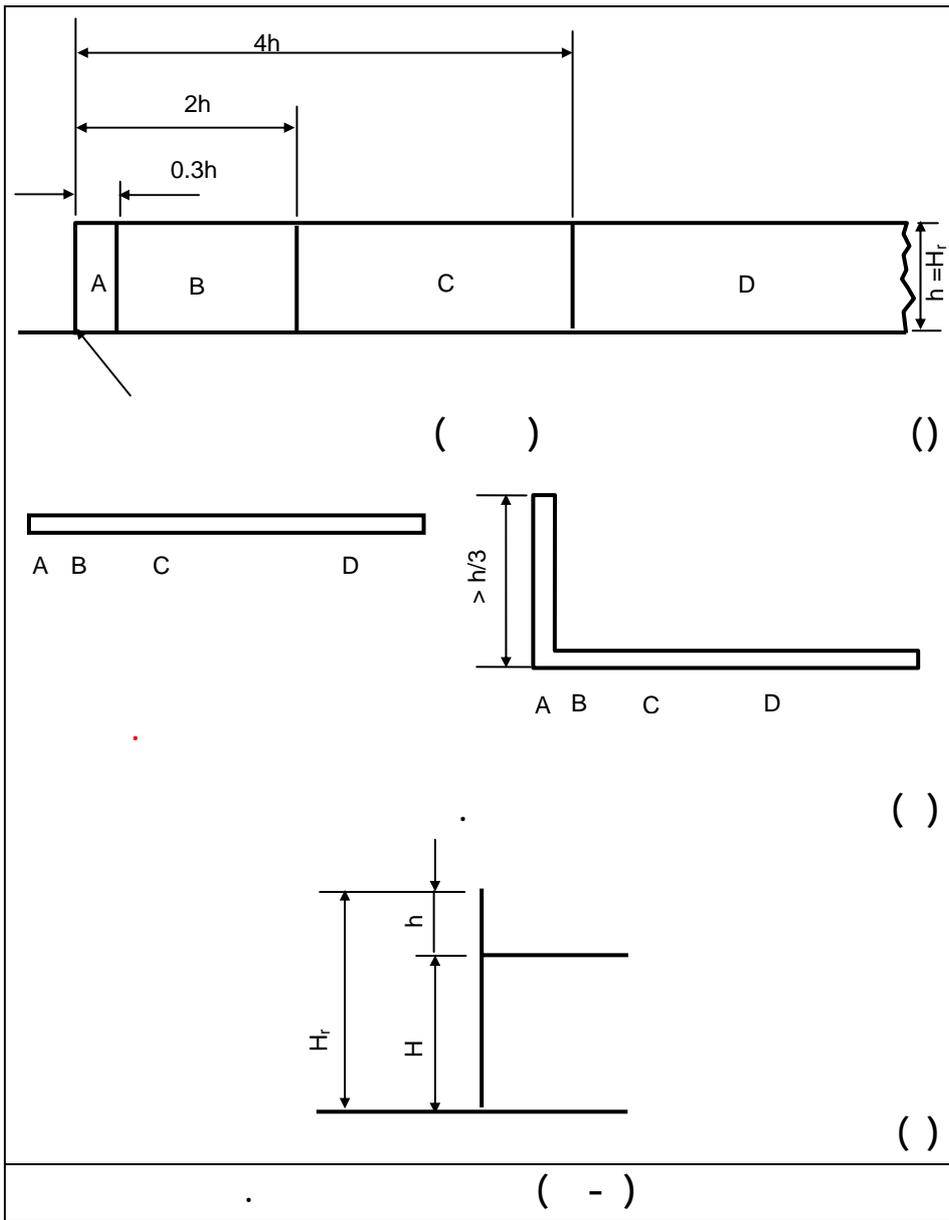
$$\left(\frac{h}{2}\right)$$

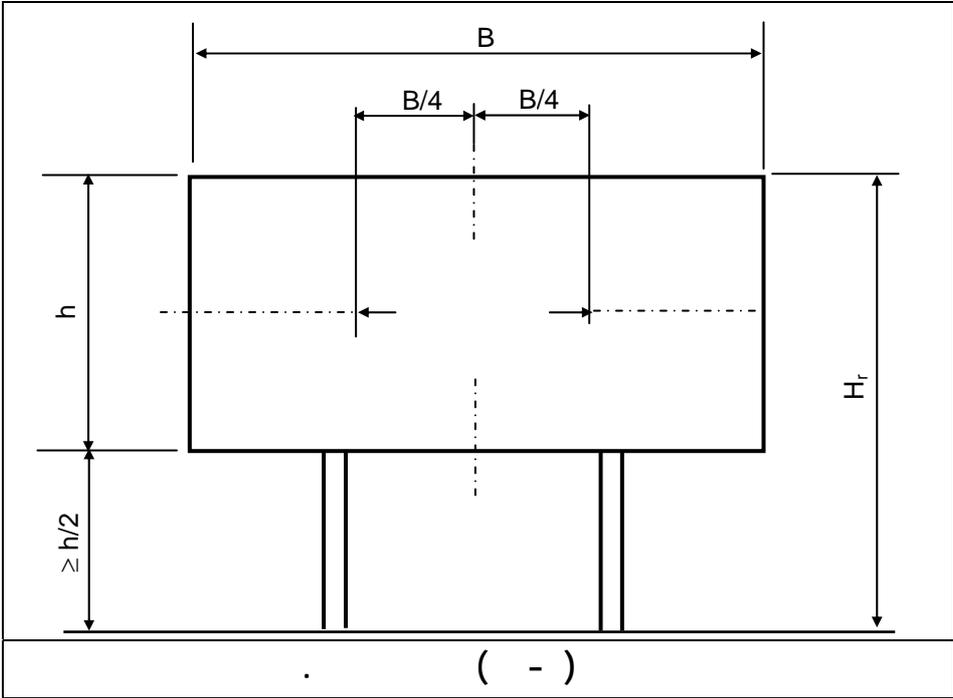
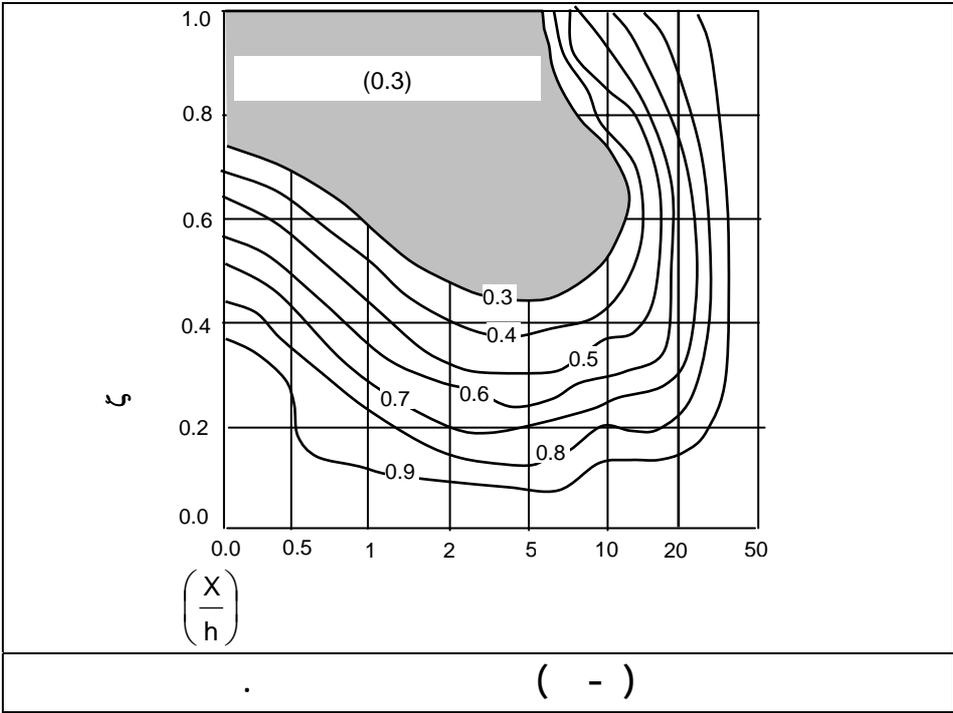
$$(1.8 = C_p)$$

.( / / )

$$(0.25B \pm)$$

.( - )





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(8.4)

(4.0)

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( )

**(Lightweight)**

/

(Public Spaces)

(Concourses)

(Dynamic Excitation)

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**(Snow Drift Load Calculation)**

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$(\rho h_{oi}/S_o)$

$\cdot \{ ( / (2) ) \}$

=  $\rho$

$\cdot ( )$

=  $h_{oi}$

$( / )$

=  $S_o$

/

$(2b_i/l_{si})$

$\cdot ( )$

=  $b_i$

$\cdot ( )$

=  $l_{si}$

(Arbitrarily)

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(Gumbel Cumulative Distribution Function (CDF))

(Probability)

(P)

(Q = 1 - P)

$\left(\frac{1}{Q}\right)$

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/ (5)

(V<sub>b</sub>)

(10)

(0.02 = Q)

(V<sub>s</sub>)

) (P)

(

(Method of Order Statistics)

(N = m)

(1 = m)

(m)

$$P(v_s) = \frac{m}{N+1}$$

(P)

(Fisher-Tippet Type 1)

(V)

(FT1)

(P)

(FT1)

(Extreme-value Theory)

(V<sub>s</sub>)

$$q = \frac{1}{2} \rho V_s^2$$

/

(1.226)

(ρ)

( ° 20)

(Isotach)

(0.02 = Q)

.( )

)

.(

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(S<sub>d</sub>)

( ° 30 ±)

(S<sub>d</sub>)

.(1.0 = S<sub>d</sub>)

/

(S<sub>s</sub>)

( )

.(1.0 = S<sub>s</sub>)

/

( / / )

(11)

(A)

(S)

.( - - Δ)                      (Hills & Ridges)                      (s)                      ( - Δ)

X/L <sub>D</sub>		X/L <sub>D</sub>				X/L <sub>U</sub>				X/L <sub>U</sub>										H/L <sub>e</sub>		
0.5	0.4	0.3	0.2	0.1	0	-0.1	-0.2	-0.3	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	-1	-1.1	-1.2	-1.3	-1.4	-1.5	-1.5	H/L <sub>e</sub>
( - Δ)									0.303	0.235	0.182	0.141	0.110	0.085	0.066	0.051	0.040	0.031	0.024	0.018	0.100	
									0.292	0.227	0.176	0.137	0.107	0.083	0.064	0.050	0.039	0.030	0.024	0.018	0.126	
									0.278	0.217	0.169	0.132	0.103	0.080	0.063	0.049	0.038	0.030	0.023	0.018	0.158	
									0.262	0.205	0.160	0.125	0.098	0.077	0.060	0.047	0.037	0.029	0.023	0.018	0.200	
0.295	0.344	0.401	0.467	0.544	0.634	0.498	0.392	0.308	0.242	0.191	0.150	0.118	0.093	0.073	0.057	0.045	0.035	0.028	0.022	0.017	0.251	
0.270	0.313	0.363	0.420	0.487	0.564	0.446	0.353	0.279	0.220	0.174	0.138	0.109	0.086	0.068	0.054	0.043	0.034	0.027	0.021	0.017	0.316	
0.242	0.278	0.320	0.369	0.425	0.489	0.389	0.310	0.246	0.196	0.156	0.124	0.099	0.079	0.063	0.050	0.040	0.032	0.025	0.020	0.016	0.398	
0.212	0.242	0.276	0.316	0.360	0.412	0.330	0.265	0.213	0.170	0.137	0.110	0.088	0.071	0.057	0.045	0.036	0.029	0.023	0.019	0.015	0.501	
0.181	0.205	0.233	0.263	0.298	0.337	0.273	0.221	0.179	0.145	0.117	0.095	0.077	0.062	0.050	0.041	0.033	0.027	0.021	0.017	0.014	0.631	
0.152	0.171	0.192	0.215	0.241	0.270	0.221	0.180	0.147	0.120	0.098	0.080	0.065	0.053	0.044	0.036	0.029	0.024	0.019	0.016	0.013	0.794	
0.125	0.139	0.155	0.172	0.191	0.212	0.174	0.144	0.118	0.097	0.080	0.066	0.054	0.045	0.037	0.030	0.025	0.021	0.017	0.014	0.012	1.000	
0.098	0.108	0.119	0.131	0.144	0.159	0.132	0.109	0.090	0.075	0.062	0.052	0.043	0.035	0.029	0.024	0.020	0.017	0.014	0.011	0.010	1.259	
0.065	0.072	0.078	0.086	0.094	0.103	0.086	0.071	0.059	0.049	0.041	0.034	0.028	0.023	0.019	0.016	0.013	0.011	0.009	0.008	0.006	1.585	
0.041	0.045	0.050	0.054	0.060	0.066	0.054	0.045	0.37	0.030	0.025	0.020	0.017	0.014	0.011	0.009	0.008	0.006	0.005	0.004	0.004	1.995	

(s)                      ( - Δ)                      ( )

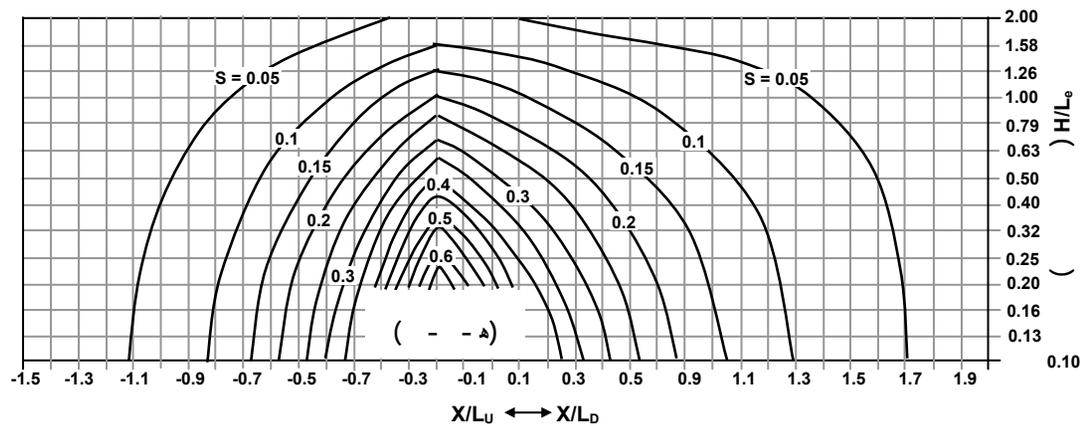
X/L <sub>D</sub>																			H/L <sub>e</sub>	
2.5	2.4	2.3	2.2	2.1	2	1.9	1.8	1.7	1.6	1.5	1.4	1.3	1.2	1.1	1	0.9	0.8	0.7	0.6	H/L <sub>e</sub>
0.013	0.015	0.018	0.022	0.025	0.030	0.035	0.042	0.049	0.058	0.069	0.082	0.096	0.114	0.134	0.159	0.187	0.221	0.261	0.309	0.100
0.013	0.016	0.018	0.022	0.026	0.030	0.035	0.042	0.049	0.058	0.068	0.80	0.095	0.112	0.132	0.155	0.183	0.215	0.253	0.299	0.126
0.013	0.016	0.019	0.022	0.026	0.030	0.035	0.041	0.049	0.057	0.067	0.079	0.093	0.109	0.128	0.150	0.177	0.207	0.244	0.286	0.158
0.014	0.016	0.019	0.022	0.026	0.030	0.035	0.041	0.048	0.056	0.066	0.077	0.090	0.106	0.124	0.145	0.169	0.198	0.232	0.271	0.200
0.014	0.016	0.019	0.022	0.026	0.030	0.035	0.041	0.047	0.055	0.064	0.075	0.087	0.101	0.118	0.138	0.160	0.187	0.218	0.254	0.251
0.014	0.016	0.019	0.022	0.026	0.030	0.034	0.040	0.046	0.054	0.062	0.072	0.083	0.096	0.112	0.129	0.150	0.174	0.201	0.233	0.316
0.015	0.017	0.019	0.022	0.026	0.029	0.034	0.039	0.045	0.052	0.059	0.068	0.079	0.090	0.104	0.120	0.138	0.159	0.183	0.210	0.398
0.015	0.017	0.019	0.022	0.025	0.029	0.033	0.038	0.043	0.049	0.056	0.064	0.073	0.084	0.095	0.109	0.125	0.142	0.162	0.186	0.501
0.015	0.017	0.019	0.022	0.025	0.028	0.032	0.036	0.041	0.046	0.052	0.059	0.067	0.076	0.086	0.098	0.110	0.125	0.142	0.160	0.631
0.015	0.017	0.019	0.022	0.024	0.027	0.031	0.034	0.039	0.043	0.048	0.054	0.061	0.068	0.077	0.086	0.096	0.108	0.121	0.136	0.794
0.015	0.017	0.019	0.021	0.023	0.026	0.029	0.032	0.036	0.040	0.427	0.049	0.054	0.060	0.067	0.074	0.083	0.092	0.102	0.113	1.000
0.014	0.016	0.017	0.019	0.021	0.023	0.026	0.028	0.031	0.034	0.037	0.041	0.045	0.050	0.055	0.061	0.067	0.074	0.081	0.089	1.259
0.011	0.012	0.013	0.014	0.015	0.017	0.018	0.020	0.022	0.024	0.026	0.029	0.031	0.034	0.038	0.041	0.045	0.050	0.054	0.060	1.585
0.006	0.007	0.008	0.008	0.009	0.010	0.011	0.012	0.013	0.015	0.016	0.018	0.019	0.021	0.023	0.026	0.028	0.031	0.034	0.037	1.995

.( - - Δ) (s) ( - Δ)

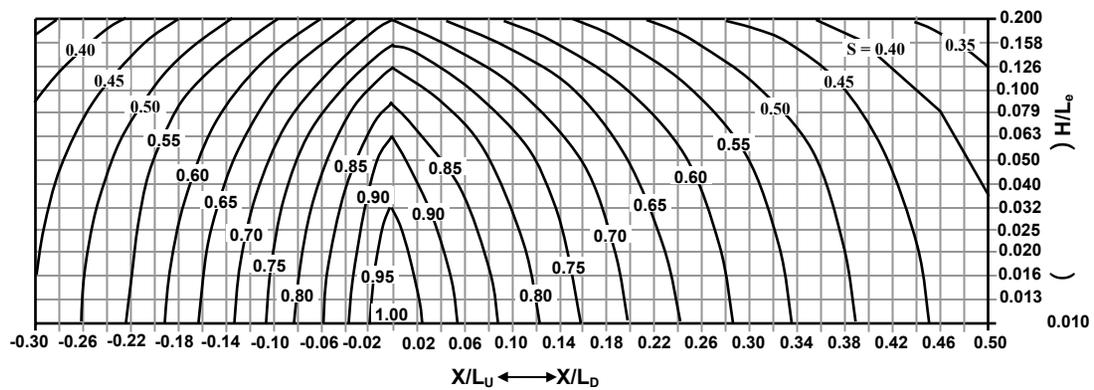
X/L <sub>D</sub>	X/L <sub>D</sub>				X/L <sub>u</sub>				X/L <sub>u</sub>								H/L <sub>e</sub>				
0.1	0.08	0.06	0.04	0.02	0	-0.02	-0.04	-0.06	-0.08	-0.1	-0.12	-0.14	-0.16	-0.18	-0.2	-0.22	0.24	-0.26	-0.28	-0.3	
0.834	0.863	0.894	0.926	0.959	0.993	0.942	0.894	0.848	0.805	0.763	0.724	0.687	0.652	0.618	0.587	0.556	0.528	0.501	0.475	0.451	0.010
0.830	0.859	0.890	0.922	0.955	0.989	0.938	0.890	0.844	0.801	0.760	0.721	0.684	0.649	0.616	0.584	0.554	0.526	0.499	0.473	0.449	0.013
0.825	0.854	0.885	0.916	0.949	0.983	0.932	0.884	0.839	0.796	0.755	0.717	0.680	0.645	0.612	0.581	0.551	0.523	0.496	0.471	0.447	0.016
0.819	0.848	0.878	0.909	0.942	0.975	0.925	0.878	0.833	0.790	0.750	0.712	0.675	0.641	0.608	0.577	0.547	0.519	0.493	0.468	0.444	0.020
0.811	0.840	0.870	0.901	0.933	0.966	0.916	0.869	0.825	0.783	0.743	0.705	0.669	0.635	0.603	0.572	0.543	0.515	0.489	0.464	0.440	0.025
0.802	0.830	0.860	0.890	0.921	0.954	0.905	0.859	0.815	0.774	0.734	0.697	0.662	0.628	0.596	0.566	0.537	0.509	0.484	0.459	0.436	0.032
0.790	0.818	0.847	0.877	0.907	0.939	0.891	0.846	0.803	0.763	0.724	0.687	0.652	0.619	0.588	0.558	0.530	0.503	0.477	0.453	0.430	0.040
0.776	0.803	0.831	0.860	0.890	0.921	0.874	0.830	0.788	0.748	0.711	0.675	0.641	0.608	0.577	0.548	0.521	0.494	0.469	0.446	0.423	0.050
0.758	0.784	0.812	0.840	0.869	0.899	0.854	0.811	0.770	0.731	0.694	0.659	0.626	0.595	0.565	0.536	0.509	0.484	0.460	0.436	0.414	0.063
0.736	0.762	0.788	0.815	0.843	0.872	0.828	0.787	0.747	0.710	0.674	0.641	0.609	0.578	0.549	0.522	0.496	0.471	0.448	0.425	0.404	0.079
0.710	0.734	0.759	0.785	0.811	0.839	0.797	0.757	0.720	0.684	0.650	0.618	0.587	0.558	0.531	0.504	0.479	0.455	0.433	0.411	0.391	0.100
0.678	0.701	0.724	0.748	0.773	0.799	0.760	0.722	0.687	0.653	0.621	0.591	0.562	0.534	0.508	0.483	0.459	0.437	0.415	0.395	0.375	0.126
0.640	0.661	0.682	0.705	0.728	0.752	0.715	0.681	0.647	0.616	0.586	0.558	0.531	0.505	0.480	0.457	0.435	0.414	0.394	0.375	0.356	0.158
0.595	0.614	0.634	0.654	0.675	0.697	0.663	0.632	0.601	0.573	0.545	0.519	0.494	0.471	0.448	0.427	0.406	0.387	0.369	0.351	0.334	0.200

(s) ( - Δ) ( )

X/L <sub>D</sub>	X/L <sub>D</sub>																		H/L <sub>e</sub>	
0.5	0.48	0.46	0.44	0.42	0.4	0.38	0.36	0.34	0.32	0.3	0.28	0.26	0.24	0.22	0.2	0.18	0.16	0.14	0.12	
0.413	0.428	0.443	0.459	0.476	0.493	0.510	0.528	0.547	0.567	0.587	0.608	0.630	0.652	0.675	0.700	0.725	0.750	0.777	0.805	0.010
0.412	0.427	0.442	0.458	0.474	0.491	0.508	0.526	0.545	0.565	0.585	0.606	0.627	0.649	0.673	0.697	0.721	0.747	0.774	0.801	0.013
0.410	0.425	0.440	0.455	0.472	0.488	0.506	0.524	0.542	0.562	0.582	0.602	0.624	0.646	0.669	0.693	0.717	0.743	0.769	0.797	0.016
0.408	0.422	0.437	0.453	0.469	0.485	0.503	0.520	0.539	0.558	0.578	0.598	0.620	0.642	0.664	0.688	0.712	0.738	0.764	0.791	0.020
0.405	0.419	0.434	0.449	0.465	0.482	0.499	0.516	0.535	0.554	0.573	0.593	0.614	0.636	0.659	0.682	0.706	0.731	0.757	0.784	0.025
0.401	0.415	0.430	0.445	0.461	0.477	0.494	0.511	0.529	0.548	0.567	0.587	0.608	0.629	0.652	0.675	0.698	0.723	0.748	0.775	0.032
0.397	0.411	0.425	0.440	0.455	0.471	0.488	0.505	0.523	0.541	0.560	0.580	0.600	0.621	0.643	0.665	0.689	0.713	0.738	0.764	0.040
0.391	0.405	0.419	0.433	0.449	0.464	0.480	0.497	0.514	0.532	0.551	0.570	0.590	0.611	0.632	0.654	0.677	0.700	0.725	0.750	0.050
0.384	0.397	0.411	0.425	0.440	0.455	0.471	0.487	0.504	0.522	0.540	0.558	0.578	0.598	0.618	0.640	0.662	0.685	0.708	0.733	0.063
0.375	0.388	0.402	0.415	0.430	0.444	0.460	0.475	0.492	0.508	0.526	0.544	0.562	0.582	0.602	0.622	0.644	0.666	0.688	0.712	0.079
0.365	0.377	0.390	0.403	0.417	0.431	0.445	0.461	0.476	0.492	0.509	0.526	0.544	0.562	0.581	0.601	0.621	0.642	0.664	0.687	0.100
0.352	0.364	0.376	0.388	0.401	0.415	0.428	0.443	0.457	0.473	0.488	0.505	0.522	0.539	0.557	0.575	0.595	0.614	0.635	0.656	0.126
0.336	0.347	0.358	0.370	0.382	0.395	0.408	0.421	0.435	0.449	0.464	0.479	0.495	0.511	0.528	0.545	0.563	0.581	0.600	0.620	0.158
0.317	0.328	0.338	0.349	0.360	0.371	0.383	0.396	0.408	0.421	0.435	0.449	0.463	0.478	0.493	0.509	0.525	0.542	0.559	0.577	0.200



(s) : ( - - Δ )



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X/L <sub>e</sub>																X/L <sub>e</sub>					H/L <sub>e</sub>	
2.1	2	1.9	1.8	1.7	1.6	1.5	1.4	1.3	1.2	1.1	1	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.2	0.1	0	
0.185	0.196	0.208	0.221	0.234	0.248	0.263	0.278	0.295	0.314	0.333	0.355	0.379	0.405	0.435	0.470	( - Δ)					0.100	
0.231	0.245	0.260	0.276	0.293	0.310	0.328	0.347	0.367	0.388	0.411	0.435	0.461	0.489	0.519	0.553						0.126	
0.259	0.276	0.293	0.310	0.328	0.347	0.367	0.387	0.409	0.431	0.455	0.480	0.506	0.534	0.564	0.597						0.158	
0.273	0.290	0.307	0.325	0.343	0.362	0.382	0.403	0.424	0.447	0.470	0.494	0.520	0.547	0.575	0.605						0.200	
0.273	0.290	0.306	0.323	0.341	0.359	0.378	0.398	0.418	0.439	0.461	0.484	0.508	0.533	0.558	0.585						0.251	
0.263	0.278	0.293	0.308	0.324	0.341	0.358	0.376	0.394	0.413	0.433	0.453	0.474	0.496	0.519	0.542						0.316	
0.243	0.256	0.269	0.283	0.296	0.311	0.325	0.340	0.356	0.372	0.389	0.407	0.424	0.443	0.462	0.481						0.398	
0.217	0.227	0.238	0.249	0.260	0.271	0.283	0.296	0.308	0.322	0.335	0.349	0.364	0.379	0.394	0.410	0.501						
0.185	0.193	0.201	0.209	0.218	0.227	0.236	0.245	0.255	0.265	0.275	0.286	0.297	0.308	0.320	0.332	0.344	0.335	0.364	0.366	0.342	0.337	0.631
0.151	0.156	0.162	0.168	0.174	0.180	0.186	0.193	0.200	0.207	0.214	0.221	0.229	0.237	0.246	0.254	0.263	0.271	0.278	0.281	0.266	0.270	0.794
0.115	0.119	0.122	0.126	0.130	0.134	0.138	0.142	0.146	0.151	0.156	0.161	0.166	0.171	0.177	0.182	0.188	0.194	0.199	0.203	0.197	0.212	1.000
0.081	0.083	0.085	0.087	0.089	0.092	0.094	0.097	0.099	0.102	0.105	0.108	0.111	0.115	0.118	0.122	0.126	0.130	0.134	0.138	0.138	0.159	1.259
0.049	0.051	0.052	0.054	0.055	0.057	0.059	0.061	0.063	0.065	0.067	0.069	0.072	0.074	0.077	0.079	0.082	0.085	0.088	0.091	0.091	0.103	1.585
0.023	0.025	0.027	0.029	0.031	0.033	0.036	0.038	0.040	0.043	0.046	0.048	0.051	0.054	0.057	0.060	0.063	0.065	0.067	0.067	0.060	0.066	1.995

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X/L <sub>e</sub>													X/L <sub>e</sub>		H/L <sub>e</sub>	
3.5	3.4	3.3	3.2	3.1	3	2.9	2.8	2.7	2.6	2.5	2.4	2.3	2.2			
0.065	0.072	0.079	0.087	0.094	0.102	0.110	0.118	0.126	0.135	0.144	0.154	0.164	0.174	0.174	0.100	
0.068	0.078	0.088	0.098	0.108	0.119	0.130	0.141	0.153	0.165	0.177	0.190	0.203	0.217	0.126		
0.073	0.084	0.096	0.108	0.120	0.132	0.145	0.158	0.171	0.185	0.199	0.213	0.228	0.244	0.158		
0.079	0.091	0.103	0.115	0.128	0.141	0.154	0.168	0.182	0.196	0.210	0.225	0.241	0.257	0.200		
0.085	0.096	0.108	0.120	0.133	0.146	0.158	0.172	0.185	0.199	0.213	0.228	0.242	0.258	0.251		
0.090	0.101	0.112	0.123	0.134	0.146	0.158	0.170	0.182	0.195	0.208	0.221	0.235	0.249	0.316		
0.094	0.103	0.113	0.122	0.132	0.142	0.152	0.163	0.174	0.185	0.196	0.207	0.219	0.231	0.398		
0.095	0.102	0.110	0.118	0.126	0.134	0.143	0.151	0.160	0.169	0.178	0.187	0.197	0.207	0.501		
0.093	0.098	0.104	0.110	0.116	0.123	0.129	0.135	0.142	0.149	0.156	0.163	0.170	0.178	0.631		
0.086	0.090	0.094	0.098	0.103	0.107	0.111	0.116	0.121	0.125	0.130	0.135	0.140	0.145	0.794		
0.074	0.077	0.079	0.082	0.085	0.087	0.090	0.093	0.096	0.099	0.102	0.105	0.108	0.112	1.000		
0.056	0.058	0.059	0.061	0.063	0.064	0.066	0.068	0.069	0.071	0.073	0.075	0.077	0.079	1.259		
0.032	0.033	0.034	0.035	0.036	0.037	0.038	0.040	0.041	0.042	0.043	0.045	0.046	0.048	1.585		
-0.001	0.000	0.002	0.003	0.005	0.007	0.008	0.010	0.012	0.013	0.015	0.017	0.019	0.021	1.995		

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( - ♣)

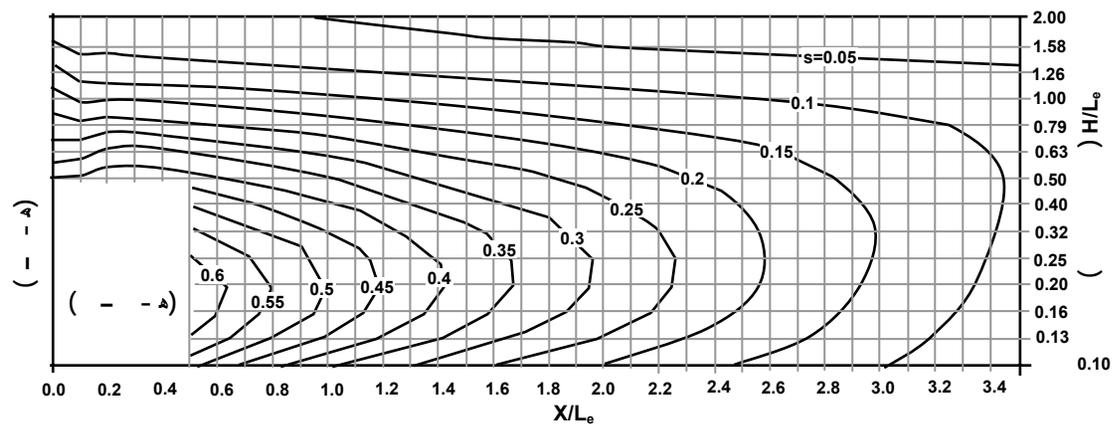
X/L <sub>e</sub>																					X/L <sub>e</sub>	H/L <sub>e</sub>
0.42	0.4	0.38	0.36	0.34	0.32	0.3	0.28	0.26	0.24	0.22	0.2	0.18	0.16	0.14	0.12	0.1	0.08	0.06	0.04	0.02	0	
0.549	0.559	0.570	0.582	0.595	0.608	0.622	0.637	0.653	0.670	0.689	0.710	0.732	0.757	0.785	0.818	0.856	0.869	0.882	0.895	0.908	0.921	0.050
0.549	0.559	0.570	0.582	0.595	0.608	0.622	0.637	0.653	0.670	0.689	0.710	0.732	0.757	0.785	0.818	0.856	0.865	0.873	0.882	0.890	0.899	0.063
0.549	0.559	0.570	0.582	0.595	0.608	0.622	0.637	0.653	0.670	0.689	0.710	0.732	0.757	0.785	0.818	0.856	0.859	0.862	0.865	0.868	0.872	0.079
0.549	0.599	0.570	0.582	0.595	0.608	0.622	0.637	0.653	0.670	0.689	0.710	0.732	0.757	0.785	0.818	0.856	0.853	0.849	0.846	0.842	0.839	0.100
0.626	0.635	0.644	0.654	0.664	0.675	0.686	0.697	0.709	0.721	0.734	0.748	0.762	0.777	0.793	0.810	0.828	0.822	0.816	0.811	0.805	0.799	0.126
0.662	0.669	0.677	0.685	0.694	0.702	0.710	0.719	0.727	0.736	0.744	0.753	0.761	0.768	0.775	0.781	0.784	0.777	0.771	0.765	0.758	0.752	0.158
0.663	0.669	0.676	0.682	0.689	0.695	0.702	0.708	0.714	0.719	0.725	0.729	0.733	0.735	0.736	0.733	0.727	0.721	0.715	0.709	0.703	0.697	0.200
0.635	0.640	0.646	0.651	0.656	0.661	0.666	0.670	0.674	0.678	0.680	0.682	0.683	0.682	0.678	0.671	0.659	0.654	0.649	0.644	0.639	0.634	0.251
0.584	0.588	0.593	0.597	0.601	0.605	0.608	0.611	0.614	0.616	0.617	0.617	0.616	0.613	0.608	0.599	0.584	0.580	0.576	0.572	0.568	0.564	0.316
0.516	0.519	0.523	0.526	0.529	0.532	0.535	0.537	0.539	0.540	0.540	0.540	0.538	0.534	0.528	0.519	0.504	0.501	0.498	0.495	0.492	0.489	0.398
0.437	0.440	0.442	0.445	0.447	0.449	0.451	0.453	0.454	0.455	0.455	0.454	0.452	0.449	0.444	0.435	0.423	0.420	0.418	0.416	0.414	0.412	0.501

(s)

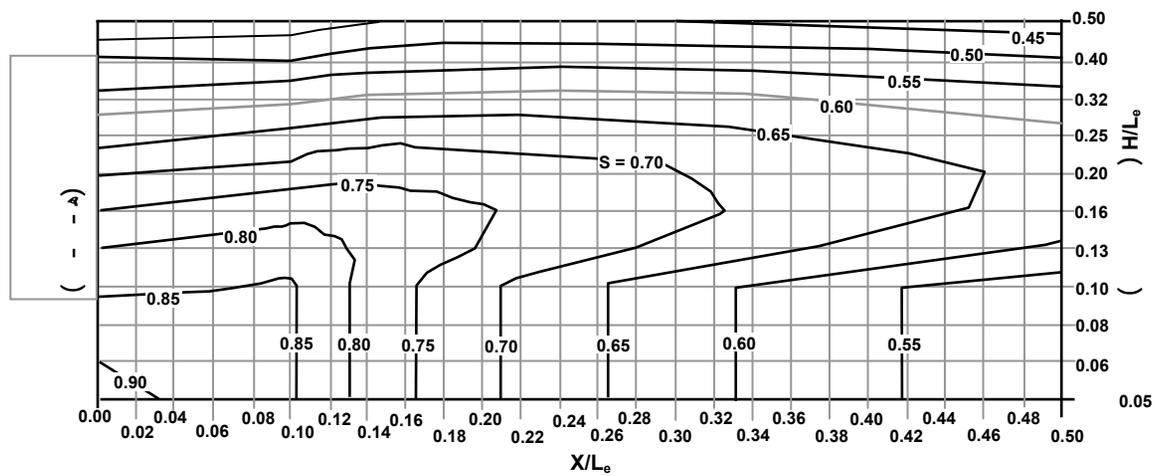
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X/L <sub>e</sub>		X/L <sub>e</sub>		H/L <sub>e</sub>
0.5	0.48	0.46	0.44	
0.510	0.519	0.529	0.538	0.050
0.510	0.519	0.529	0.538	0.063
0.510	0.519	0.529	0.538	0.079
0.510	0.519	0.529	0.538	0.100
0.591	0.600	0.608	0.617	0.126
0.632	0.639	0.646	0.654	0.158
0.637	0.643	0.650	0.656	0.200
0.613	0.618	0.624	0.629	0.251
0.565	0.570	0.575	0.579	0.316
0.501	0.505	0.508	0.512	0.398
0.425	0.428	0.431	0.434	0.501



(s) : ( - - Δ )



(s) : ( - - Δ )

( - )

( )	
Width	
Furniture	
Snow Loads	
Live Loads, Imposed Loads	
Dynamic Loads	
Impact Loads	
Equivalent Loads	
Uniformly Distributed Loads	
Height	
Storage Height	
Rice in Sacks	
Floor	
Frames	
Acrylic	
Ammonia	
Dynamic Excitation	
( )	
Span	
Paraffin (Kerosene)	
Landing	
Onion in Sacks	

( )	
Silk Goods in Envelopes	
Wool Goods (Encased Pieces)	
Cotton Goods (Encased Pieces) in Bales	
Cotton Goods (Encased Pieces)	
Potato in Sacks	
Potato, Loose	
Benzene, Benzol	
Bitumen	
Eggs in Cartoons	
( )	
Hay (Pressed in Bales)	
Loads Combination	
Turpentine	
Parapet	
Fig in Boxes	
( )	
Beam	
Girder	
Cheese, Loose	
Rigidity	
Leathers in Bales	
Ice	
Gymnasium	

( )	
Hemp (Cannabis) in Bales	( )
( )	
Guard Rail	
Acetic Acid	
Sulfuric Acid	
Nitric Acid	
Whirled Ropes	
Brewer's Grains (Wet)	
Milk	
Dead Load	
Wheat in Sacks	
Wheat, Loose	
Panic Barriers	
( )	
Ground Roughness	
Amplitude Line	
( )	
Balustrade	
Stairs	
Fats	
( )	
Joist	
Crane	

( )	
Overhead Crane	
Lounge	
( )	
Butter in Barrels	
Glass	
Linseed Oil	
( )	
Carpets	
Suction	
Frictional Drag	
Design Wind Speed	
Basic Wind Speed	
Ceiling	
Roof	
Inaccessible Roofs	
Pitched Roofs	
Sloping Roofs	
Accessible Roofs	
Curved Roofs	
Sugar, Loose	
( )	
Tea in Chests	
Balcony	

( )	
Display & Sale Hall	
Art Galley	
Wool, Loose	
Wool Pressed in Bales	
( )	
Dynamic Pressure	
( )	
Flour in Sacks	
Flour in Bulk	
Length	
Longitudinal	
( )	
Height Factor	
Soil Factor	
Dynamic Factor	
Breadth	
Lateral	
Overturning Moment	
Torsional Moment	
Gust	
Bracing Element	
Depth	
Structural Members	

( )	
Billiard Room	
Dressing Room	
Drill Room	
Stack Room	
Filing Room	
Laundry	
Boiler Room	
Reading Room	
Bed Room	
( )	
Coal, Loose	
Fresh Fruits in Sacks	
Dry Fruits in Sacks	
( )	
Tar, Pitch	
Bank Hall	
Assembly Hall	
Dance Hall	
Dormitory	( )
Base of Structure	
Partitions	
Stiffness	
Cotton in Bales	

( )	
Coffee in Sacks	
Coffee, Loose	
Drag Force	
Wind Forces	
Earthquake Forces	
( )	
Stacking Books	
Alcohol	
Methylated Spirit	
Roof Cladding	
Access Hatches	
( )	
Canned Meats	
( )	
Sea Water	
Fresh Water	
Museum	
Design Requirements	
Motor	
Tinned Pickles	
Hallway	
Garage	
Fan	

( )	
Effective Frontal Area	
Foundry	
Warehouse	
Cold Storage	
Stationery	( )
Theater	
Workshops	
Drinks, Loose	
Drinks in Barrels	
Drinks in Bottles	
Lift	
Factory	
Rubber	
Kitchen	
Drag Coefficient	
Pressure Coefficient	
Force Coefficient	
Plastic Hinge	
Slipping Resistance	
Fly Gallery	
Reciprocating Machinery	
Salt in Packets	
Salt, Loose	
Corridor	

( )	
Cat Walk	
Foot Bridge	( )
Footpath	
Special Structure	
Stage	( )
Skylight	
( )	
Aspect Ratio	
Paper Wastes (Pressed)	
Sewage	
Naphtha	
(A)	
Ductile Frame	
Space Frame	
Braced Frame	
( )	
Paper	

( - )

<b>(A)</b>	
Acetic Acid	
Access Hatches	
Accessible Roofs	
Acrylic	
Alcohol	
Ammonia	
Amplitude Line	
Art Gallery	
Aspect Ratio	
Assembly Hall	
<b>(B)</b>	
Balcony	
Balustrade	
Bank Hall	
Base of Structure	
Basic Wind Speed	
Beam	
Bed Room	
Benzene, Benzol	
Billiard Room	
Bitumen	
Boiler Room	
Braced Frame	

<b>(B)</b>	
Bracing Element	
Breadth	
Brewer's Grains (Wet)	
Butter in Barrels	
<b>(C)</b>	
Canned Meats	
Carpets	
Cat Walk	
Ceiling	
Cheese, Loose	
Coal, Loose	
Coffee in Sacks	
Coffee, Loose	
Cold Storage	
Corridor	
Cotton Goods (Encased Pieces)	
Cotton Goods (Encased Pieces) in Bales	
Cotton in Bales	
Crane	
Curved Roofs	
<b>(D)</b>	
Dance Hall	
Dead Load	
Depth	
Design Requirements	

<b>(D)</b>	
Design Wind Speed	
Display & Sale Hall	
Dormitory	( )
Drag Coefficient	
Drag Force	
Dressing Room	
Drill Room	
Drinks in Barrels	
Drinks in Bottles	
Drinks, Loose	
Dry Fruits in Sacks	
Ductile Frame	
Dynamic Excitation	
Dynamic Factor	
Dynamic Loads	
Dynamic Pressure	
<b>(E)</b>	
Earthquake Forces	
Effective Frontal Area	
Eggs in Cartoons	
Equivalent Loads	
<b>(F)</b>	
Factory	
Fan	
Fats	

<b>(F)</b>	
Fig in Boxes	
Filing Room	
Floor	
Flour in Bulk	
Flour in Sacks	
Fly Gallery	
Foot Bridge	(       )
Footpath	
Force Coefficient	
Foundry	
Frames	
Fresh Fruits in Sacks	
Fresh Water	
Frictional Drag	
Furniture	
<b>(G)</b>	
Garage	
Girder	
Glass	
Ground Roughness	
Guard Rail	
Gust	
Gymnasium	
<b>(H)</b>	
Hallway	

<b>(H)</b>	
Hay (Pressed in Bales)	
Height	
Height Factor	
Hemp (Cannabis) in Bales	( )
<b>(I)</b>	
Ice	
Impact Loads	
Imposed Loads	
Inaccessible Roofs	
<b>(J)</b>	
Joist	
<b>(K)</b>	
Kitchen	
<b>(L)</b>	
Landing	
Lateral	
Laundry	
Leathers in Bales	
Length	
Lift	
Linseed Oil	
Live Loads	
Loads Combination	
Longitudinal	
Lounge	

<b>(M)</b>	
Methylated Spirit	
Milk	
Motor	
Museum	
<b>(N)</b>	
Naphtha	
Nitric Acid	
<b>(O)</b>	
Onion in Sacks	
Overhead Crane	
Overturning Moment	
<b>(P)</b>	
Panic Barriers	
Paper	
Paper Waste (Pressed)	
Paraffin (Kerosene)	
Parapet	
Partitions	
Pitched Roofs	
Plastic Hinge	
Potato in Sacks	
Potato, Loose	
Pressure Coefficient	
<b>(R)</b>	
Reading Room	

<b>(R)</b>	
Reciprocating Machinery	
Rice in Sacks	
Rigidity	
Rolling Loads	
Roof	
Roof Cladding	
Rubber	
<b>(S)</b>	
Salt in Packets	
Salt, Loose	
Sea Water	
Sewage	
Silk Goods in Envelopes	
Skylight	
Slipping Resistance	
Sloping Roofs	
Snow Loads	
Soil Factor	
Space Frame	
Span	
Special Structure	
Stack Room	
Stacking Books	
Stage	( )

<b>(S)</b>	
Stairs	
Stationery	(       )
Stiffness	
Storage Height	
Structural Members	
Suction	
Sugar, Loose	
Sulfuric Acid	
<b>(T)</b>	
Tar, Pitch	
Tea in Chests	
Theater	
Tinned Pickles	
Torsional Moment	
Turpentine	
<b>(U)</b>	
Uniformly Distributed Loads	
<b>(W)</b>	
Warehouse	
Wheat in Sacks	
Wheat, Loose	
Whirled Ropes	
Width	
Wind Forces	
Wool Goods (Encased Pieces)	

	(W)
Wool Pressed in Bales	
Wool, Loose	
Workshops	

3. DESIGN LOADING FOR BUILDINGS,  
Part 1. Code of Practice For Dead & Imposed Loads,  
BS 6399:Part 1:1996,  
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4. LOADING FOR BUILDINGS,  
Part 2. Code of Practice For wind Loads,  
BS 6399:Part 2:1997,  
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Part 4. Code of Practice For Loading of Guyed Masts,  
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British Standards Institution.

(SI-Units)

	mm cm m km		
	mg g kg t		
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	mL L m <sup>3</sup>		
	mm <sup>2</sup> m <sup>2</sup>		
	N kN		
/	N/mm <sup>2</sup>	/	
/	kN/m <sup>2</sup>	/	
°	°C	°	

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.	9.81	=	1
/	9.81	=	1
/	0.0981	=	1
/	9.81	=	1
/	9.81	=	1
	1	=	0.102
.	1	=	0.102
/	1	=	0.102
/	1	=	10.20
/	1	=	0.102
/	1	=	0.102

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