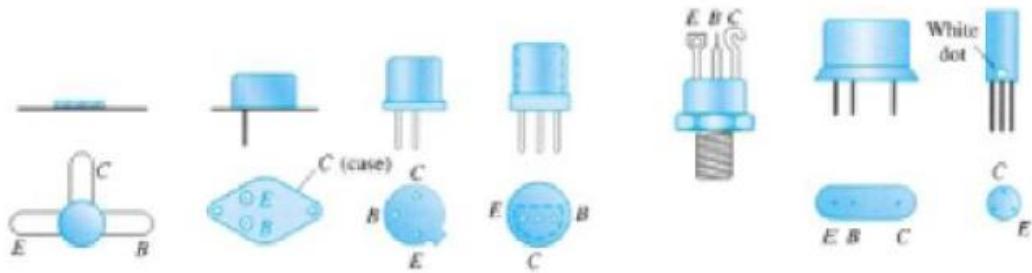


L9 - part 2
sec 1
27/7/2021



ENEE2360 Analog Electronics

T6: Bipolar Junction Transistor

B J T

Instructor : Nasser Ismail

The First Transistor

Co-inventors of the first transistor at Bell Laboratories: Dr. William Shockley (seated); Dr. John Bardeen (left); Dr. Walter H. Brattain. (Courtesy of AT&T Archives.)

Dr. Shockley Born: London, England, 1910
PhD Harvard, 1936

Dr. Bardeen Born: Madison, Wisconsin, 1908
PhD Princeton, 1936

Dr. Brattain Born: Amoy, China, 1902
PhD University of Minnesota, 1928

All shared the Nobel Prize in 1956 for this contribution.

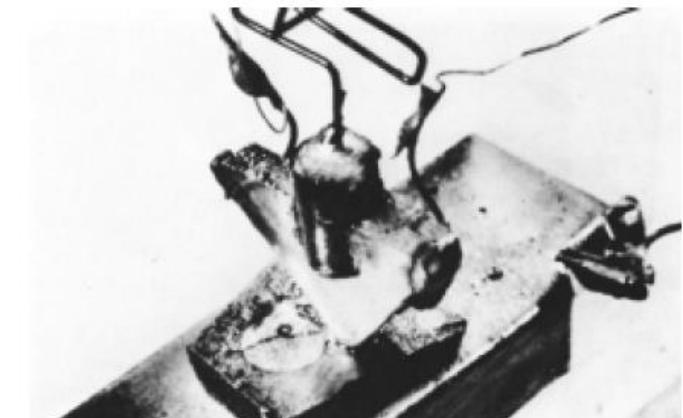
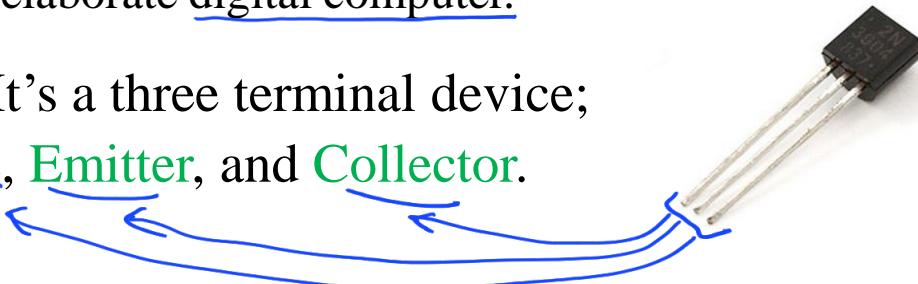


Figure 3.1 The first transistor. (Courtesy Bell Telephone Laboratories.)

Bipolar Junction Transistor (BJT):

BJT:

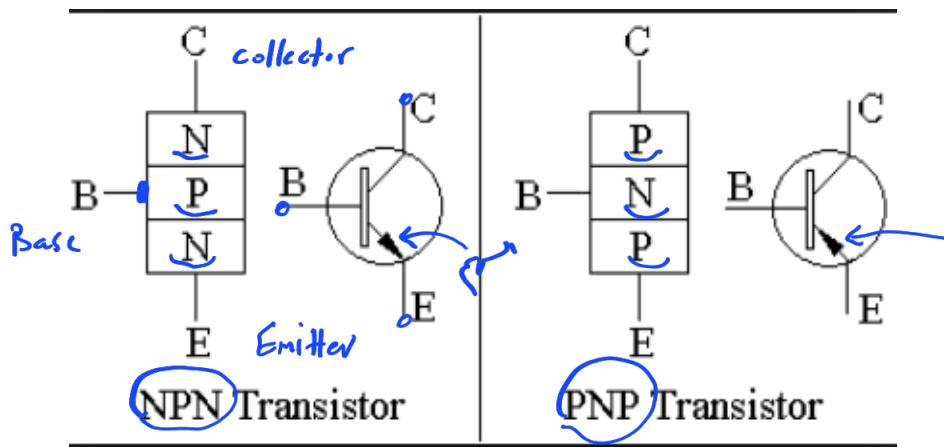
1. It's a semiconductor device that can amplify electrical signals such as radio or television signals.
2. Its essential ingredient of every electronic circuits; from the simplest amplifier or oscillator to the most elaborate digital computer.
3. It's a three terminal device;
Base, Emitter, and Collector.



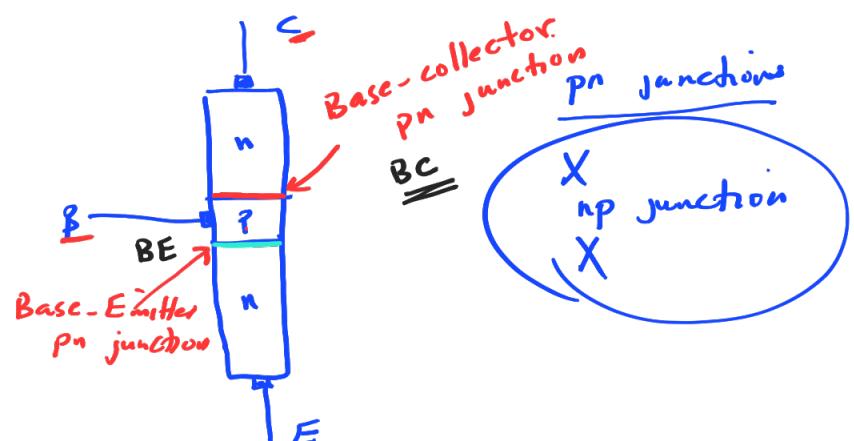
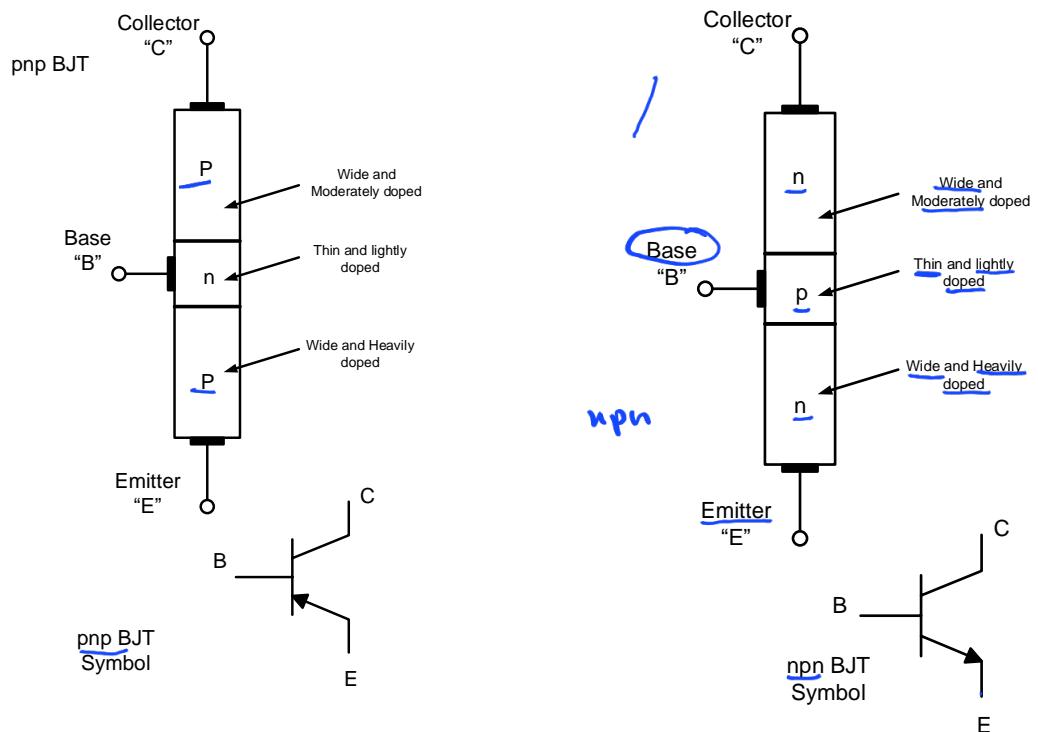
There are two type of BJT:

➤ npn type *ن PNPN*

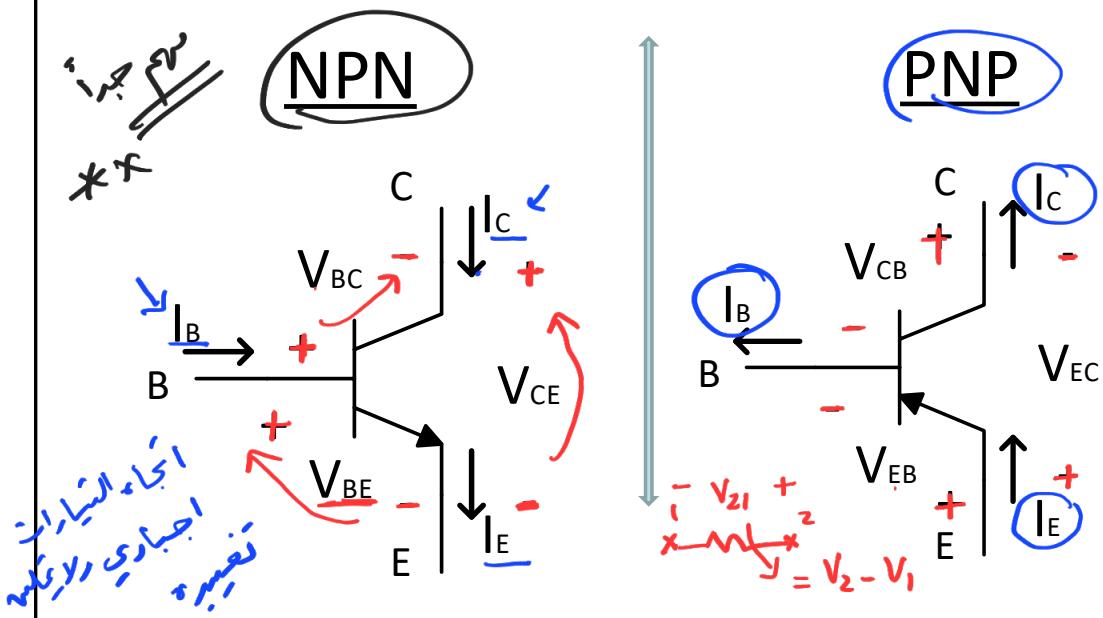
➤ pnp type

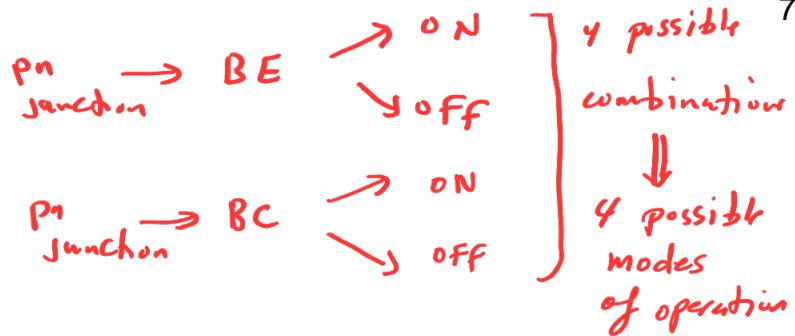
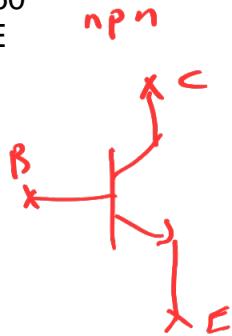


Construction and Symbol



Transistor structure:



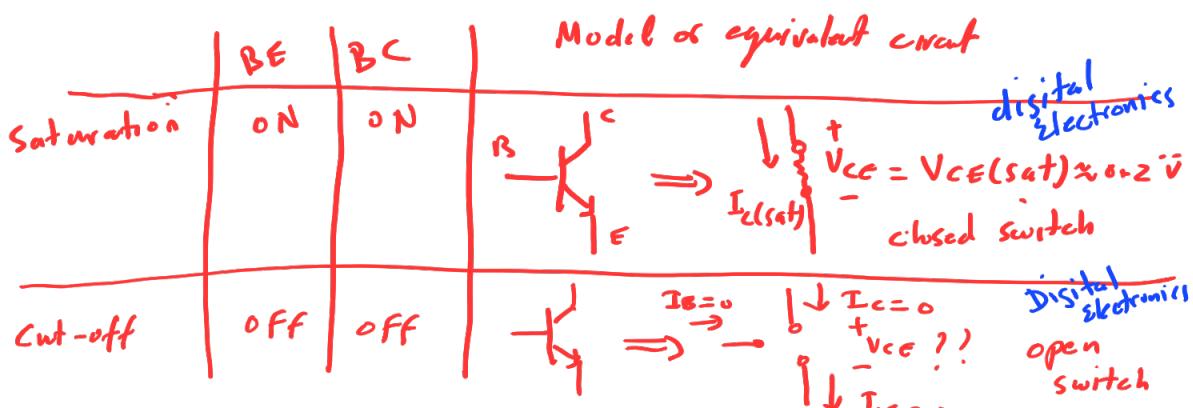


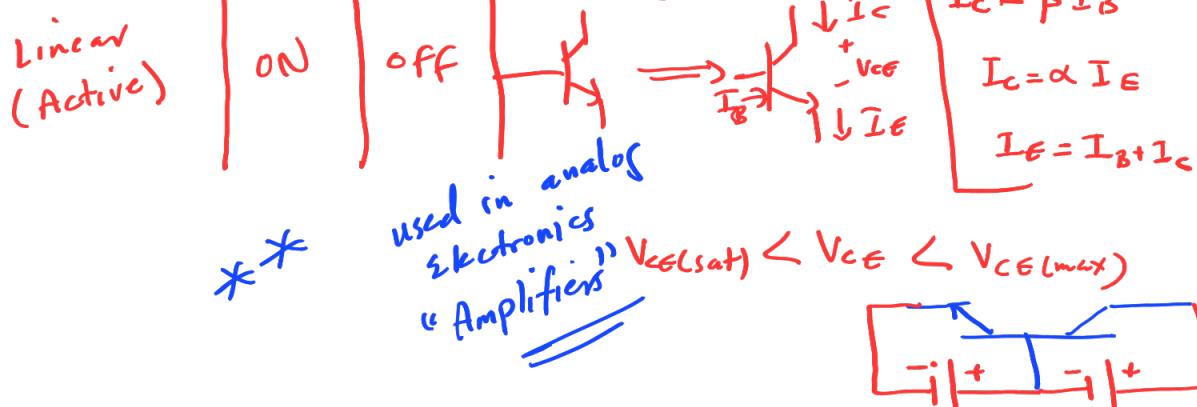
Transistor biasing:

- In order to operate properly as an amplifier, it's necessary to correctly bias the two pn-junctions with external voltages.
- Depending upon external bias voltage polarities used; the transistor works in one of **four regions** (modes). npn transistor modes of operation

- For transistor to be used as an Active device (**Amplifier**); the **emitter-base** junction must be **forward** bias, while the **collector-base** junction must be **reverse** biased.

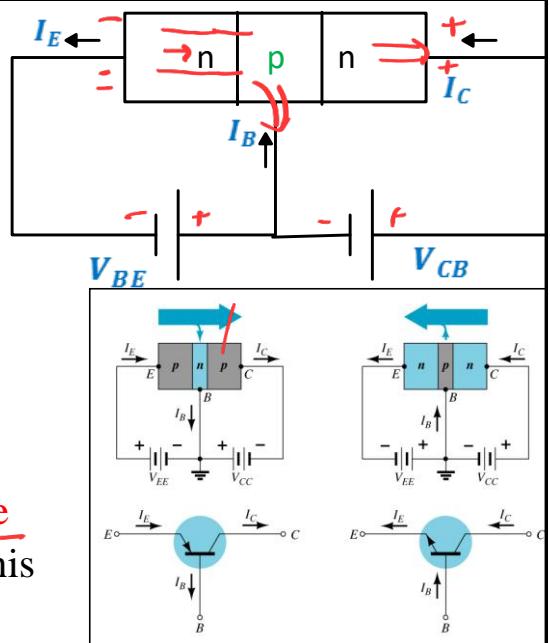
Junction/ Mode	BE	BC	Remarks
1) Saturation Mode	Forward	Forward	Equivalent to short circuit $I_c = I_c(sat)$ $V_{ce} = V_{ce}(sat) \approx 0.2V$
2) Active Mode (Linear Region)	Forward	Reverse	I_c proportional to I_b V_{ce} defined by circuit
3) Cut-off Mode	Reverse	Reverse	Equivalent to open circuit $I_c = I_b = 0$ V_{ce} defined by circuit
X) Inverse Mode	Reverse	Forward	Rarely used and will not be discussed in this course X

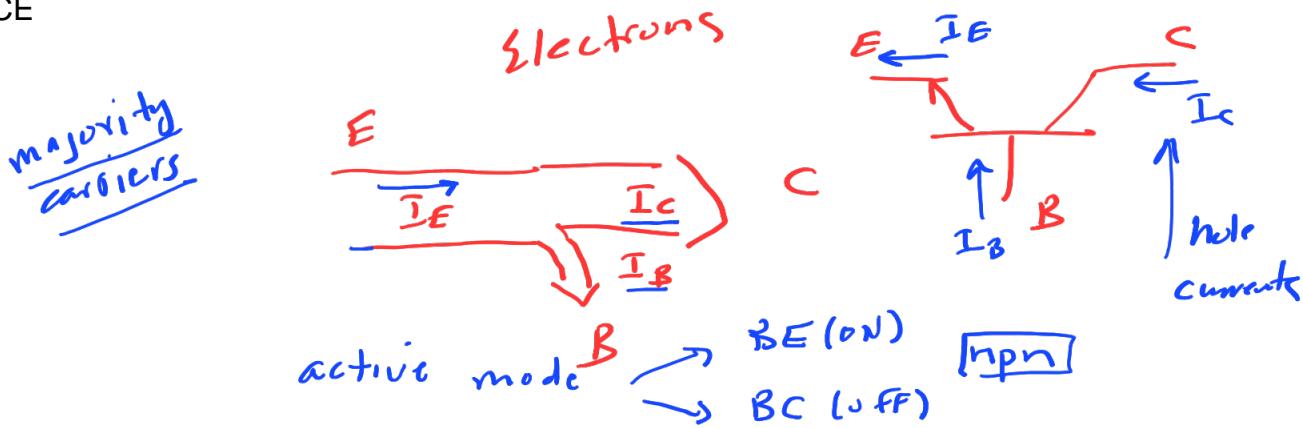




In active region

- ✓ The base region is thin and lightly doped
- ✓ The base-emitter junction is forward biased, thus the depletion region at this junction is reduced.
- ✓ The base-collector junction is reverse biased, thus the depletion region at this junction is increased.
- ✓ The forward biased BE-junction causes the electrons in the n-type emitter to flow toward the base; this constitutes the emitter current I_E .
- ✓ As these electrons flow through the P-type base; they tend to recombine with holes in p-type base. →





✓ Since the **base** region is **lightly doped**; very **few** of the **electrons** injected into the **base** from the **emitter** recombine with **holes** to constitute **base current I_B** and the remaining **large number** of electrons cross the **base** and move through the **collector region** to the **positive terminal** of the external DC source; this constitute **collector current I_C**

✓ There is another component for **I_C** due to the **minority carrier**; **I_{CBO}** which will be ignored

$$I_C = \alpha I_E + I_{CBO}$$

Minority

Majority

$0.998 > \alpha > 0.9$

$I_E > I_C$

$I_E \leftrightarrow I_C$

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$$\begin{aligned} I_C &= \alpha I_E + I_{CBo} \quad \checkmark \\ \underline{I_E = I_C + I_B} &\quad \times \\ I_C &= \alpha(I_C + I_B) + I_{CBo} \\ \diamond I_C &= \frac{\alpha}{1-\alpha} I_B + \frac{1}{1-\alpha} I_{CBo} \end{aligned}$$

Let Beta, $\underline{\underline{\beta}} = \frac{\alpha}{1-\alpha}$

$$\diamond I_C = \beta I_B + (\beta + 1) I_{CBo}$$

$$I_C = \beta I_B + I_{CBo}$$

$$\boxed{\beta = \frac{\alpha}{1 - \alpha}}$$

If $\alpha = 0.99$

If $\alpha = 0.995$

$$\longrightarrow \beta = 99$$

$$\longrightarrow \beta = 199$$



In active region:

$$I_C = \alpha I_E + I_{CBo}$$

$$I_C = \beta I_B + (\beta + 1)I_{CBo}$$

$$I_C = \beta I_B + I_{CEO}$$

$$I_E = I_C + I_B$$

Approximate relationships:

$$I_C \approx \alpha I_E$$

$$I_C \approx \beta I_B$$

$$I_E \approx (\beta + 1)I_B$$

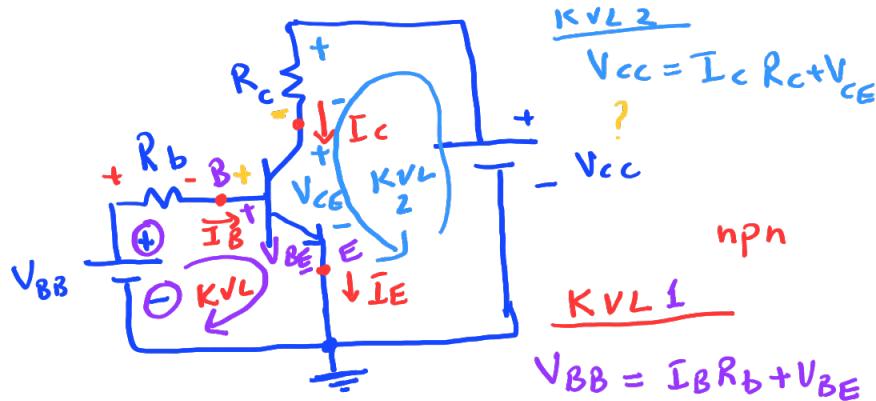
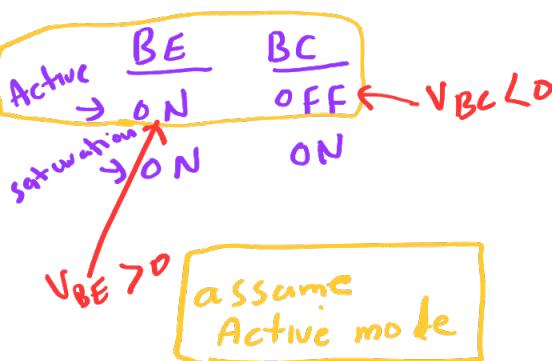
$$\beta = \frac{\alpha}{1 - \alpha}$$

Summary

will be used in this course



- <https://www.youtube.com/watch?v=7ukDKVHnac4>



Basic BJT Amplifiers Circuits

$$\alpha \approx \frac{I_C}{I_E}$$

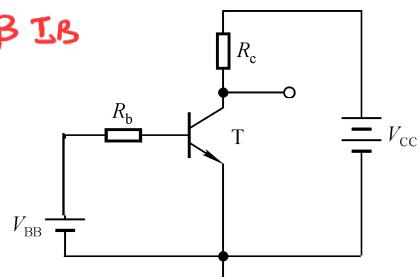
BJT in Active Mode

$$I_E = I_B + I_C$$

$$\beta \approx \frac{I_C}{I_B}$$

$$\beta = \frac{\alpha}{1-\alpha}$$

---common-emitter current gain



BJT DC Analysis

- Make sure the BJT current equations and region of operation match

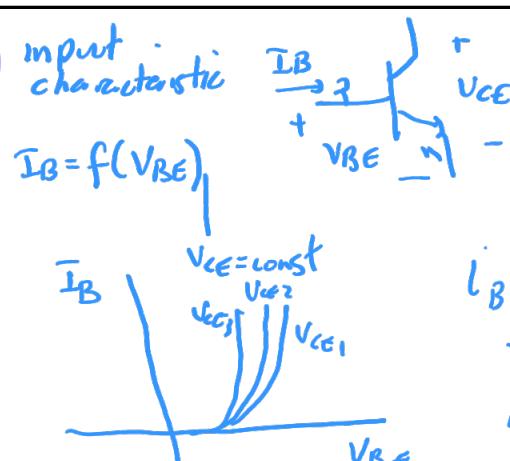
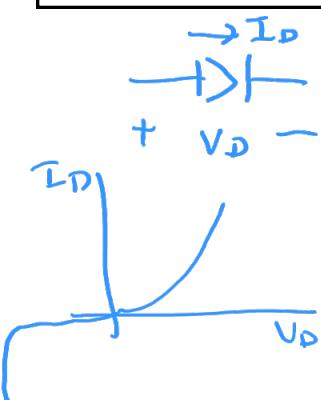
$$V_{BE} > 0, \checkmark$$

$$V_{BC} < 0, \checkmark \rightarrow V_E < V_B < V_C$$

- Utilize the relationships (β and α) between collector, base, and emitter currents to solve for all currents

$$\begin{cases} I_E = I_C + I_B = (1 + \beta)I_B \\ I_C = \beta I_B \\ I_C = \alpha I_E \end{cases}$$

* Active region



$$i_B(t) = I_{BD} \left(e^{\frac{V_{BE}}{2V_T}} - 1 \right)$$

$$i_B(t) = I_{B0} e^{\frac{V_{BE}}{2V_T}}$$

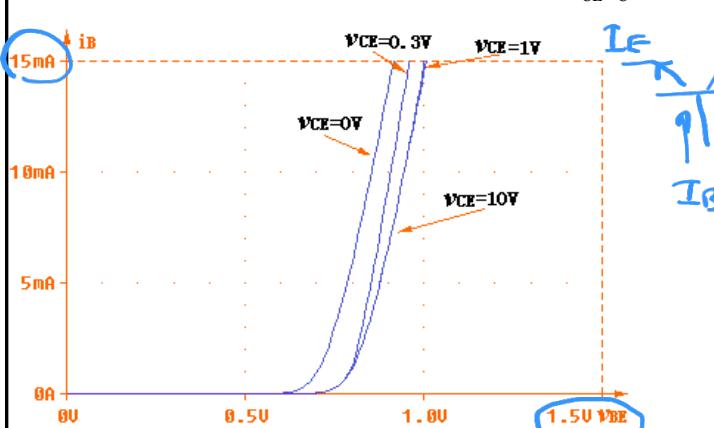
$$i_c(t) = \beta i_B(t)$$

Basic BJT Amplifiers Circuits

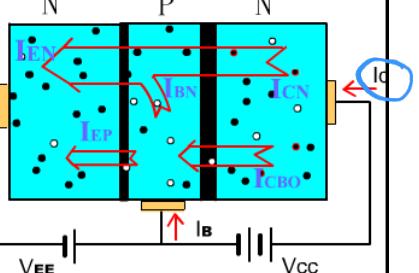
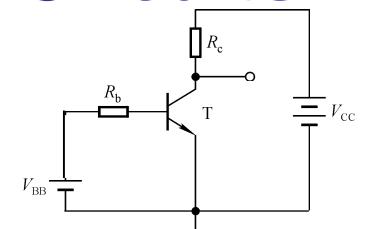
C-E Circuits I-V Characteristics

Base-emitter Characteristic (Input characteristic)

$$i_B = f(v_{BE}) \Big|_{v_{CE}=C}$$



$$i_C(t) \cong I_S \left(e^{\frac{V_{BE}(t)}{nV_T}} \right)$$



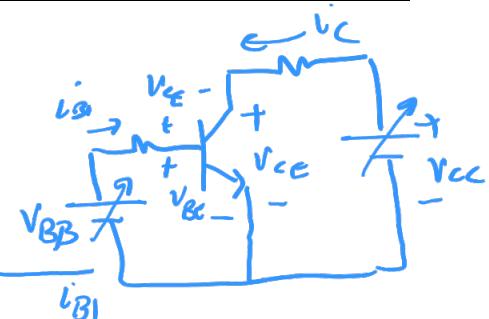
$$i_{B(t)} = I_{Bo} \left(e^{\frac{V_{BE}(t)}{nV_T}} - 1 \right)$$

$$i_{B(t)} \cong I_{Bo} \left(e^{\frac{V_{BE}(t)}{nV_T}} \right)$$

2) Output (collector) characteristic

$$i_C = f(v_{CE}) \Big|_{i_B = \text{const}}$$

i_C
cut-off
 $v_{CE(sat)}$



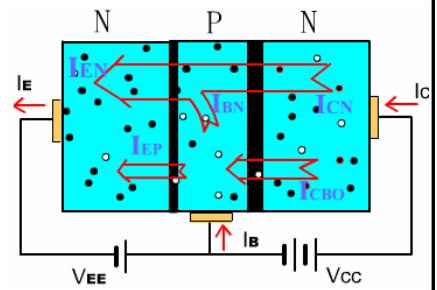
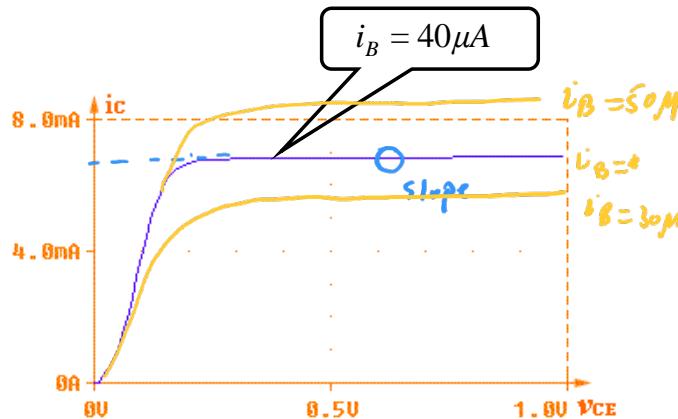
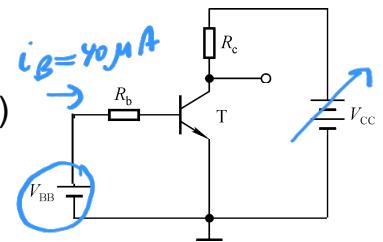
v_{CE}

Basic BJT Amplifiers Circuits

C-E Circuits I-V Characteristics

Collector characteristic (output characteristic)

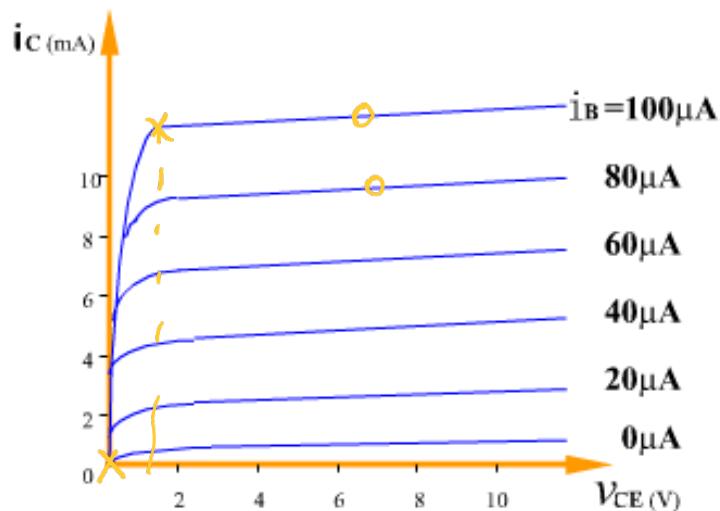
$$i_C = f_{(V_{CE})} \Big|_{i_B=C}$$



Basic BJT Amplifiers Circuits

C-E Circuits I-V Characteristics

Collector characteristic (output characteristic) $i_C = f_{(V_{CE})} \Big|_{i_B=C}$



in general

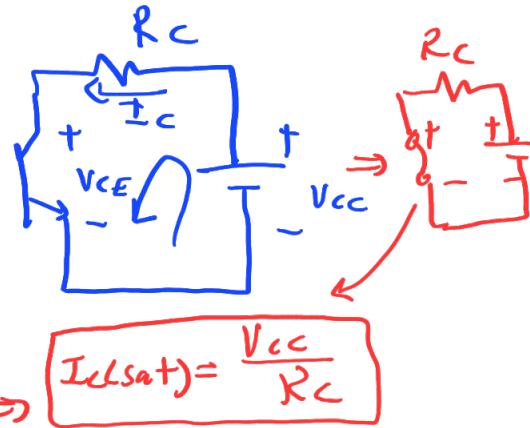
$$V_{CC} - I_C R_C - V_{CE} = 0$$

in saturation mode

$$V_{CE} = V_{CE(sat)} \approx 0.2 \text{ V}$$

$$I_C = I_{C(sat)} = \frac{V_{CC} - 0.2}{R_C}$$

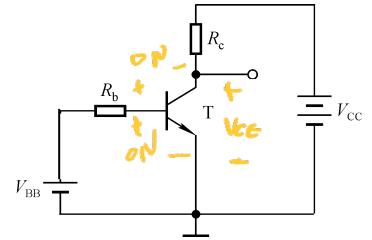
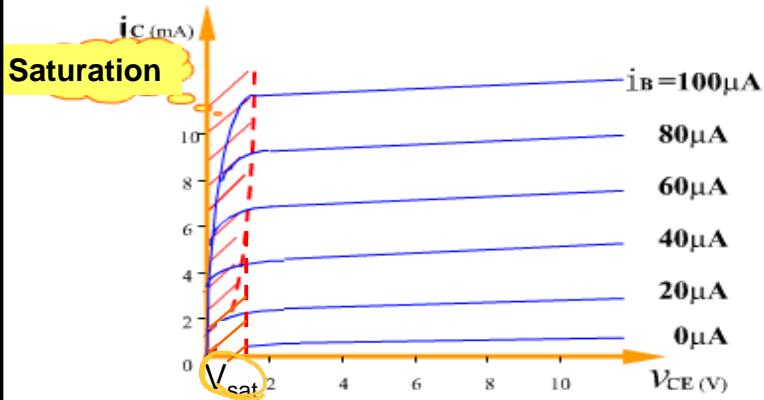
if $V_{CE(sat)}$ assumed = 0 \Rightarrow



Basic BJT Amplifiers Circuits

C-E Circuits I-V Characteristics

Collector characteristic



$$V_{CE(sat)} \approx 0.2 \text{ V}$$

Saturation occurs when the supply voltage, V_{CC} , is across the total resistance of the collector circuit, R_C .

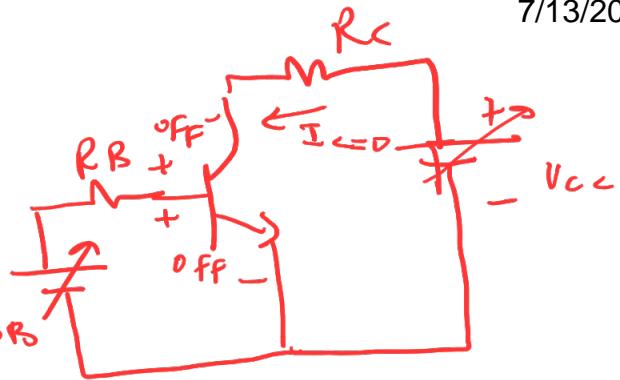
$$I_{C(sat)} = V_{CC}/R_C$$

Once the base current is high enough to produce saturation, further increases in base current have no effect on the collector current and the relationship $I_C = \beta I_B$ is no longer valid. When V_{CE} reaches its saturation value, $V_{CE(sat)}$, the base-collector junction becomes forward-biased.

In cut off mode

$$V_{CC} - I_C R_C - V_{CE} = 0$$

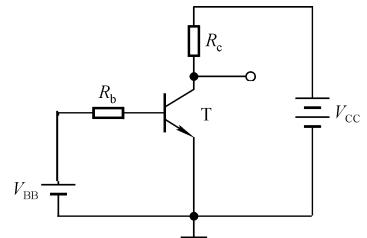
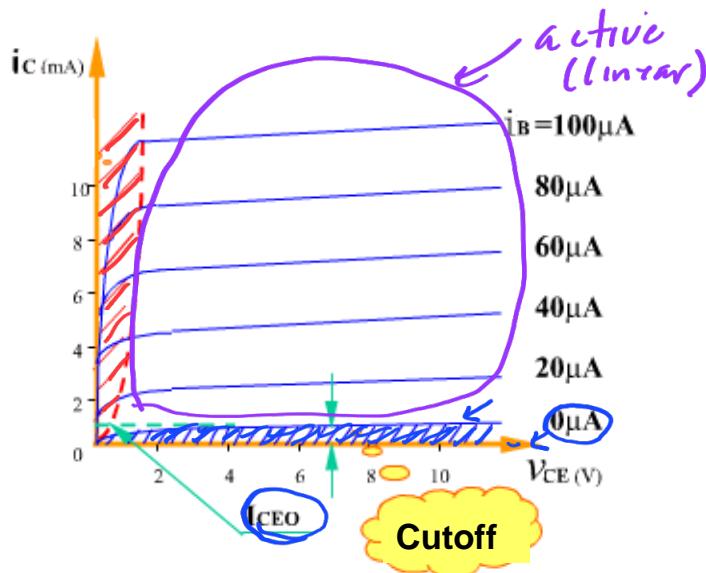
$$\therefore V_{CE} = V_{CC} = V_{CE}(\text{cut-off})$$



Basic BJT Amplifiers Circuits

C-E Circuits I-V Characteristics

Collector characteristic



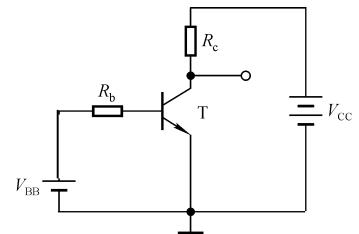
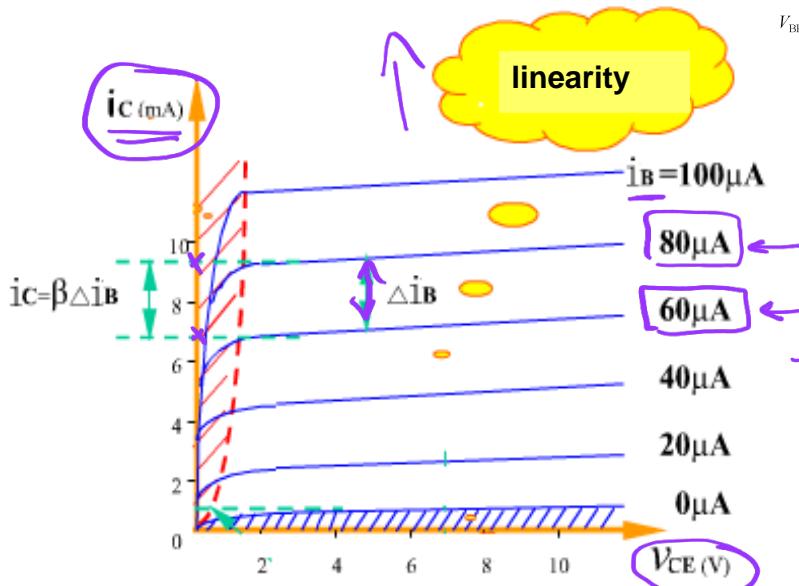
When $I_B = 0$, the transistor is in cutoff and there is essentially no collector current except for a very tiny amount of collector leakage current, I_{CEO} , which can usually be neglected. $I_C \approx 0$.

In cutoff both the base-emitter and the base-collector junctions are reverse-biased.

Basic BJT Amplifiers Circuits

C-E Circuits I-V Characteristics

Collector characteristic



* Summary

1. In the cutoff region :

$$I_B = I_C = I_E = 0$$

2. In the active region :

$$I_C = \alpha I_E$$

$$I_C = \beta I_B$$

$$I_E = (\beta + 1)I_B$$

$$V_{BE} = 0.7v, \text{ Si}, \text{ npn}$$

$$V_{BE} = -0.7v, \text{ Si}, \text{ pnp}$$

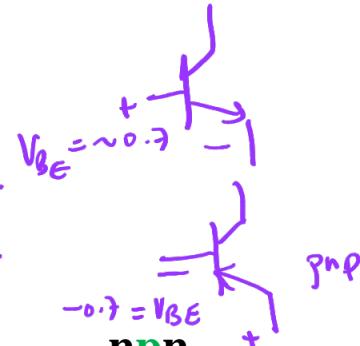
$$V_{CE} > V_{CE,sat} = 0.2v, \text{ Si}, \text{ npn}$$

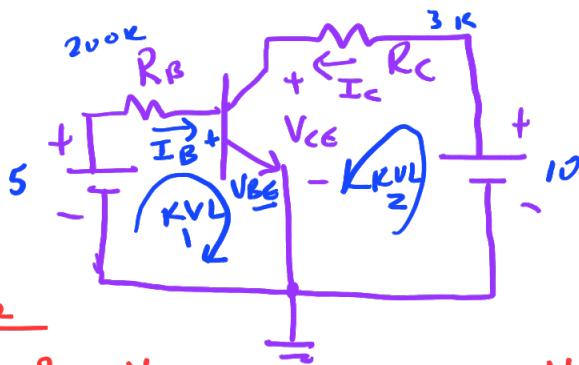
$$V_{CE} < V_{CE,sat} = -0.2v, \text{ Si}, \text{ pnp}$$

$$\uparrow \text{ or } V_{CE(sat)} = 0.2$$

3. In the saturation region :

$$V_{CE} = V_{CE,sat}$$





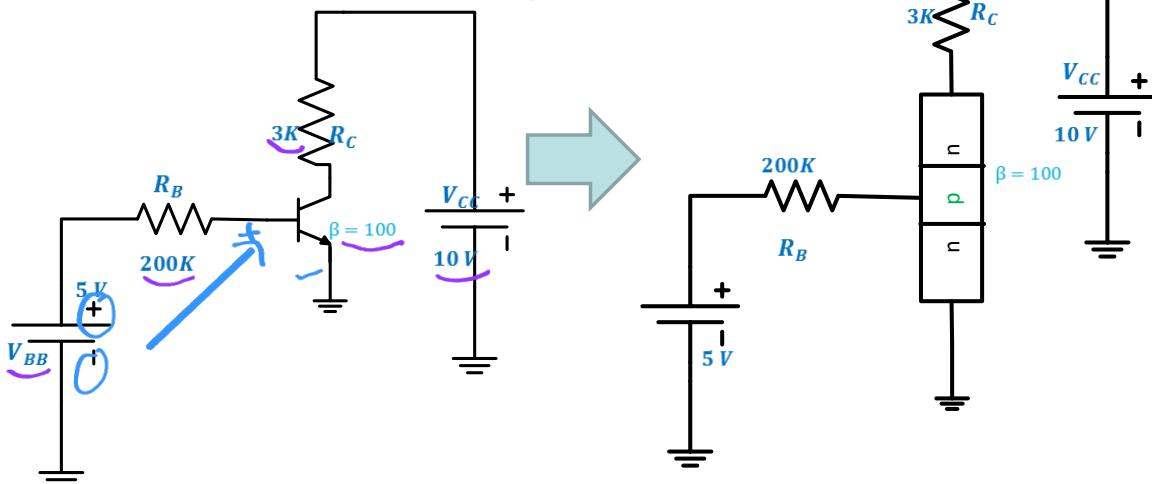
$$V_{CE} = 10 - (2.15mA \times 3k) = 3.55V$$

→ *V_{CEsat}* ? *V_{CE}* in active mode?

$$\begin{aligned} V_{BE} &= 0.7 \leftarrow \text{active} \\ \therefore I_B &= \frac{5 - 0.7}{200k} = 21.5\text{mA} \\ I_C &= \beta I_B = 100 \times 21.5\text{mA} \\ &= 2.15\text{mA} \end{aligned}$$

Example: *BJT assumed in operating point*

Find mode of operation and the Q point V_{CEQ} , I_{CQ}



Since the base emitter junction is forward bias; the transistor could be either in the active or the saturation region

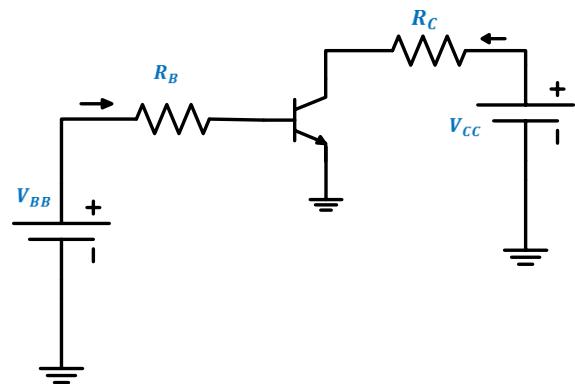


In General

1) In the active region:

$$\begin{aligned} I_B &= \frac{V_{BB} - V_{BE}}{R_B} \\ I_C &= \beta I_B \\ V_{CE} &= V_{CC} - R_C I_C \end{aligned}$$

As : R_B , I_B , I_C , V_{CE}



2) In the saturation region:

$$V_{CE} = V_{CE,sat} = 0.2 \text{ v} , \text{ Si} , \text{ nPn}$$

$$I_C = I_{C,sat} = \frac{V_{CC} - V_{CE,sat}}{R_C}$$

➤ Assume that the transistor is in the active region:

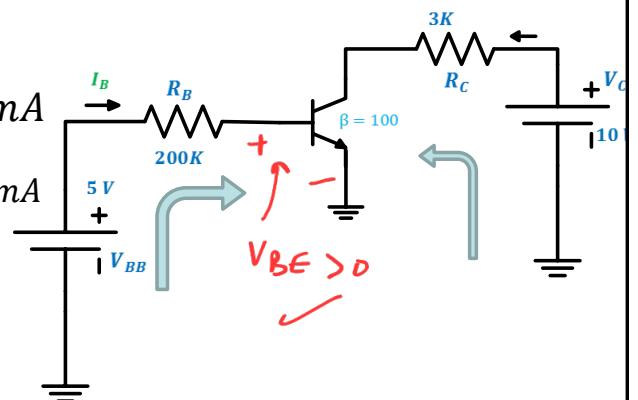


KVL: $5 = 200k I_B + V_{BE}$

✓ $I_B = \frac{5 - 0.7}{200k} = 0.0215 \text{ mA}$

KVL: $10 = R_C I_C + V_{CE}$

✓ $V_{CE} = 10 - R_C I_C$



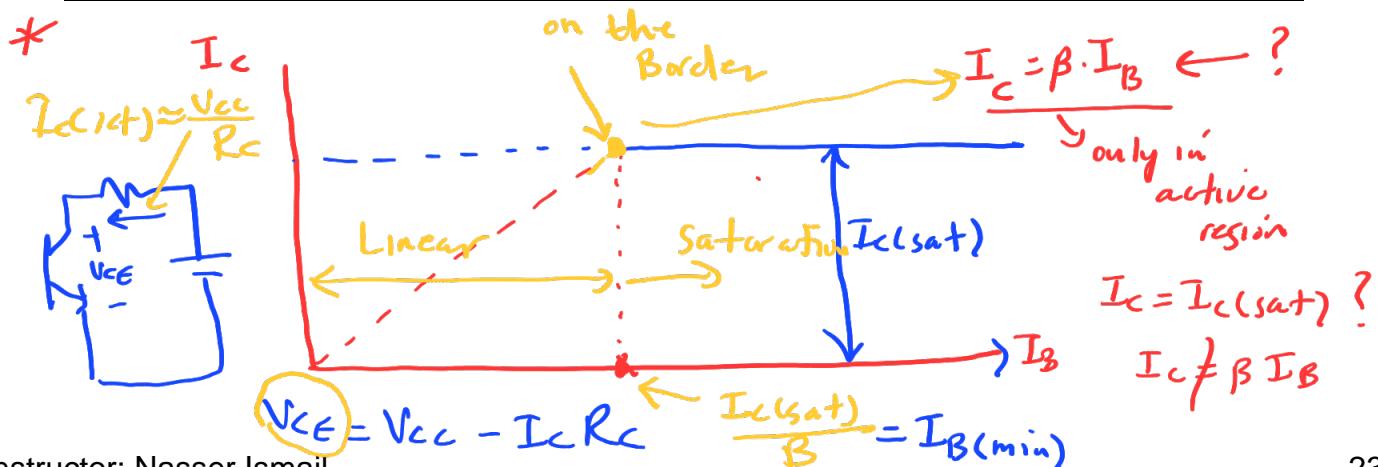
❖ $V_{CE} = 10 - 3k * 2.15 \text{ mA} = 3.55 \text{ Volt}$

Since

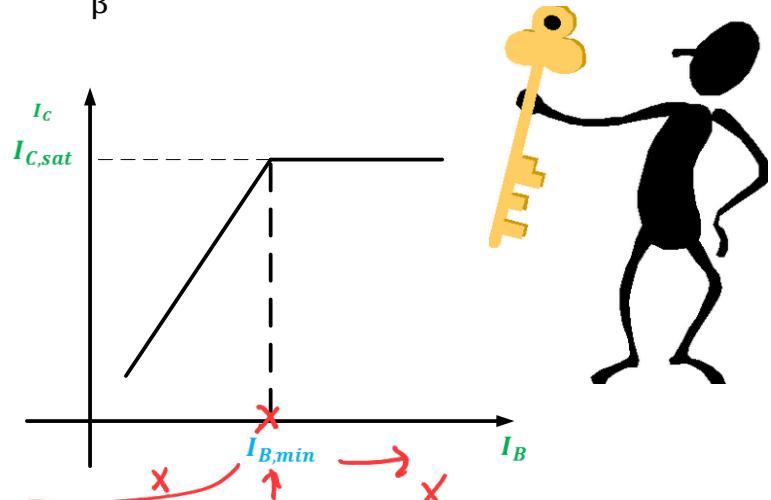
$V_{CE} > V_{CE,sat}$ ➤ The transistor is in the active region

➤ $V_{CEQ} = 3.55 \text{ Volt}$

➤ $I_{CQ} = 2.15 \text{ mA}$



Let define: $I_B(min) = \frac{I_{C,sat}}{\beta}$

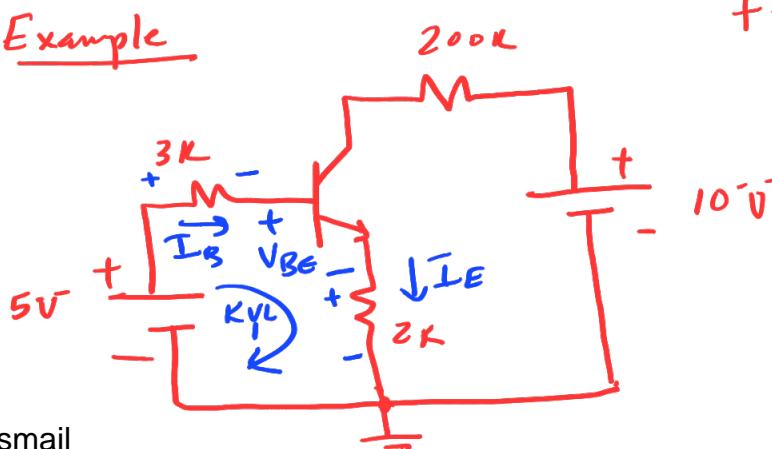


$$I_B(min) = \frac{I_{C,sat}}{\beta}$$

- If $I_B > I_B(min)$ the transistor is in the Saturation region.
- If $I_B < I_B(min)$ the transistor is in the Active region.

$$\beta = 100$$

Example



Find Mode of operation & I_c, V_{ce} ?

$V_{BE} > 0 \rightarrow \text{BJT}$

assume active mode

$$5 = 3k(I_B) + V_{BE} + 2k(I_E)$$

$$I_E = I_C + I_B = \beta I_B + I_B = (\beta + 1)I_B$$

$$\left. \begin{aligned} I_B &= \frac{5 - 0.7}{3k + 2k(\beta + 1)} \\ I_B &= 10.7 \mu A \end{aligned} \right\}$$

Determine Mode of Operation of BJT?

- Solution 1:
- 1) Since BE junction is forward biased \Rightarrow Q1 can be either in Active (Linear) or Saturation mode
- Assume it is in Active Mode

$$5 = 200 \text{ k}\Omega \cdot I_B + V_{BE} + 2 \text{ k}\Omega \cdot I_E$$

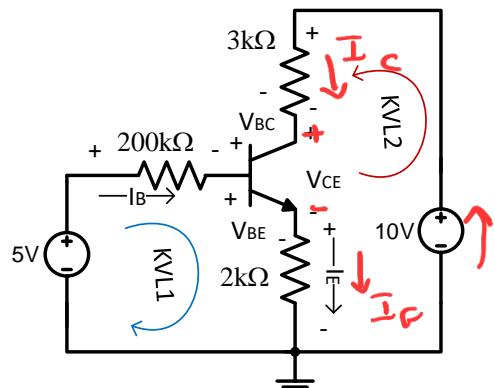
But,

$$I_E = (1 + \beta)I_B$$

Solve for $I_B = \frac{5 - V_{BE}}{200 \text{ k}\Omega + (1 + \beta) \cdot 2 \text{ k}\Omega}$

$$I_B = \frac{5 - 0.7}{200 \text{ k}\Omega + (1 + 100) \cdot 2 \text{ k}\Omega}$$

$$= \frac{4.3 \text{ V}}{402 \text{ k}\Omega} = 10.7 \mu A$$



$$I_C = \beta I_B = 100 \times 10.7 \mu A = 1.07 \text{ mA}$$

$$I_E = (\beta + 1)I_B = 101 \times 10.7 \mu A = 1.087 \text{ mA}$$

$$\underline{\text{KVL2}} \quad 10 = I_C \cdot 3k + V_{CE} + I_E \cdot 2k$$

$$V_{CE} = 10 - 1.07 \text{ mA} \times 3k - 1.087 \text{ mA} \times 2k$$

1.07
1.087

$$\approx 4.63 > V_{CE(sat)}$$

active

$$V_{BE} > 0 \quad V_{BC} < 0$$

$$V_{BC} ?$$

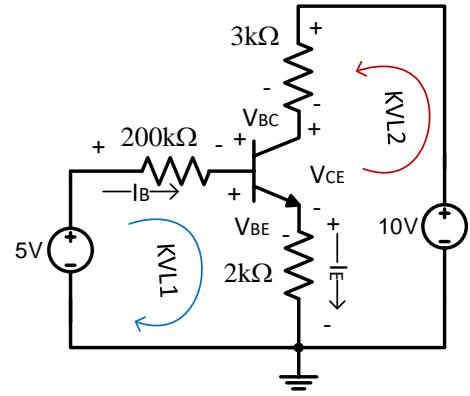
$$? V_{BC} = V_{BE} - V_{CE} ?$$

$$= 0.7 - 4.63 = -3.33$$

$$\begin{aligned}
 I_C &= \beta I_B \\
 &= (100) \cdot (10.7 \mu\text{A}) \\
 &= 1.07 \text{ mA} \\
 I_E &= (\beta + 1) I_B \\
 &= 1.0807 \text{ mA}
 \end{aligned}$$

Now we find V_{CE} from output circuit

$$\begin{aligned}
 10 - I_C \cdot 3 \text{ k}\Omega - I_E \cdot 2 \text{ k}\Omega &= V_{CE} \\
 \Rightarrow V_{CE} &= 4.63 \text{ V} > V_{CE(\text{sat})}
 \end{aligned}$$



\therefore Q1 is in active mode and the assumption is true
 we can also verify that the BC junction is reverse
 biassed which is required so that the BJT operates
 in active mode

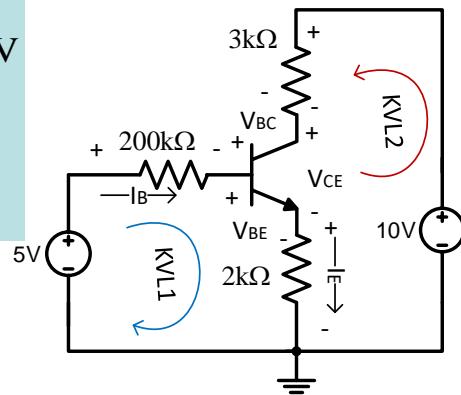
$$10 - I_C \cdot 3 \text{ k}\Omega - I_E \cdot 2 \text{ k}\Omega = V_{CE}$$

$$\Rightarrow V_{CE} = V_{CB} - V_{EB}$$

$$\Rightarrow V_{CB} = V_{CE} - V_{BE} = 4.63 - 0.7 = 3.93 \text{ V}$$

$$\therefore V_{BC} = -V_{CB} = -3.33 \text{ V}$$

BC junction is reverse biased



OR Second method: Assume Saturation

- 1) Since BE junction is forward biased ==> Q1 can be either in Active (Linear) or Saturation mode
- Assume it is in **saturation mode**:

$$10 - I_{C(sat)} \cdot 3k\Omega - I_{E(sat)} \cdot 2k\Omega = V_{CE(Sat)}$$

assume $I_{E(sat)} = I_{C(sat)}$

$$\therefore I_{C(sat)} = \frac{10 - 0.2}{5k\Omega} = 1.96 \text{ mA}$$

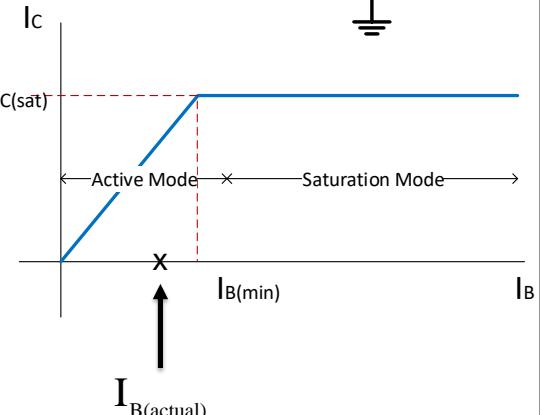
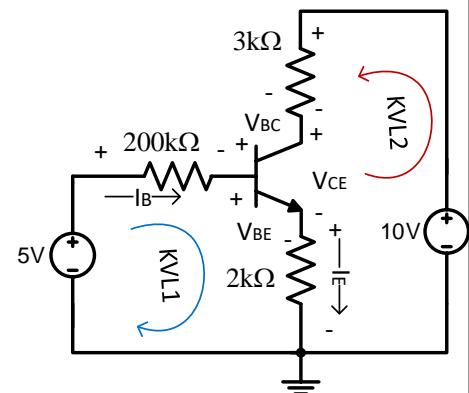
$$I_{B(min)} = \frac{I_{C(sat)}}{\beta} = 19.6 \mu\text{A}$$

Now we find the actual value of I_B

$$I_{B(actual)} = 10.7 \mu\text{A} \text{ (it was found previously)}$$

since

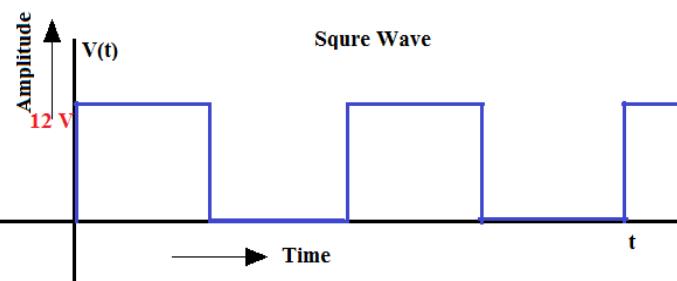
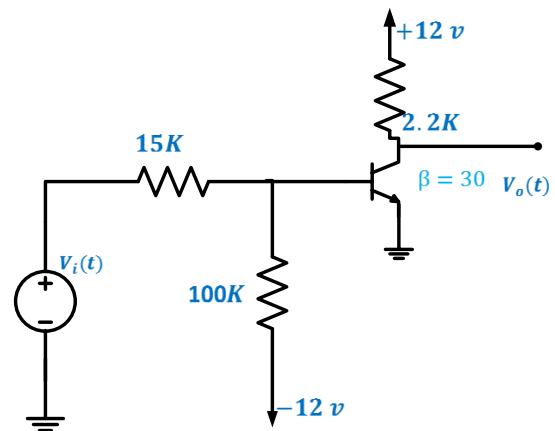
$I_{B(actual)} < I_{B(sat)} = I_{B(min)}$ \Rightarrow the assumption made earlier that BJT in saturation mode is wrong , and actually it is in active mode



BJT as switch:

Example:

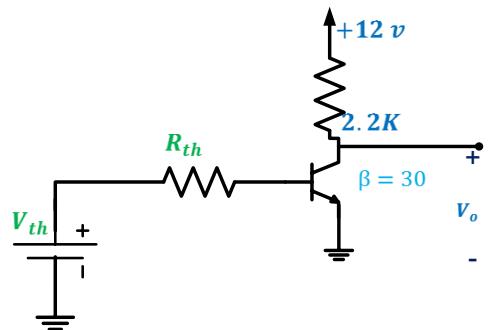
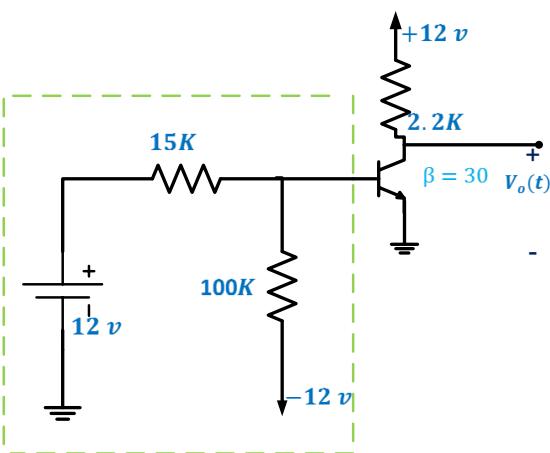
Find $V_o(t)$ for the input given below:



Solution:

❖ Let $V_i(t) = +12 \text{ volt}$

Calculate V_{th} & R_{th}



$$R_{th} = 15k // 100k = \frac{100k * 15k}{15k + 100k} = 13k$$

$$V_{th} = 8.9 \text{ volt} \quad \text{Proof!!}$$



Since the base emitter junction is **forward** bias; the transistor could be either in the **active** or the **saturation** region

➤ Assume that the transistor is in the **saturation** region

$$I_C = I_{C,sat} = \frac{V_{CC} - V_{CE,sat}}{R_C} = \frac{12 - 0.2}{2.2k} = 5.36 \text{ mA}$$

$$I_B(\min) = \frac{I_{C,sat}}{\beta} = \frac{5.36mA}{30} = 0.18mA$$

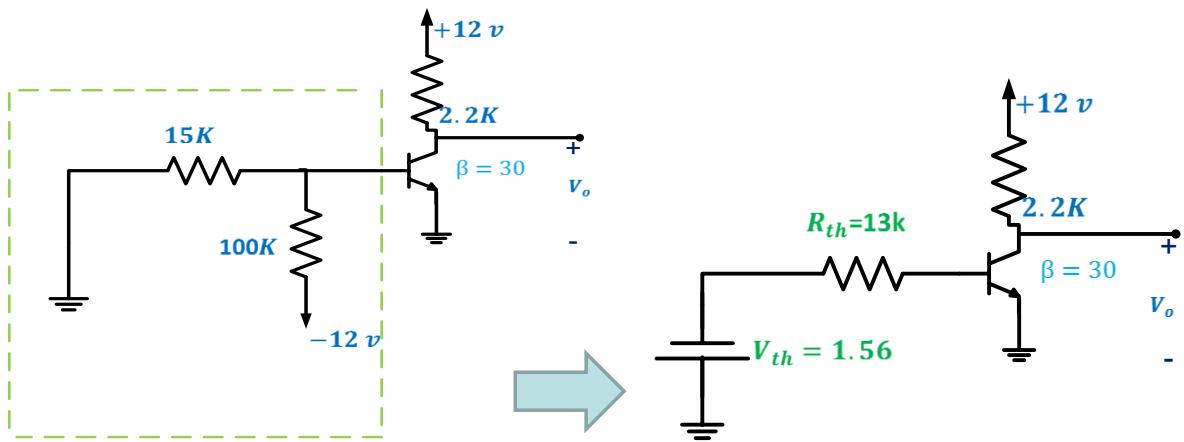
$$I_B = \frac{V_{th} - V_{BE}}{R_{TH}} = \frac{8.9 - 0.8}{13k} = 0.62 \text{ mA}$$

✚ Since $I_B > I_B(\min)$ the transistor is in the **saturation** region.

✓ $V_o = V_{CE,sat} = 0.2 \text{ volt}$

✓ $I_C = 5.36 \text{ mA}$

❖ Let $V_i(t) = 0 \text{ volt}$



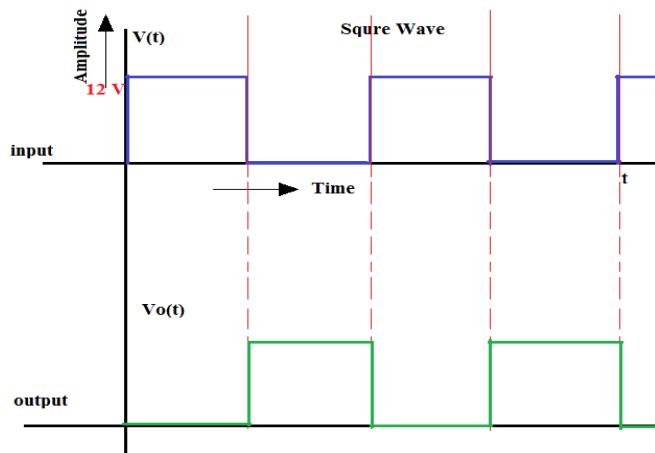
Since $V_{th} = -1.56 \text{ volt}$

Base emitter junction is reverse biased the transistor in cutoff region

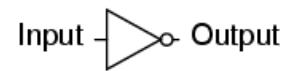
✓ $V_o = V_{CE} = 12 \text{ volt}$

✓ $I_C = 0 \text{ mA}$

The circuit acts as inverter or not gate



NOT gate truth table



Input	Output
0	1
1	0