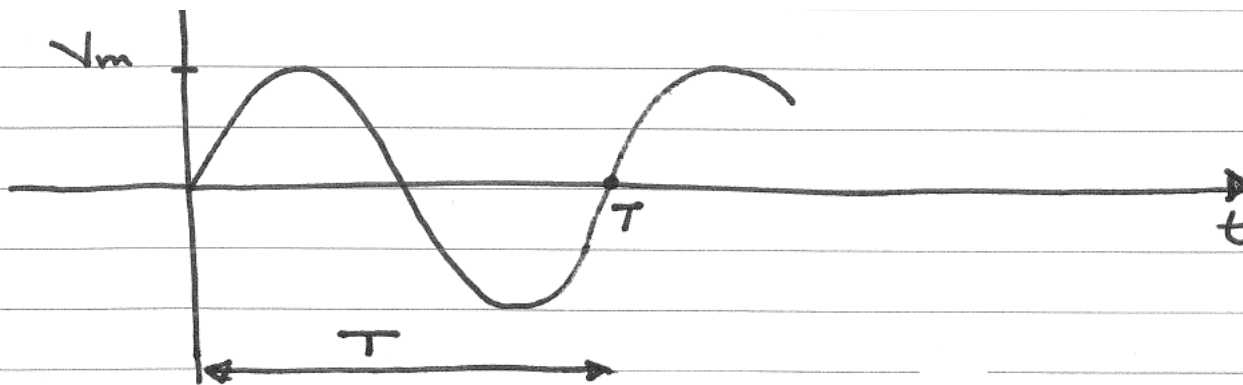
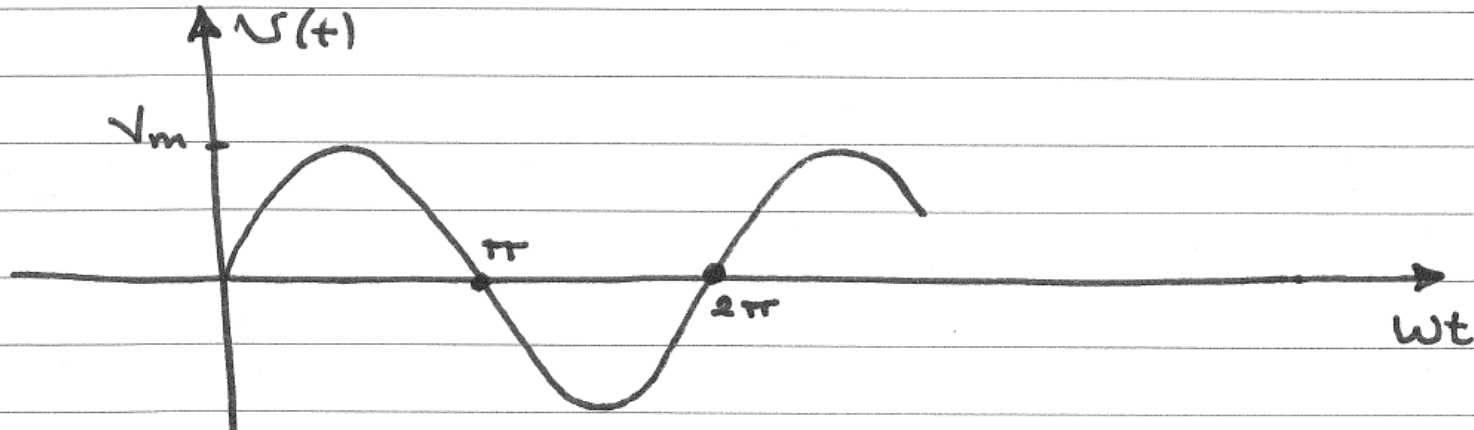


ENEE2301

SINUSOIDAL STEADY-STATE ANALYSIS

CH 9

Sinusoidal Steady – State Analysis

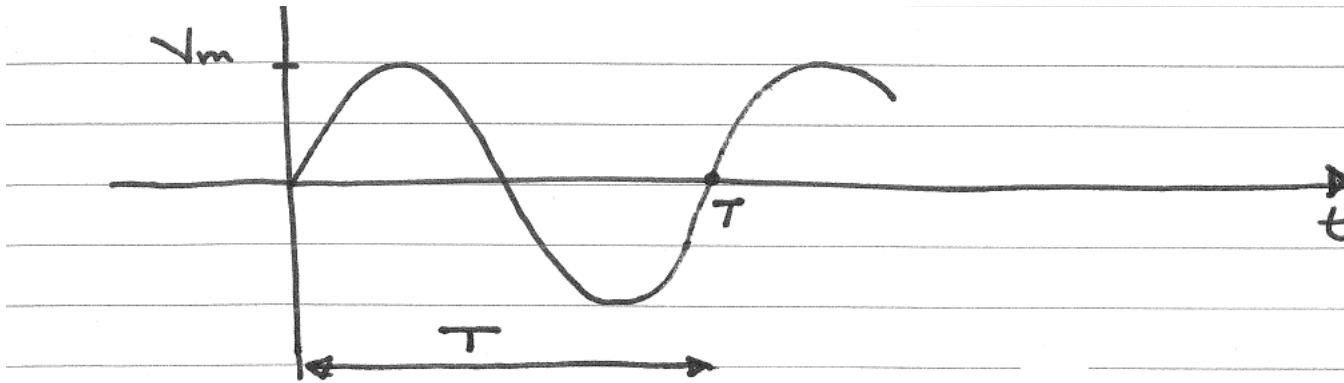


$$v_s(t) = V_m \sin \omega t$$

$V_m \equiv$ Amplitude of the sinusoid

$\omega \equiv$ Angular frequency in radian/s

Sinusoidal Steady – State Analysis



$$\omega = 2\pi f$$

$$f = \frac{1}{T}$$

$f \equiv$ frequency in Hertz

$T \equiv$ period in seconds

PHASE OF SINUSOIDS

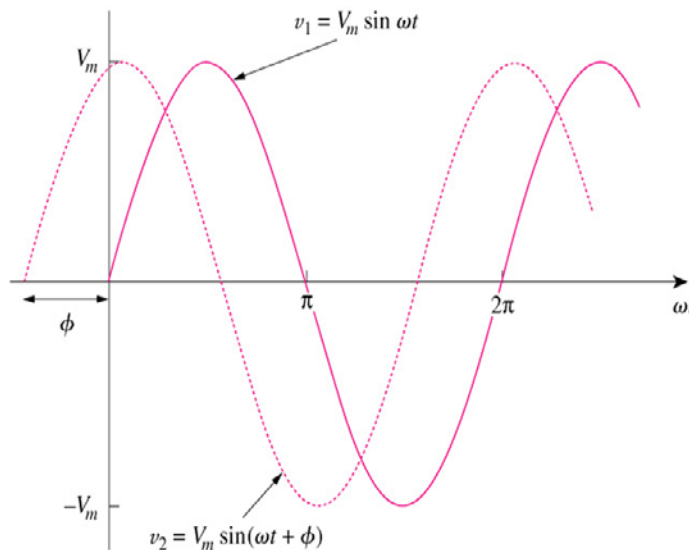
- The term lead and lag are used to indicate the relationship between two sinusoidal wave forms of the same frequency plotted on the same set of axes.

$$V_1 = V_m \sin \omega t$$

$$V_2 = V_m \sin(\omega t + \theta)$$

$\therefore V_2$ leads V_1 by θ or V_1 lags V_2 by θ

➤ Consider the sinusoidal voltage having phase ϕ , $v(t) = V_m \sin(\omega t + \phi)$



- v_2 LEADS v_1 by phase ϕ .
- v_1 LAGS v_2 by phase ϕ .
- v_1 and v_2 are out of phase.

Trigonometric identities :

$$\sin(A \mp B) = \sin A \cos B \mp \cos A \sin B$$

$$\cos(A \mp B) = \cos A \cos B \pm \sin A \sin B$$

$$\sin(\omega t \mp 180^\circ) = -\sin \omega t$$

$$\cos(\omega t \mp 180^\circ) = -\cos \omega t$$

$$\sin(\omega t \mp 90^\circ) = \mp \cos \omega t$$

$$\cos(\omega t \mp 90^\circ) = \pm \sin \omega t$$

$$A \cos \omega t + B \sin \omega t = C \cos(\omega t - \theta)$$

where

$$C = \sqrt{A^2 + B^2} \quad \text{And} \quad \theta = \tan^{-1} \frac{B}{A}$$

Phase and Phase Angle

* We usually use *cosine function* to model a sinusoidal signal.

In case there is a sine function, we can use the following conversion:

$$\sin(z) = \cos(z - 90)$$

For example :

$$v_x(t) = 10 \sin(200t + 30^\circ)$$

$$\begin{aligned} v_x(t) &= 10 \cos(200t + 30^\circ - 90^\circ) \\ &= 10 \cos(200t - 60^\circ) \end{aligned}$$

and thus we can say that the phase angle of $v_x(t)$ is -60°

Examples :

1) let

$$V1(t) = 10 \sin(5t - 30^\circ) \quad , \quad V2(t) = 15 \sin(5t + 10^\circ)$$

$\therefore V2(t)$ leads $V1(t)$ by 40°

2) let

$$i1(t) = 2 \sin(377t + 45^\circ)$$

$$i2(t) = 0.5 \cos(377t + 10^\circ)$$

$$\cos \alpha = \sin(\alpha + 90^\circ)$$

$$0.5 \cos(377t + 10^\circ) = 0.5 \sin(377t + 100^\circ)$$

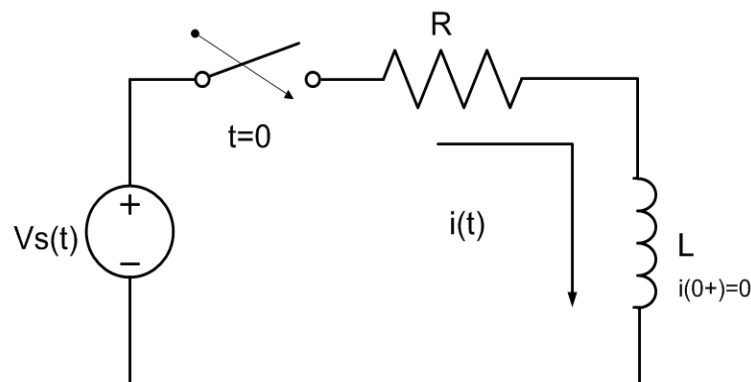
$\therefore i2(t)$ leads $i1(t)$ by 55°

The sinusoidal response :

find $i(t)$ for $t > 0$

given

$$V_s(t) = V_m \cos \omega t \text{ volt.}$$



Solution

KVL:

$$V_s(t) = Ri(t) + L \frac{di(t)}{dt}$$

$$V_m \cos \omega t = Ri(t) + L \frac{di(t)}{dt}$$

$$\therefore i(t) = i_n(t) + i_f(t)$$

$$i(t) = Ae^{-\frac{t}{\tau}} + i_f(t)$$

$$i_f(t) = I_1 \cos \omega t + I_2 \sin \omega t$$

first order non homogenous differential equation .

To find I_1 and I_2 :

$$V_m \cos \omega t = Ri(t) + L \frac{di(t)}{dt}$$

$$V_m \cos \omega t = R[I_1 \cos \omega t + I_2 \sin \omega t] + L\omega[-I_1 \sin \omega t + I_2 \cos \omega t]$$

collect the sine and cosine terms

$$0 = [-L\omega I_1 + RI_2] \sin \omega t + [L\omega I_2 + RI_1 - V_m] \cos \omega t$$

$$-\omega LI_1 + RI_2 = 0$$

$$\omega LI_2 + RI_1 - V_m = 0$$

$$I_1 = \frac{RV_m}{R^2 + \omega^2 L^2}$$

$$I_2 = \frac{\omega LV_m}{R^2 + \omega^2 L^2}$$

$$i(t) = \frac{RV_m}{R^2 + \omega^2 L^2} \cos \omega t + \frac{\omega LV_m}{R^2 + \omega^2 L^2} \sin \omega t$$

$$i(t) = I_1 \cos \omega t + I_2 \sin \omega t$$

$$i(t) = C \cos(\omega t - \phi)$$

$$i(t) = C \cos \omega t \cos \phi + C \sin \omega t \sin \phi$$

$$\therefore I_1 = C \cos \phi$$

$$I_2 = C \sin \phi$$

$$\frac{I_2}{I_1} = \tan \phi$$

$$\phi = \tan^{-1} \frac{I_2}{I_1} = \tan^{-1} \frac{\omega L}{R} \rightarrow \rightarrow (1)$$

$$I_1^2 + I_2^2 = C^2 \cos^2 \phi + C^2 \sin^2 \phi$$

$$I_1^2 + I_2^2 = C^2$$

$$C = \sqrt{I_1^2 + I_2^2}$$

$$C = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} \rightarrow \rightarrow (2)$$

$$i_f(t) = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} \cos \left(\omega t - \tan^{-1} \frac{\omega L}{R} \right)$$

$$I_1 = C \cos \phi$$

$$I_2 = C \sin \phi$$

$$\frac{I_2}{I_1} = \tan \phi$$

$$I_1 = \frac{RV_m}{R^2 + \omega^2 L^2}$$

$$I_2 = \frac{\omega LV_m}{R^2 + \omega^2 L^2}$$

$$\therefore i(t) = Ae^{-\frac{t}{\tau}} + \frac{Vm}{\sqrt{R^2 + \omega^2 L^2}} \cos\left(\omega t - \tan^{-1} \frac{\omega L}{R}\right)$$

$$i(0^+) = A + \frac{Vm}{\sqrt{R^2 + \omega^2 L^2}} \cos\left(-\tan^{-1} \frac{\omega L}{R}\right) = 0$$

$$\therefore A = -\frac{Vm}{\sqrt{R^2 + \omega^2 L^2}} \cos\left(-\tan^{-1} \frac{\omega L}{R}\right)$$

$$i(t) = i_n(t) + i_f(t)$$

$i(t) = \text{transient component} + \text{steady-state component}$

the steady state solution is a sinusoidal function with the same frequency as the source signal.

R-L Circuit

If $V_s(t) = V_m \cos(\omega t + \phi)$

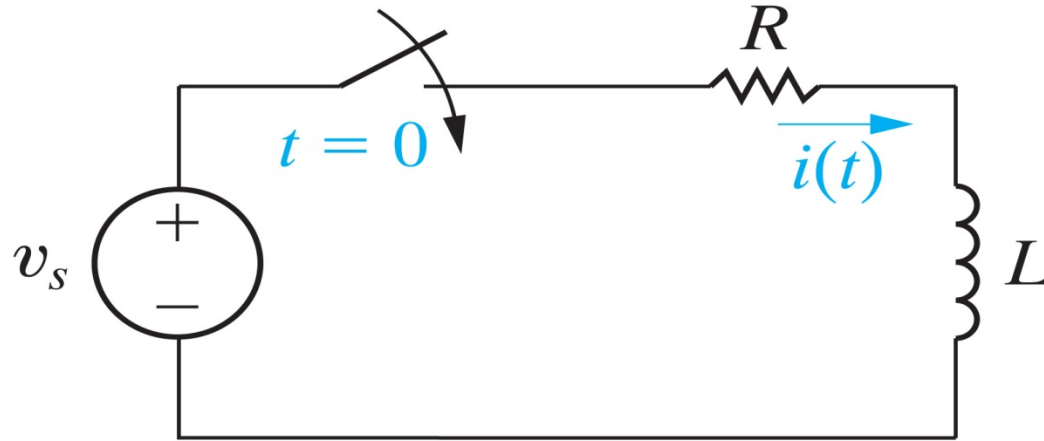


Figure: 09-05

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$$L \frac{di}{dt} + Ri = V_m \cos(\omega t + \phi)$$

$$i = \frac{-V_m}{\sqrt{R^2 + \omega^2 L^2}} \cos(\phi - \theta) e^{-(R/L)t} + \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}} \cos(\omega t + \phi - \theta)$$

$$\theta = \tan^{-1} \frac{\omega L}{R}$$

Transient

Steady-state

Complex Numbers:

a complex number may be written in three forms :

1) rectangular form : $Z = X + jY$

$$j = \sqrt{-1} \quad ,$$

$$X = RE\{Z\} \quad ,$$

$$Y = Im\{Z\}$$

2) Exponential form : $Z = |Z|e^{j\theta}$

$$|Z| = \text{magnitude} \quad , \theta = \text{angle}$$

3) Polar form $Z = |Z|\angle\theta$

Euler's law: $e^{j\theta} = \cos \theta + j \sin \theta$

1 - Conversion from polar to rectangular form

$$Z = |Z|e^{j\theta}$$

$$Z = |Z| \cos \theta + j|Z| \sin \theta$$

$$Z = X + jY$$

$$X = |Z| \cos \theta$$

$$Y = |Z| \sin \theta$$

2 - Conversion from rectangular to polar form

$$X^2 + Y^2 = |Z|^2 \cos^2 \theta + |Z|^2 \sin^2 \theta$$

$$X^2 + Y^2 = |Z|^2 [\cos^2 \theta + \sin^2 \theta]$$

$$X^2 + Y^2 = |Z|^2$$

$$\therefore |Z| = \sqrt{X^2 + Y^2}$$

$$\frac{Y}{X} = \frac{|Z| \sin \theta}{|Z| \cos \theta} = \tan \theta \implies \therefore \theta = \tan^{-1} \frac{Y}{X}$$

Mathematical operation of complex numbers:

1) Addition : $Z_1 + Z_2 = (X_1 + X_2) + j(Y_1 + Y_2)$

2) Subtraction: $Z_1 - Z_2 = (X_1 - X_2) + j(Y_1 - Y_2)$

3) Multiplication: $Z_1 Z_2 = |Z_1||Z_2|\angle\theta_1 + \theta_2$

4) Division: $\frac{Z_1}{Z_2} = \frac{|Z_1|}{|Z_2|}\angle\theta_1 - \theta_2$

5) Complex Conjugate:

$$\text{If } Z = X + jY = |Z|\angle + \theta$$

$$Z^* = X - jY \quad \text{OR} \quad Z^* = |Z|\angle - \theta$$

Example $Z1 = 4 + j3 = 5\angle 36.9^\circ$

$$Z2 = 3 + j4 = 5\angle 53.1^\circ$$

$$Z1 + Z2 = 7 + j7$$

$$Z1 - Z2 = 1 - j1$$

$$Z1 Z2 = 5\angle 36.9^\circ \cdot 5\angle 53.1^\circ = 25\angle 90^\circ$$

$$\frac{Z1}{Z2} = \frac{5\angle 36.9^\circ}{5\angle 53.1^\circ} = 1\angle -16.2^\circ$$

OR

$$Z1 Z2 = (4 + j3)(3 + j4)$$

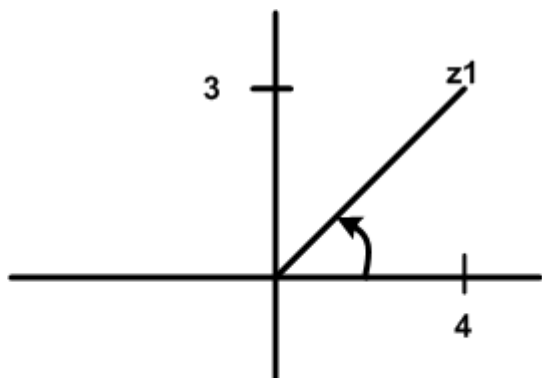
$$= 12 + j16 + j9 - 12$$

$$Z1 Z2 = j25$$

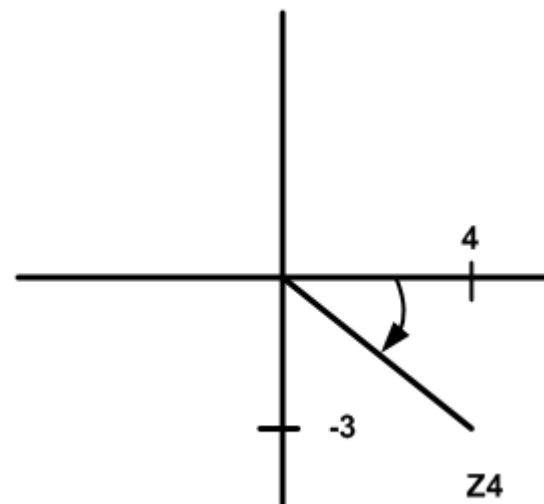
$$\frac{Z1}{Z2} = \frac{4 + j3}{3 + j4} \cdot \frac{3 - j4}{3 - j4} = \frac{12 - j16 + j9 + 12}{25} = \frac{24 - j7}{25}$$

$$\frac{Z1}{Z2} = \frac{24}{25} - j\frac{7}{25}$$

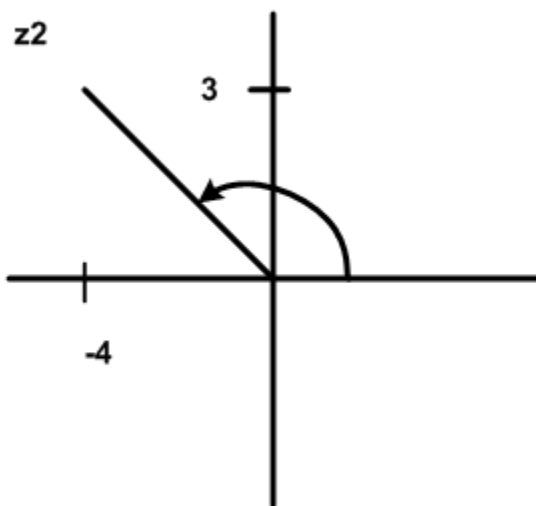
THE GRAPHICAL REPRESENTATION



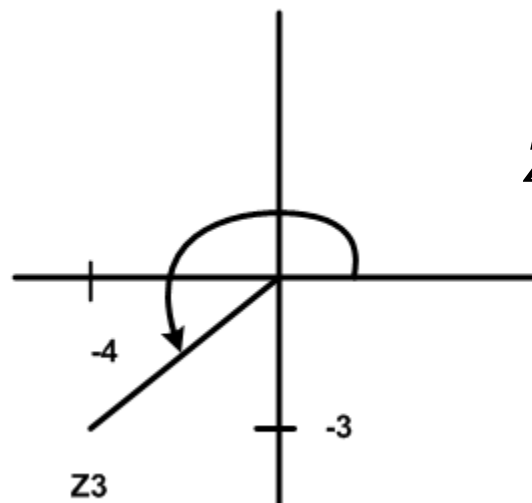
$$Z_1 = 4 + j3$$
$$Z_1 = 5 \angle 36.9^\circ$$



$$Z_4 = 4 - j3$$
$$Z_4 = 5 \angle -36.9^\circ$$

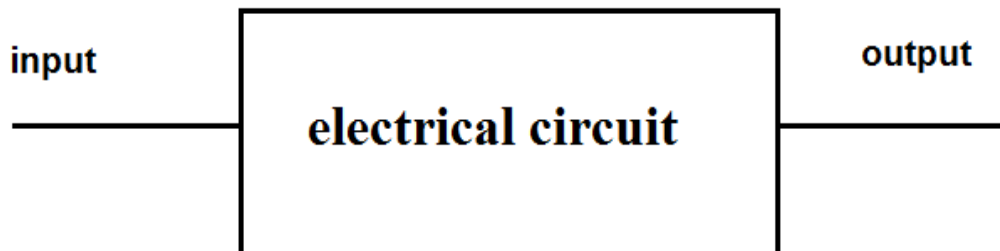


$$Z_2 = -4 + j3$$
$$Z_2 = 5 \angle 143.1^\circ$$



$$Z_3 = -4 - j3$$
$$Z_3 = 5 \angle 216.9^\circ$$

The phasor concept



$$Vm \cos(\omega t + \theta) \longrightarrow Im \cos(\omega t + \phi)$$

$$Vm \sin(\omega t + \theta) \longrightarrow Im \sin(\omega t + \phi)$$

$$jVm \sin(\omega t + \theta) \longrightarrow j Im \sin(\omega t + \phi)$$

$$Vm \cos(\omega t + \theta) + jVm \sin(\omega t + \theta) \longrightarrow Im \cos(\omega t + \phi) + j Im \sin(\omega t + \phi)$$

$$Vm e^{j(\omega t + \theta)} \longrightarrow Im e^{j(\omega t + \phi)}$$

- Instead of applying a real forcing function to obtain the desired real response , we apply a **complex forcing function** whose real part is the given real forcing function.

- we obtain a complex response whose **real part** is the desired real response.

Sinusoidal and Complex forcing function:

$$V_s(t) = V_m \cos \omega t$$

$$\therefore i(t) = I_m \cos(\omega t + \phi)$$

The steady – state response

$$V_s(t) \rightarrow V_m e^{j\omega t}$$

$$i(t) \rightarrow I_m e^{j(\omega t + \phi)}$$

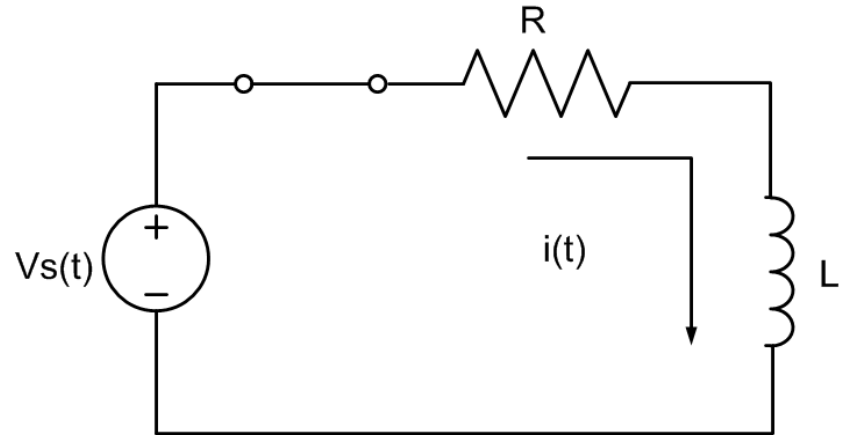
$$KVL: \quad V_s(t) = Ri(t) + L \frac{di(t)}{dt}$$

$$V_m e^{j\omega t} = RI_m e^{j(\omega t + \phi)} + j\omega L I_m e^{j(\omega t + \phi)}$$

a complex algebraic equation .
to find I_m and ϕ ;devide by $e^{j\omega t}$

$$V_m = RI_m e^{j\phi} + j\omega L I_m e^{j\phi}$$

$$V_m = I_m e^{j\phi} (R + j\omega L)$$



$$\therefore I_m e^{j\phi} = \frac{V_m}{R + j\omega L}$$

$$I_m e^{j\phi} = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2} e^{j \tan^{-1} \frac{\omega L}{R}}}$$

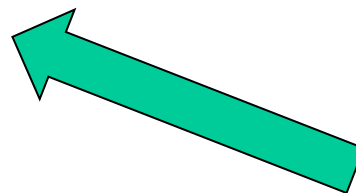
$$Im e^{j\phi} = \frac{Vm}{\sqrt{R^2 + \omega^2 L^2}} e^{-j \tan^{-1} \frac{\omega L}{R}}$$

$$\therefore Im = \frac{Vm}{\sqrt{R^2 + \omega^2 L^2}}$$

$$\phi = -\tan^{-1} \frac{\omega L}{R}$$

$$i(t) = Im \cos(\omega t + \phi)$$

$$i(t) = \frac{Vm}{\sqrt{R^2 + \omega^2 L^2}} \cos(\omega t + \phi)$$



The steady – state response

Phasors:

Given the sinusoids $i(t) = I_m \cos(\omega t + \phi_i)$

$$V(t) = V_m \cos(\omega t + \theta_v).$$

we can obtain the phasor forms as:

$$i(t) = I_m \cos(\omega t + \phi_i)$$

$$\text{then } \vec{I} = I_m \angle \phi_i$$

$$V(t) = V_m \cos(\omega t + \theta_v)$$

$$\text{then } \vec{V} = V_m \angle \theta_v.$$

$$V(t) = -4 \sin(30t + 50^\circ) V.$$

$$\cos(\omega t \mp 90) = \pm \sin \omega t$$

$$V(t) = 4 \cos(30t + 140) V.$$

$$\therefore \vec{V} = 4 \angle 140^\circ V.$$

Phasor relationships for circuit elements:

1) Resistor :

$$V(t) = Ri(t)$$

$$Vm e^{j(\omega t + \theta v)} = RIm e^{j(\omega t + \phi i)}$$

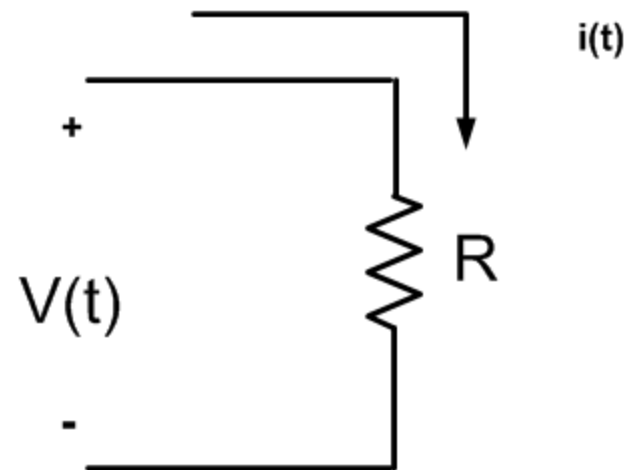
$$Vm e^{j\theta v} = RIm e^{j\phi i}$$

$$Vm \angle \theta v = RIm \angle \phi i$$

$$\vec{V} = R\vec{I}$$

$$Vm = RIm$$

$$\theta v = \phi i$$



■ *voltage and current of a resistor are in phase*

2) Inductor:

$$V(t) = L \frac{di(t)}{dt}$$

$$Vm e^{j(\omega t + \theta v)} = L \frac{d}{dt} (Im e^{j(\omega t + \phi i)})$$

$$Vm e^{j(\omega t + \theta v)} = j\omega L Im e^{j(\omega t + \phi i)}$$

$$Vm e^{j\theta v} = j\omega L Im e^{j\phi i}$$

$$Vm \angle \theta v = j\omega L Im \angle \phi i$$

$$\vec{V} = j\omega L \vec{I}$$

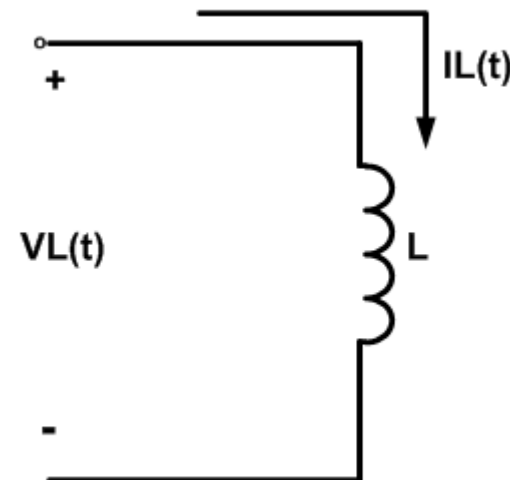
$$Vm \angle \theta v = \omega L \angle 90^\circ \cdot Im \angle \phi i$$

$$Vm \angle \theta v = \omega L Im \angle \phi i + 90^\circ$$

$$\therefore Vm = \omega L Im$$

$$\theta v = \phi i + 90^\circ$$

■ **The voltage leads the current by 90° .**



3. Capacitor

$$i(t) = C \frac{dV(t)}{dt}$$

$$Im e^{j(\omega t + \phi_i)} = C \frac{d}{dt} (Vm e^{j(\omega t + \theta_v)})$$

$$Im e^{j(\omega t + \phi_i)} = j\omega C Vm e^{j(\omega t + \theta_v)}$$

$$Im e^{j\phi_i} = j\omega C Vm e^{j\theta_v}$$

$$Im \angle \phi_i = j\omega C Vm \angle \theta_v$$

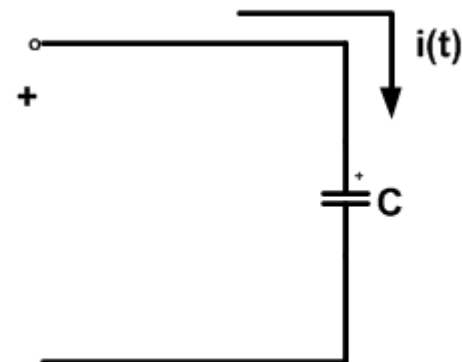
$$\vec{I} = j\omega C \vec{V}$$

$$Im \angle \phi_i = \omega C \angle 90^\circ \cdot Vm \angle \theta_v$$

$$Im \angle \phi_i = \omega C Vm \angle \theta_v + 90^\circ$$

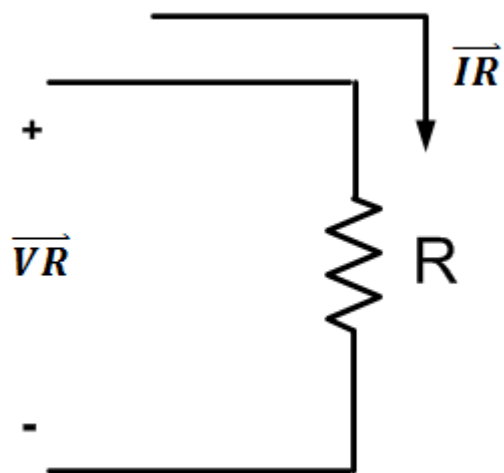
$$Im = \omega C Vm$$

$$\phi_i = \theta_v + 90^\circ$$

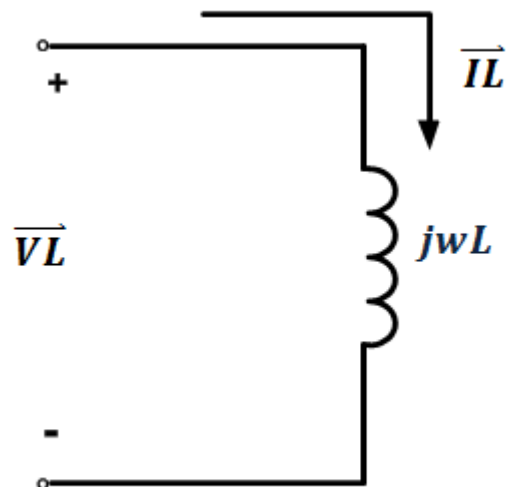


■ *The current leads the voltage by 90°*

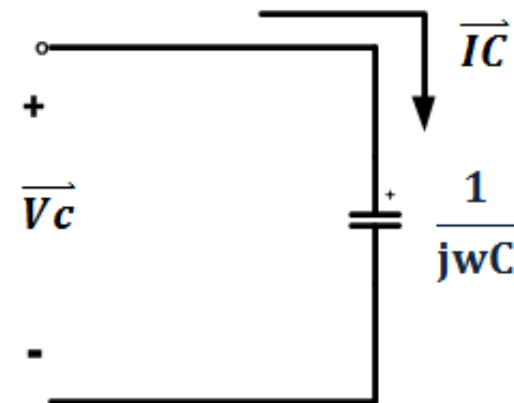
Phasor Relationships for circuit elements



$$\vec{V}_R = R * \vec{I}_R$$



$$\vec{V}_L = j\omega L * \vec{I}_L$$



$$\vec{V}_C = \frac{1}{j\omega C} \vec{I}_C$$

$$\vec{V} = Z(j\omega) \vec{I}$$

Impedance and Admittance:

$$\mathbf{Z}(j\omega) = \frac{\vec{V}}{\vec{I}} ; \text{ Impedance in } \Omega$$

Or

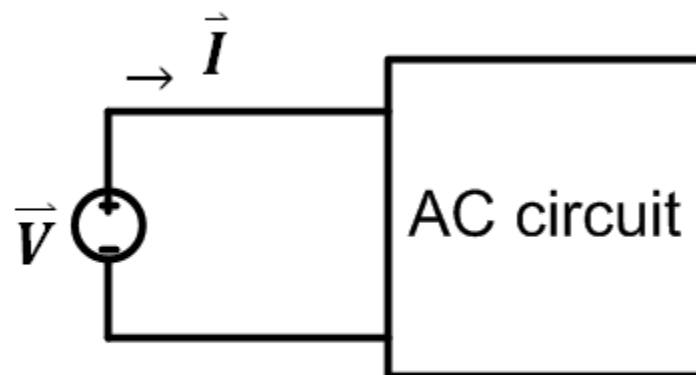
$$\vec{V} = \mathbf{Z}(j\omega) \cdot \vec{I}$$

$$\mathbf{Y}(j\omega) = \frac{\vec{I}}{\vec{V}} ; \text{ Admittance in Siemens}$$

Or

$$\vec{I} = \mathbf{Y}(j\omega) \cdot \vec{V}$$

$$\mathbf{Z}(j\omega) = \frac{\mathbf{1}}{\mathbf{Y}(j\omega)}$$



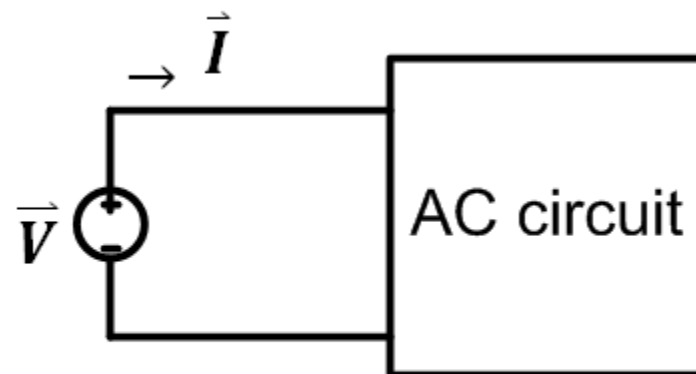
Element	Impedance	Admittance
R	$Z(j\omega) = R$	$Y(j\omega) = \frac{1}{R}$
C	$Z(j\omega) = \frac{1}{j\omega C}$	$Y(j\omega) = j\omega C$
L	$Z(j\omega) = j\omega L$	$Y(j\omega) = \frac{1}{j\omega L}$

Impedance : $Z(j\omega)$

$$Z(j\omega) = \frac{\vec{V}}{\vec{I}} = \frac{Vm\angle\theta v}{Im\angle\theta i}$$

$$Z(j\omega) = \frac{Vm}{Im} \angle\theta v - \theta i$$

$$Z(j\omega) = |Z|\angle\theta z$$



The unit of impedance is ohm

Impedance is not a phasor but a complex number that can be written in polar or Cartesian forms.

$$\vec{Z} = R + jX$$

$R \equiv$ Real part

$X \equiv$ Reactive part.

$$Z = |Z| \angle \theta_z$$

Or

$$Z = R + jX$$

$$|Z| = \sqrt{R^2 + X^2} \quad \text{magnitude}$$

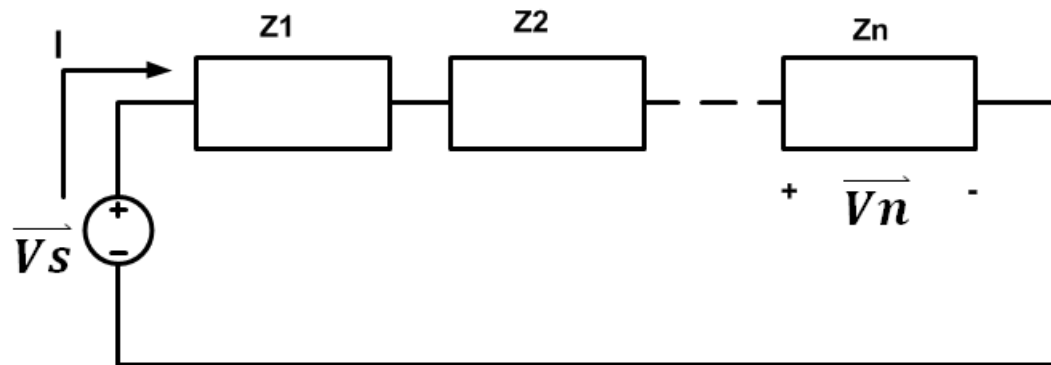
$$\theta_z = \tan^{-1} \frac{X}{R} \quad \text{phase}$$

Where,

$$X = |Z| \sin \theta_z$$

$$R = |Z| \cos \theta_z$$

Application of KVL for Phasors



KVL :

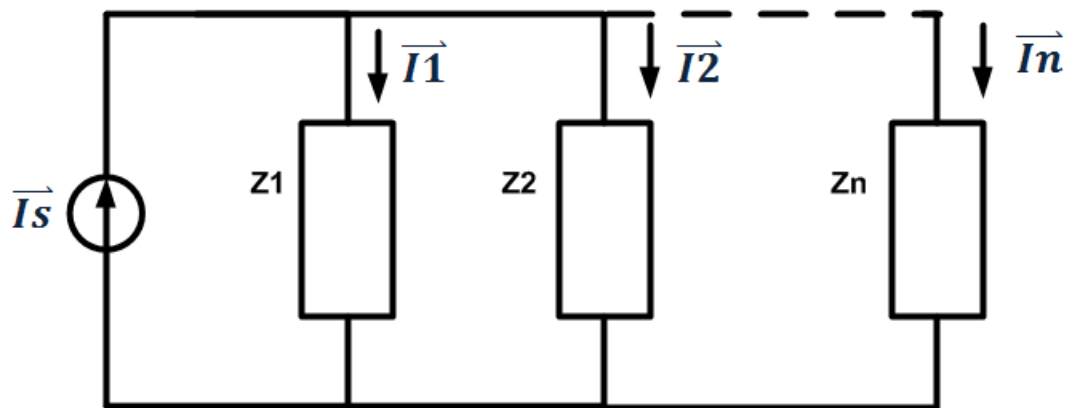
$$V_s(t) = V_1(t) + V_2(t) + \dots V_n(t)$$

$$\vec{V}_s = \vec{V}_1 + \vec{V}_2 + \dots \vec{V}_n$$

$$Z_{eq} = Z_1 + Z_2 + Z_3 + \dots Z_n$$

$$\vec{V}_n = \frac{Z_n}{Z_1 + Z_2 + Z_3 + \dots Z_n} \cdot \vec{V}_s$$

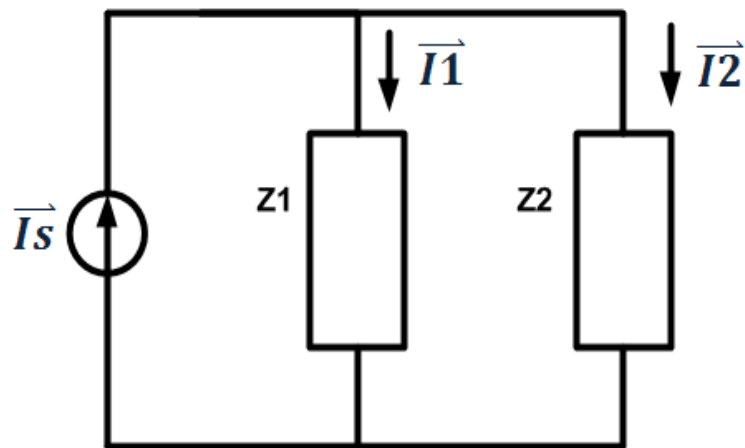
Application of KCL for phasors



KCL:

$$\vec{I}_s = \vec{I}_1 + \vec{I}_2 + \dots + \vec{I}_n$$

Current Divider :



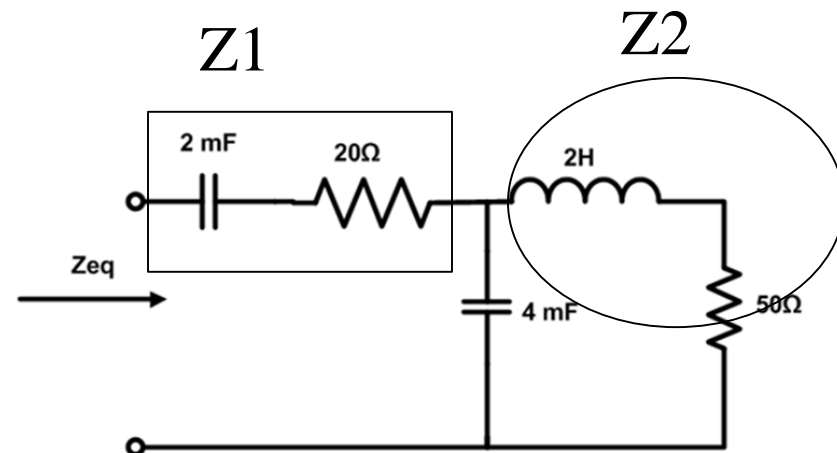
$$\vec{I}_1 = \frac{Z_2}{Z_1 + Z_2} \cdot \vec{I}_s$$

$$\vec{I}_2 = \frac{Z_1}{Z_1 + Z_2} \cdot \vec{I}_s$$

Find Z_{eq}

$$Z_C(j\omega) = \frac{1}{j\omega C}$$

$$Z_L(j\omega) = j\omega L$$



$$\omega = 10 \text{ rad/sec}$$

$$Z1 = 20 + \frac{1}{j(10)(2)(10^{-3})} = 20 - j50$$

$$Z2 = 50 + j(10)(2) = 50 + j20$$

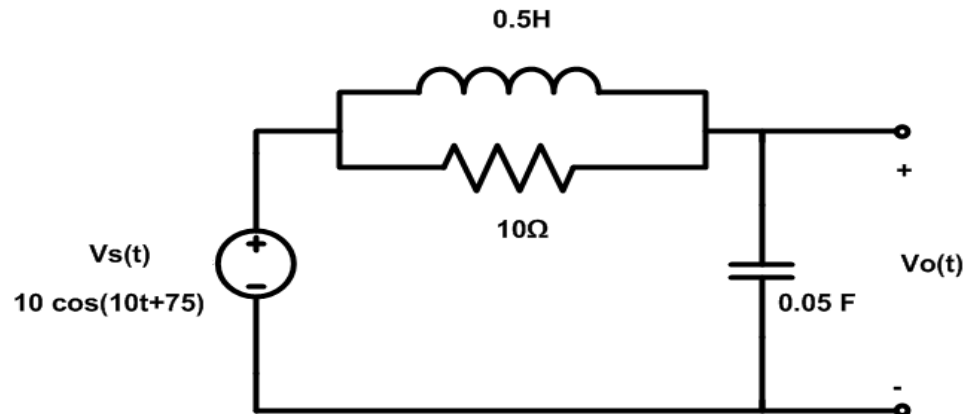
$$Z3 = (50 + j20) \parallel \left(\frac{1}{j(10)(4)(10^{-3})} \right)$$

$$Z3 = (50 + j20) \parallel -j25$$

$$Z3 = \frac{(50 + j20)(-j25)}{50 + j20 - j25} = 12.38 - j23.76$$

$$Z_{eq} = Z1 + Z3 = 32.38 - j73.76 \Omega$$

Calculate $V_o(t)$



$$Z_L(j\omega) = j\omega L = j5 \Omega$$

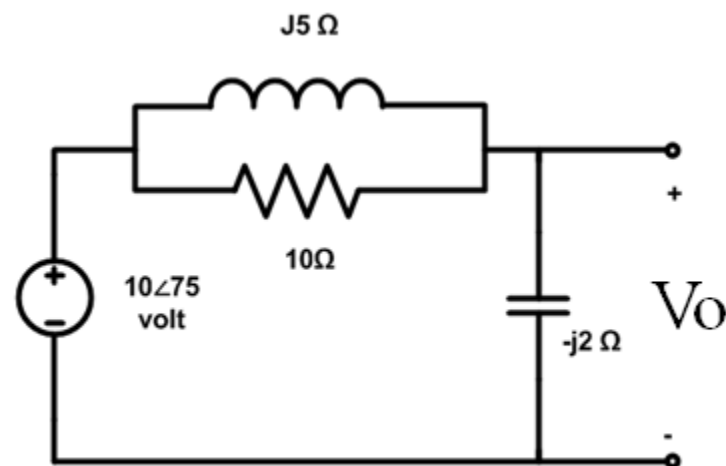
$$Z_C(j\omega) = -j \frac{1}{\omega C} = -j2 \Omega$$

$$\vec{V}_s = 10 \angle 75^\circ \text{ volt}$$

$$\vec{V}_o = \frac{-j2}{-j2 + (10 \parallel j5)} \cdot 10 \angle 75^\circ$$

$$\vec{V}_o = 7.071 \angle -60^\circ \text{ volt}$$

$$\therefore V_o(t) = 7.071 \cos(10t - 60^\circ) \text{ volt}$$



Calculate $i_o(t)$

$$i_s(t) = 0.05 \cos 2000t \text{ A}$$

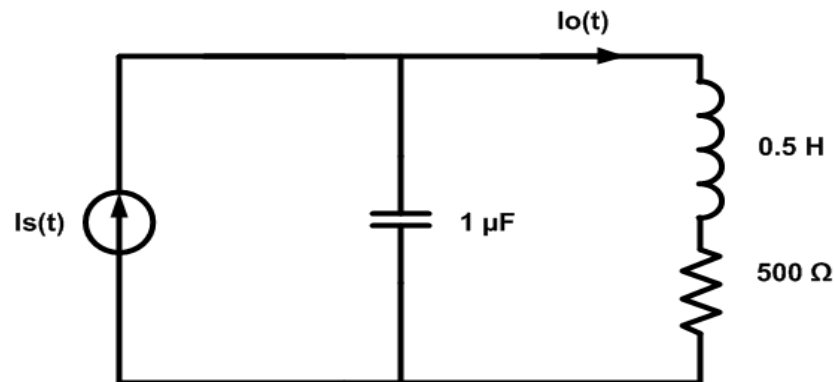
$$Z_C(j\omega) = -j \frac{1}{\omega C} = -j500 \Omega$$

$$Z_L(j\omega) = j\omega L = j1000 \Omega$$

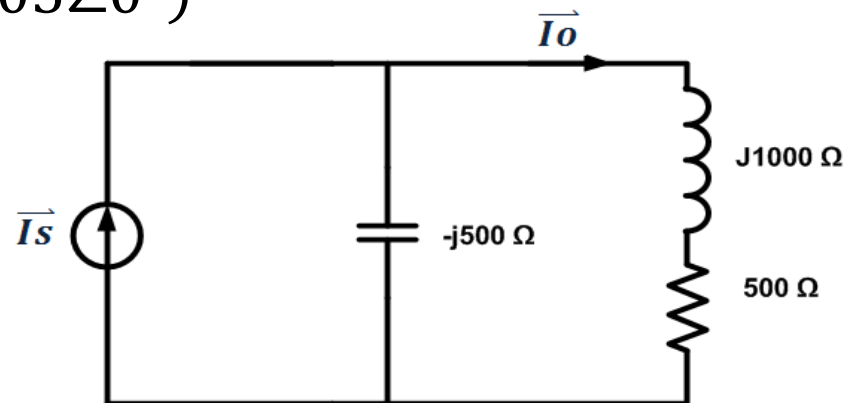
$$\vec{I}_o = \frac{-j500}{-j500 + 500 + j1000} \cdot (0.05 \angle 0^\circ)$$

$$\vec{I}_o = 0.03535 \angle -135^\circ \text{ A}$$

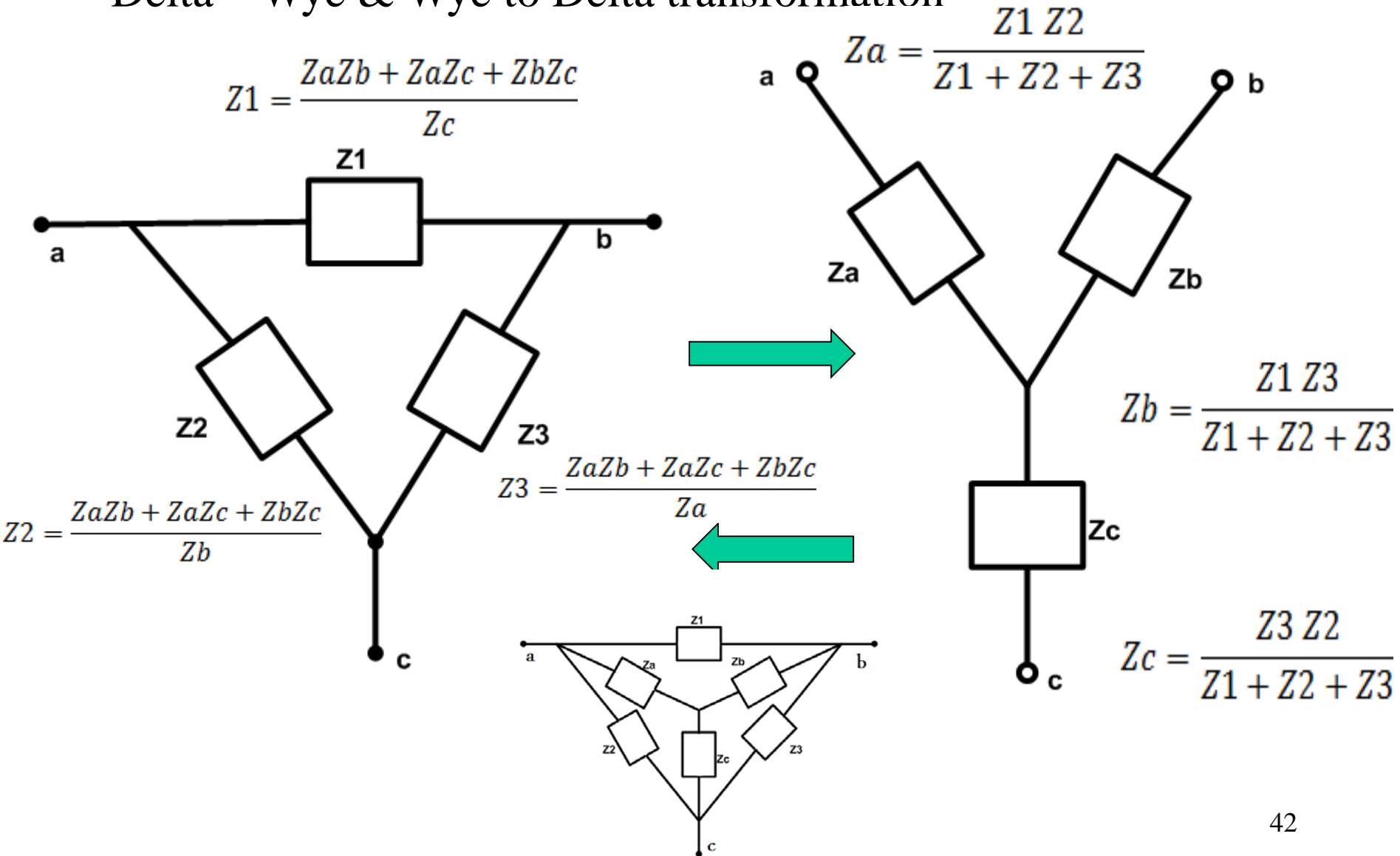
$$\therefore i_o(t) = 0.03535 \cos(2000t - 135^\circ) \text{ A}$$



$$\vec{I}_s = 0.05 \angle 0^\circ \text{ A}$$



Delta – Wye & Wye to Delta transformation



Series RL circuit

$$V_s(t) = 60 \cos(200\pi t) \text{ volt}$$

find $i(t)$

$$\vec{V}_s = \vec{V}_R + \vec{V}_L$$

$$60 \angle 0^\circ = 20 \vec{I} + j12.57 \vec{I}$$

$$\vec{I} = \frac{60 \angle 0^\circ}{20 + j12.57} = \frac{60 \angle 0^\circ}{23.6 \angle 32.1^\circ}$$

$$\therefore \vec{I} = 2.54 \angle -32.1^\circ \text{ A}$$

$$\vec{V}_R = 20 \vec{I} = 50.8 \angle -32.1^\circ \text{ volt}$$

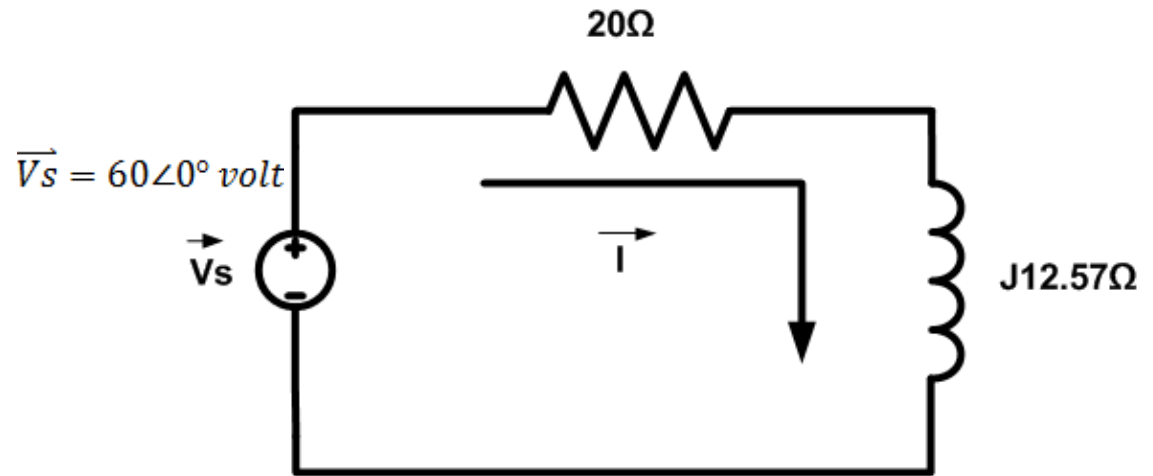
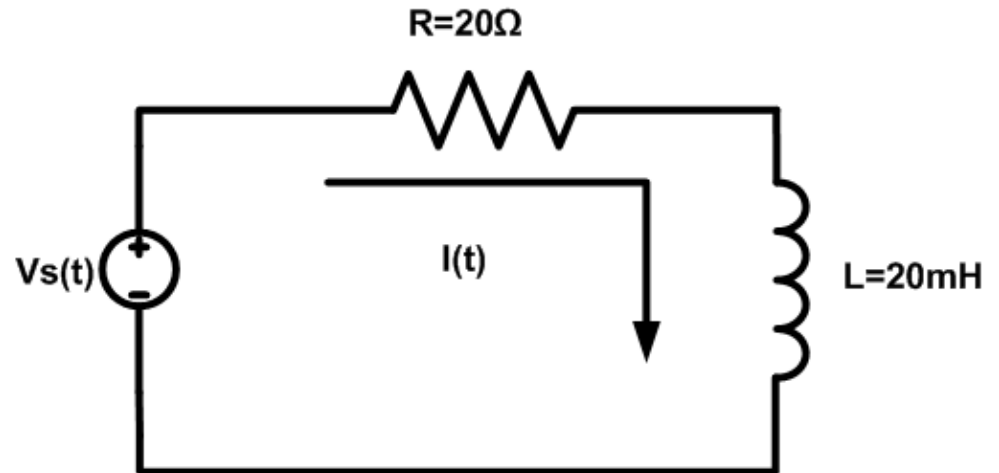
$$\vec{V}_L = j12.57 \vec{I} = 31.9 \angle +57.9^\circ \text{ volt}$$

\vec{V}_L leads \vec{V}_R by 90°

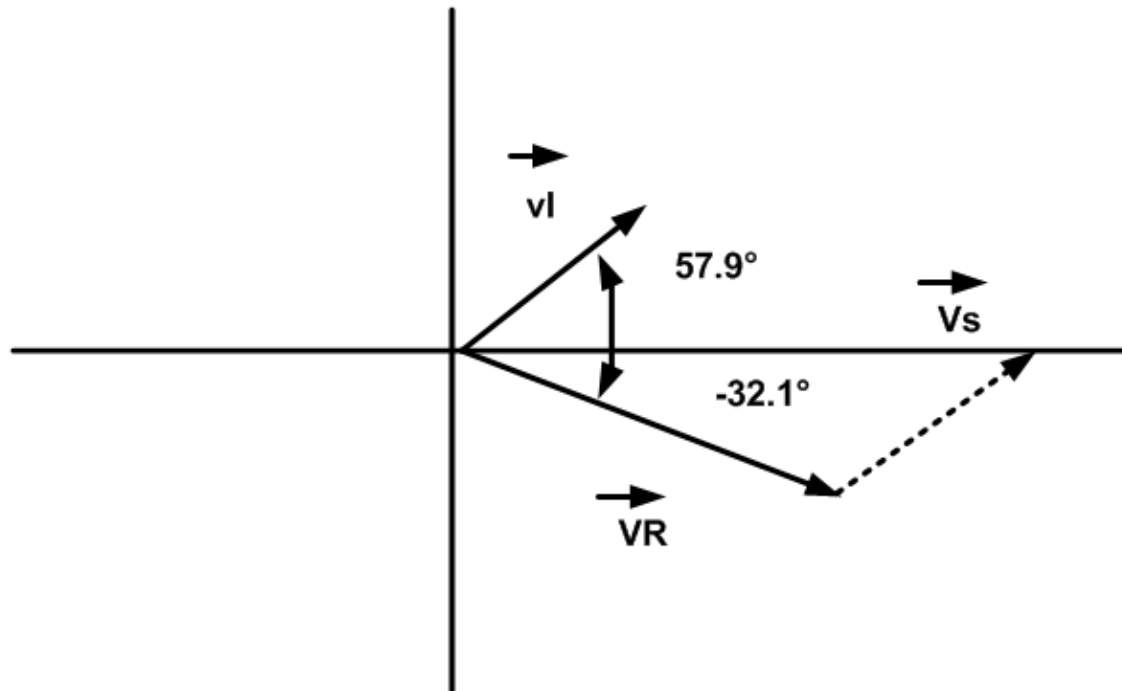
\vec{I} lags \vec{V}_s by 32.1°

$$\begin{aligned} Z_{eq} &= 20 + j12.57 \Omega \\ &= 23.6 \angle 32.1^\circ \Omega \end{aligned}$$

inductive
inductive



Phasor Diagram



Series RC circuit

$$V_s(t) = 100 \cos 600\pi t \text{ volt}$$



$$Z_R(j\omega) = 47 \Omega$$

$$Z_C(j\omega) = -j \frac{1}{\omega C} = -j 53.1 \Omega$$

$$\vec{V}_s = 100 \angle 0^\circ \text{ volt}$$

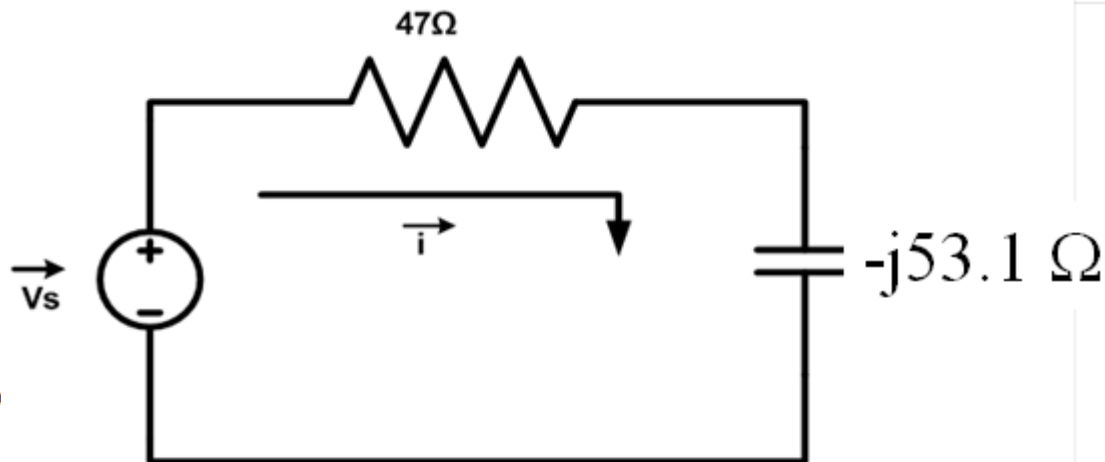
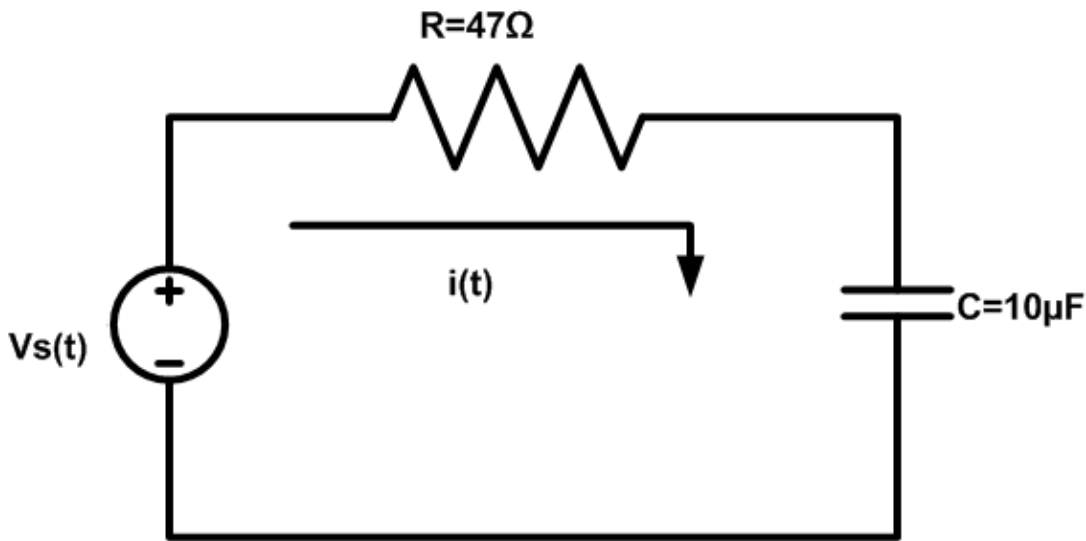
KVL:

$$\vec{V}_s = 47 \vec{I} - j53.1 \vec{I}$$

$$\vec{I} = \frac{\vec{V}_s}{47 - j53.1} = \frac{100 \angle 0^\circ}{47 - j53.1}$$

$$\vec{I} = \frac{100 \angle 0^\circ}{70.9 \angle -48.5^\circ} \longrightarrow \vec{I} = 1.41 \angle 48.5^\circ$$

\vec{I} leads \vec{V}_s by 48.5°



→ *capacitive circuit*

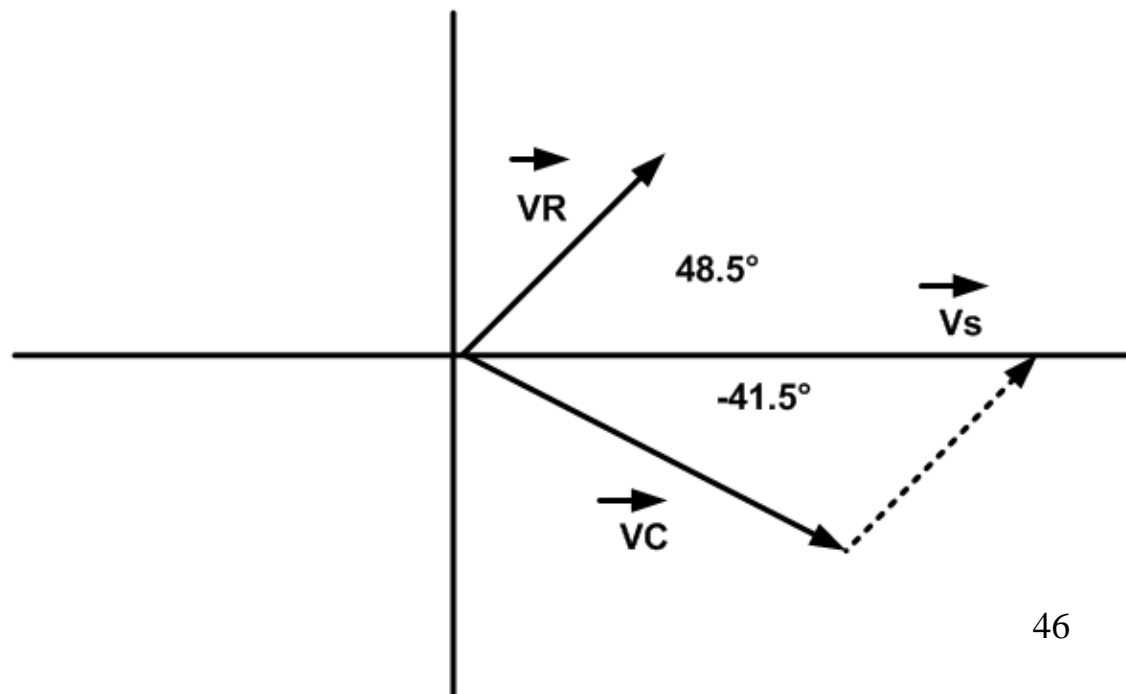
$$Z(j\omega) = 47 - j53.1 \Omega \quad \text{capacitive}$$

$$Z(j\omega) = 70.9 \angle -48.5^\circ \Omega \quad \text{capacitive}$$

$$\vec{V}_R = 47 \vec{I} = 66.3 \angle 48.5^\circ \text{ volt}$$

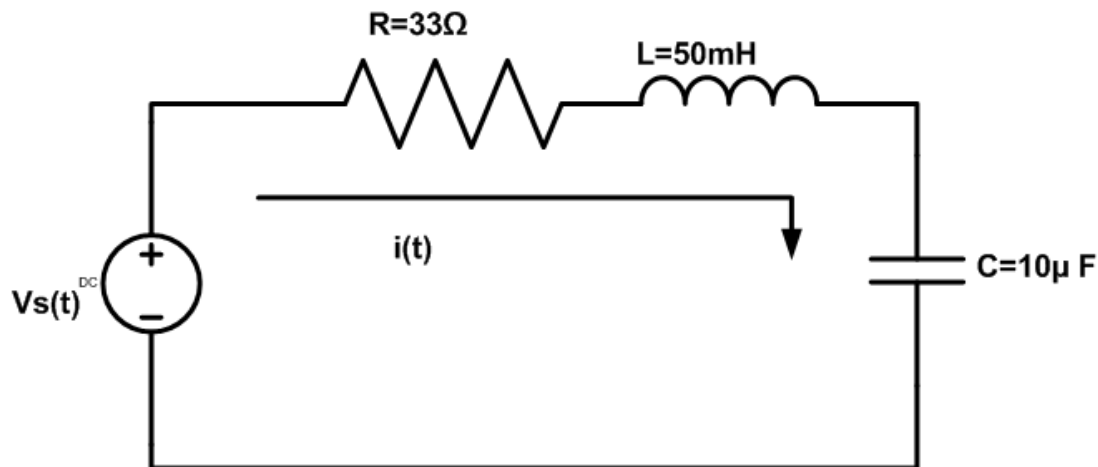
$$\vec{V}_C = -j53.1 \vec{I} = 74.9 \angle -41.5^\circ$$

\vec{V}_C lags \vec{I} by 90° .



Series RLC circuit

$$V_s(t) = 75 \cos 400\pi t \text{ volt}$$



$$KVL: \vec{V}_s = \vec{V}_R + \vec{V}_L + \vec{V}_C$$

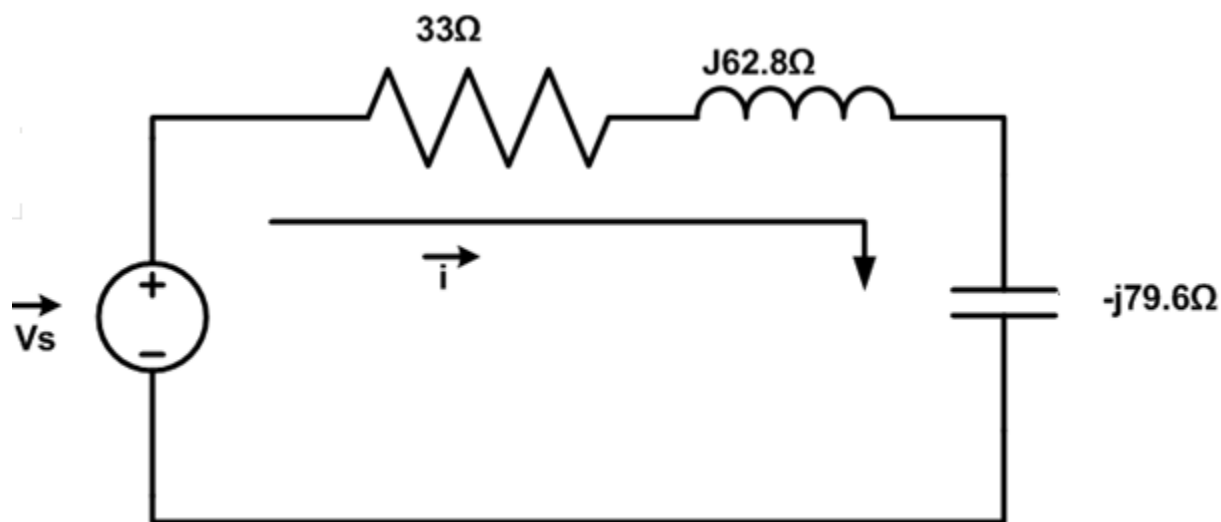
$$\vec{V}_s = 33\vec{I} + j62.8\vec{I} - j79.6\vec{I}$$

$$\vec{I} = \frac{\vec{V}_s}{33 - j16.8} = \frac{75\angle 0^\circ}{37\angle -27^\circ}$$

$$\vec{I} = 2.03 \angle 27^\circ \text{ A}$$

\vec{I} leads \vec{V}_s by 27°

\therefore capacitive circuit



ENEE2301 – Network Analysis 1

∴ *capacitive circuit*

$$Z_{eq} = R + j\omega L - j\frac{1}{\omega C}$$

$$Z_{eq} = 33 + j62.8 - j79.6$$

$$Z_{eq} = 33 - j16.8 \Omega \quad \text{capacitive}$$

$$Z_{eq} = 37 \angle -27 \Omega \quad \text{capacitive}$$

$$\vec{V}_R = R\vec{I} = 67 \angle 27^\circ \text{ volt}$$

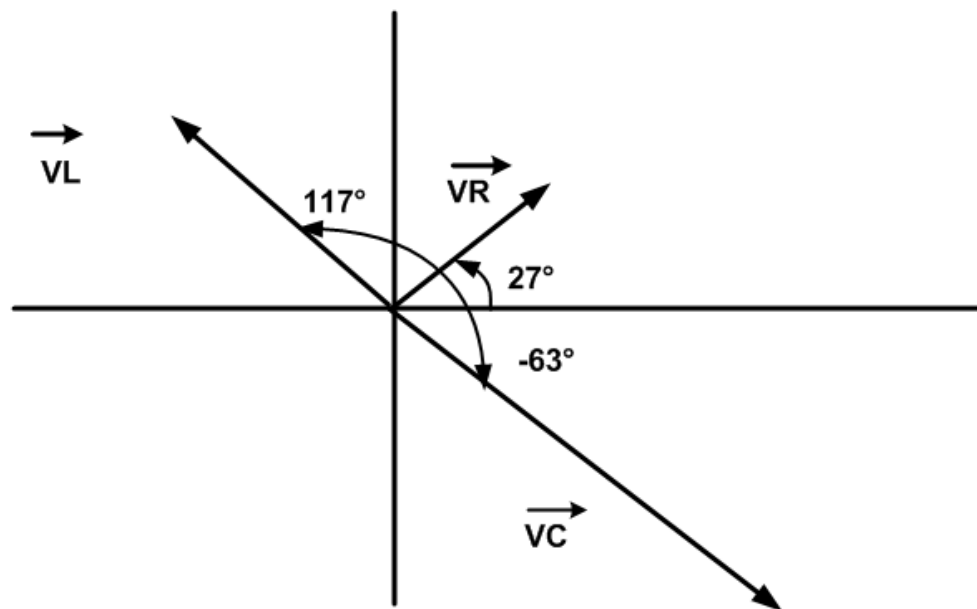
$$\vec{V}_L = j\omega L \vec{I} = 127 \angle 117^\circ \text{ volt}$$

$$\vec{V}_C = -j\frac{1}{\omega C} \vec{I} = 162 \angle -63^\circ \text{ volt}$$

$$\text{if } j\omega L - j\frac{1}{\omega C} = 0$$

$$\omega = \frac{1}{\sqrt{LC}} \quad \text{Resonant frequency}$$

$$Z_{eq} = R \quad \text{Resistive}$$

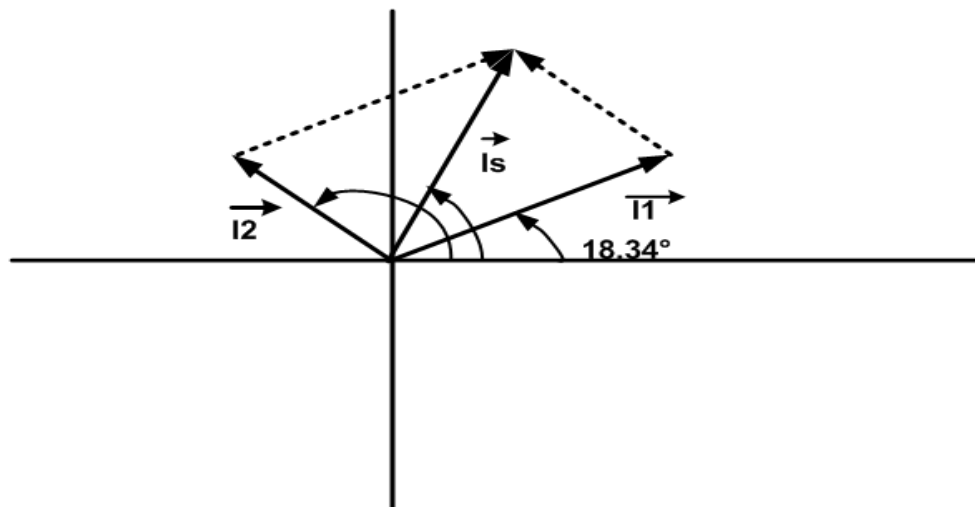
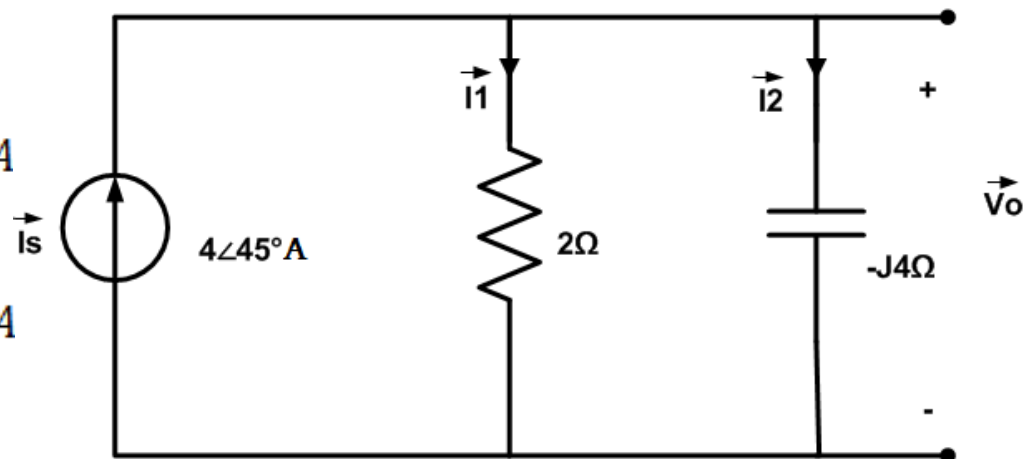


Find I_1 , I_2 , and V_o

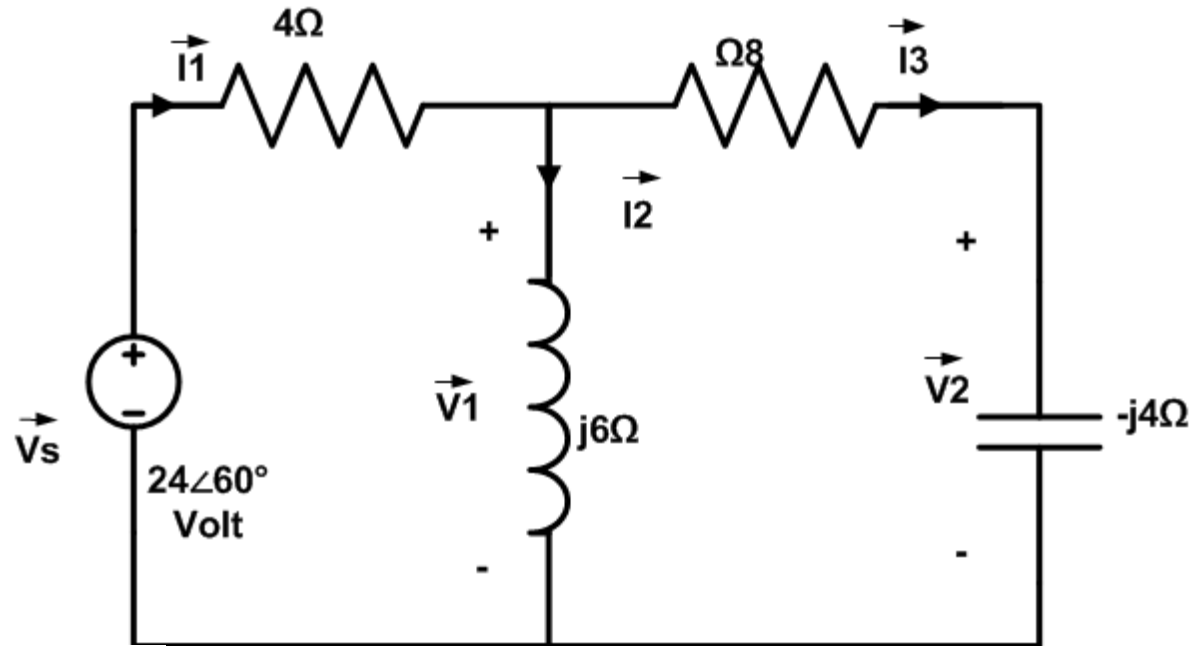
$$\vec{I}_1 = \frac{-j4}{-j4 + 2} \cdot \vec{I}_s = 3.578 \angle 18.435^\circ \text{ A}$$

$$\vec{I}_2 = \frac{2}{-j4 + 2} \cdot \vec{I}_s = 1.789 \angle 108.435^\circ \text{ A}$$

$$\vec{V}_o = 2 \vec{I}_1 = 7.156 \angle 18.435^\circ \text{ volt}$$



Calculate all voltages and currents



$$Z_{eq} = 4 + (j6 \parallel (8 - j4))$$

$$Z_{eq} = 9.604 \angle 30.964^\circ \Omega$$

$$\vec{I}_1 = \frac{\vec{V}_s}{Z_{eq}} = \frac{24\angle 60^\circ}{9.604\angle 30.964^\circ} = 2.498 \angle 29.036^\circ \text{ A}$$

$$\vec{I}_3 = \frac{j6}{j6 + 8 - j4} \cdot \vec{I}_1 = 1.82 \angle 105^\circ \text{ A}$$

$$\vec{I}_2 = \frac{8 - j4}{j6 + 8 - j4} \cdot \vec{I}_1 = 2.71 \angle -11.58^\circ \text{ A}$$

$$\vec{V}_1 = j6 \vec{I}_2 = 16.26 \angle 78.42^\circ \text{ volt}$$

$$\vec{V}_2 = -j4 \vec{I}_3 = 7.28 \angle 15^\circ \text{ volt}$$

ENEE2301 – Network Analysis 1

if $\vec{V}_o = 8\angle 45^\circ$ volt, find \vec{V}_s

$$\vec{I}_3 = \frac{\vec{V}_o}{2} = 4\angle 45^\circ \text{ A}$$

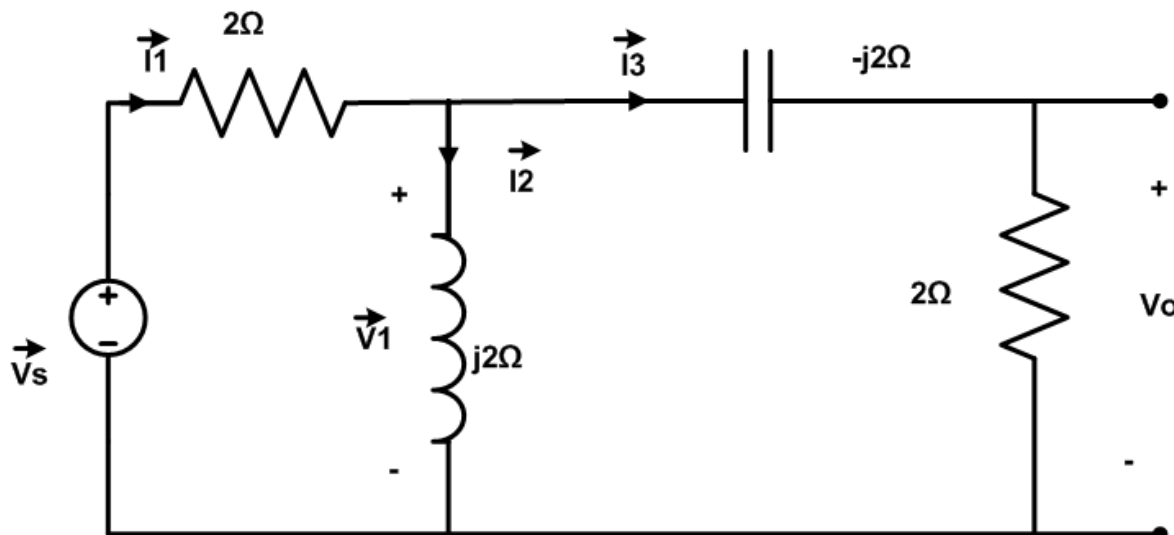
$$\vec{V}_1 = (2 - j2)\vec{I}_3 = 11.314 \angle 0^\circ$$

$$\vec{I}_2 = \frac{\vec{V}_1}{j2} = 5.657 \angle -90^\circ \text{ A}$$

$$\vec{I}_1 = \vec{I}_2 + \vec{I}_3 = (2.828 - j2.829)\text{A}$$

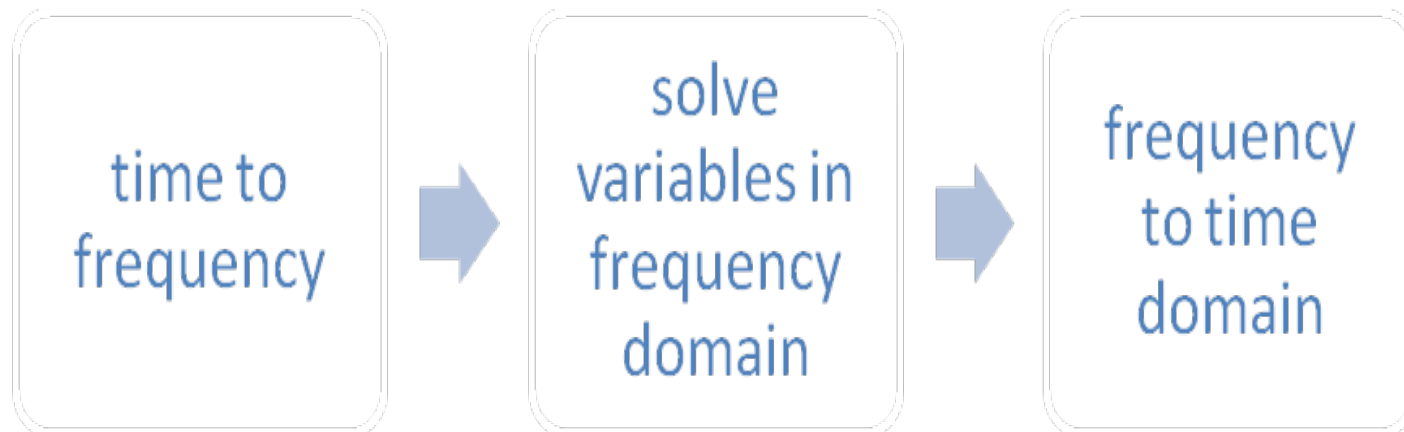
$$\vec{V}_s = 2\vec{I}_1 + \vec{V}_1$$

$$\vec{V}_s = 17.888 \angle -18.439^\circ \text{ volt}$$



Steps to analyze Ac circuits

- Transform the circuit to the phasor or frequency domain.
- Solve the problem using circuit techniques (Nodal analysis , Mesh analysis , Superposition , ... etc).
- Transform the resulting phasor to the time domain.



Nodal Analysis

find \vec{I}_o using Nodal analysis

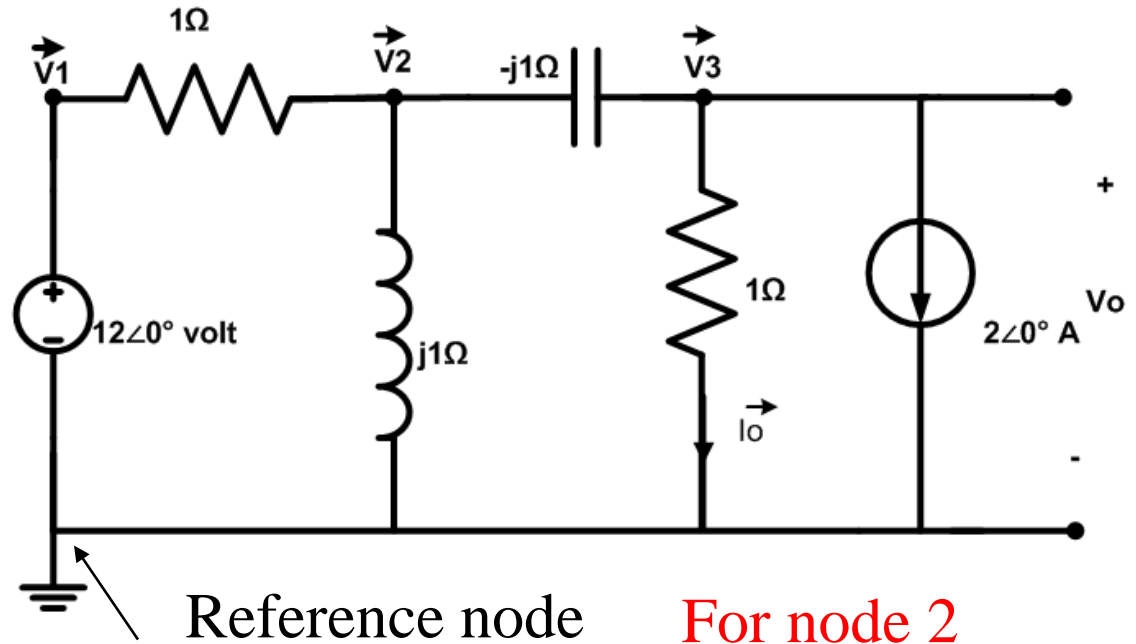
$$\vec{I}_o = \frac{\vec{V}_3}{1}$$

$$\vec{V}_1 = 12\angle 0^\circ \quad \text{constrain equation}$$

KCL at Node 2:

$$\frac{\vec{V}_2 - \vec{V}_1}{1} + \frac{\vec{V}_2}{j1} + \frac{\vec{V}_2 - \vec{V}_3}{-j1} = 0$$

$$-\vec{V}_1 + \vec{V}_2 - j\vec{V}_3 = 0$$



Reference node

For node 2

$$\text{Self admittance} = Y_{22} = \left(1 + \frac{1}{j1} + \frac{1}{-j1}\right) = 1$$

$$\text{Mutual admittance } Y_{23} = -\frac{1}{-j1} = -j$$

$$\text{Mutual admittance } Y_{21} = -1$$

KCL at node 3:

$$-2\angle 0^\circ = -\frac{1}{-j1}\vec{V}_2 + \left(\frac{1}{-j1} + 1\right)\vec{V}_3 \quad \longrightarrow \quad -2\angle 0^\circ = -\frac{1}{-j1}\vec{V}_2 + (j1 + 1)\vec{V}_3$$

solving for \vec{V}_3 ;

$$\vec{V}_3 = \left(\frac{8}{5} + j \frac{26}{5} \right) V$$

$$\therefore \vec{I}_o = \frac{\vec{V}_3}{1} = \left(\frac{8}{5} + j \frac{26}{5} \right) A$$

Mesh analysis :

find \vec{I}_o using Mesh analysis

$$\vec{I}_o = \vec{I}_2 - \vec{I}_3$$

$$\vec{I}_3 = 2\angle 0^\circ \text{ A} \quad \text{Constrain equation}$$

KVL for mesh 1:

$$12\angle 0^\circ = (1 + j1)\vec{I}_1 - j1\vec{I}_2$$

KVL for mesh 2 :

$$0 = -j1\vec{I}_1 + (1 + j1 - j1)\vec{I}_2 - \vec{I}_3$$

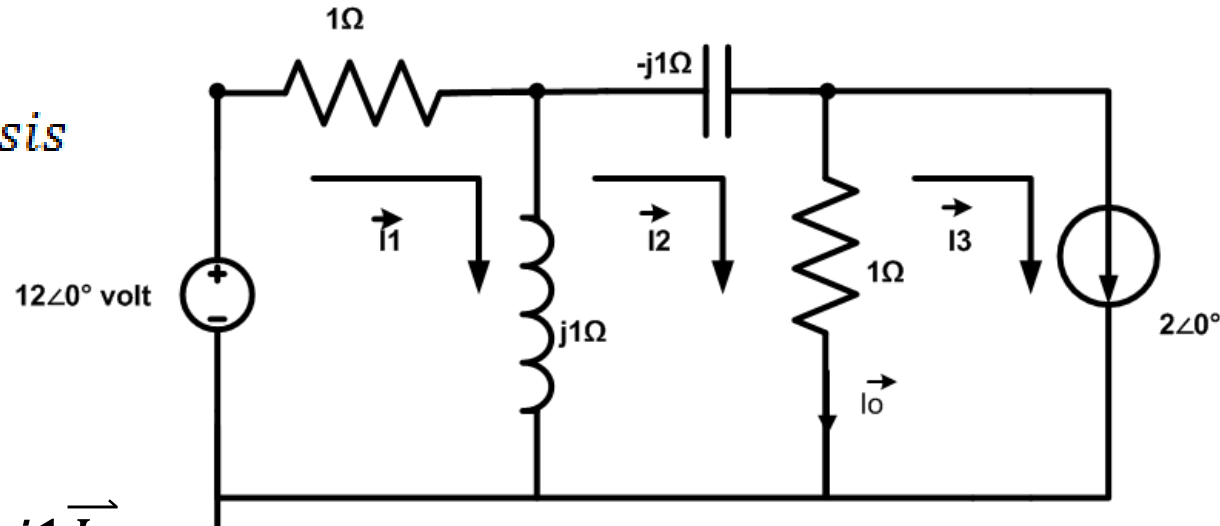
$$0 = -j1\vec{I}_1 + \vec{I}_2 - \vec{I}_3$$

solving for \vec{I}_2 and \vec{I}_3

$$\vec{I}_2 = \left(\frac{18}{5} + j\frac{26}{5}\right) \text{ A}$$

$$\vec{I}_3 = 2\angle 0^\circ \text{ A}$$

$$\therefore \vec{I}_o = \left(\frac{8}{5} + j\frac{26}{5}\right) \text{ A}$$



For mesh 1

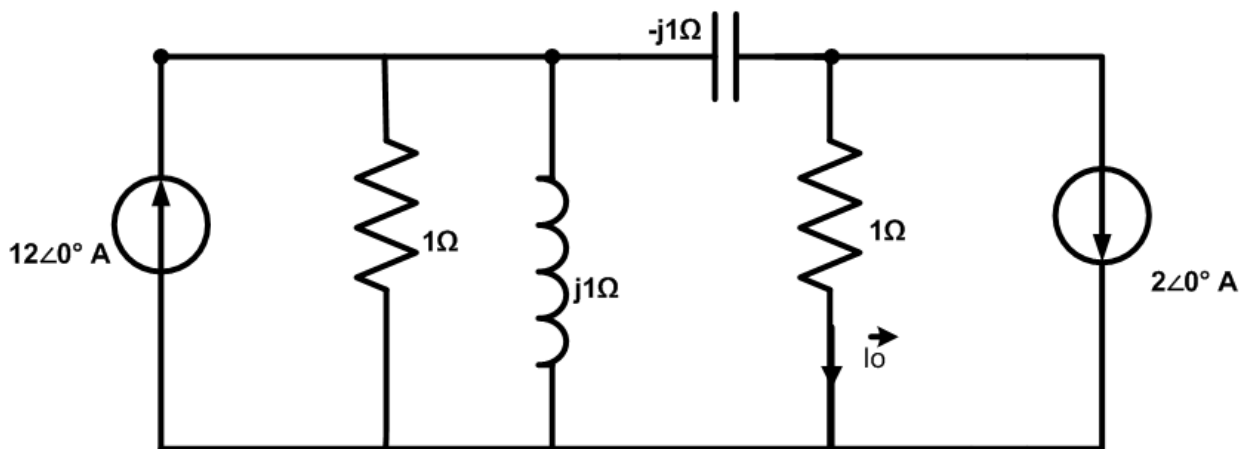
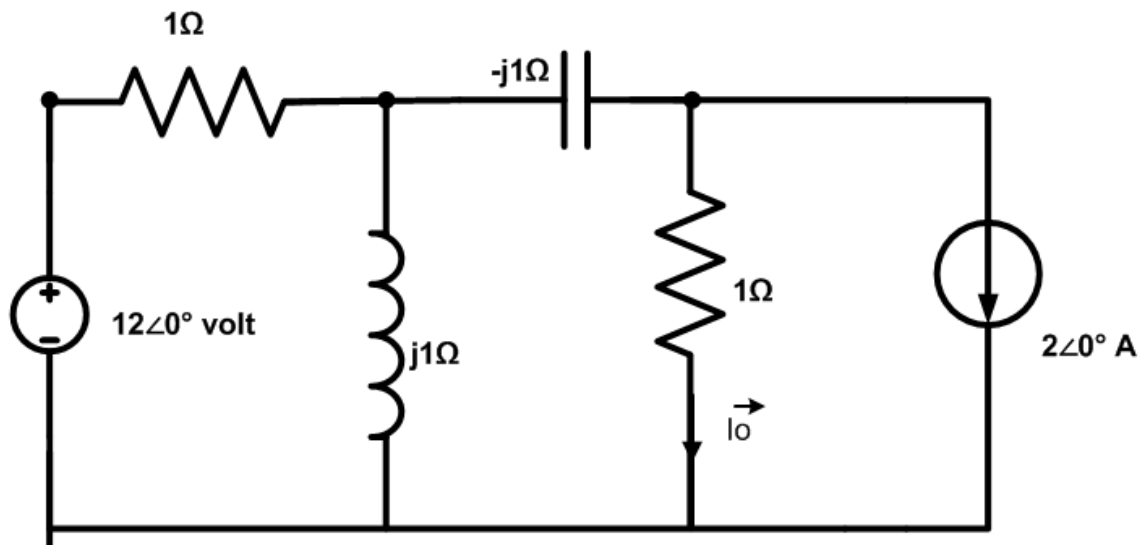
Self impedance $Z_{11} = + (1+j1)$

Mutual impedance $Z_{12} = - j1$

Mutual impedance $Z_{13} = - 0$

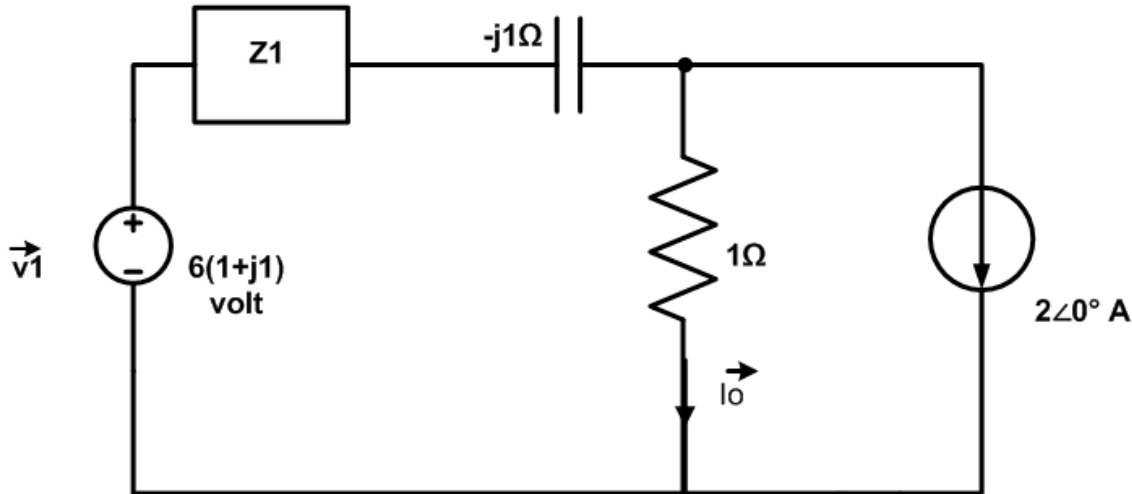
Source Transformation

find \vec{I}_o using source transformation



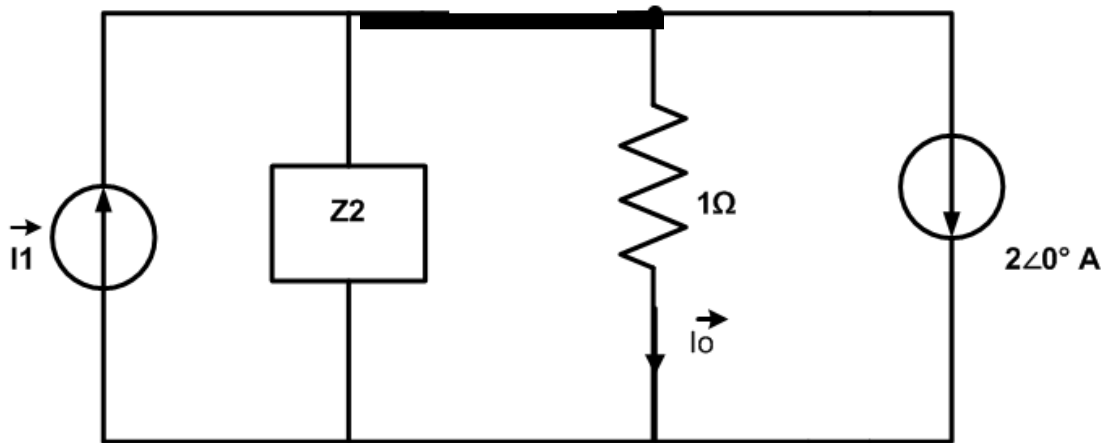
$$Z_1 = 1 \parallel (j1) = \left(\frac{1}{2} + j\frac{1}{2}\right) \Omega$$

ENEE2301 – Network Analysis 1



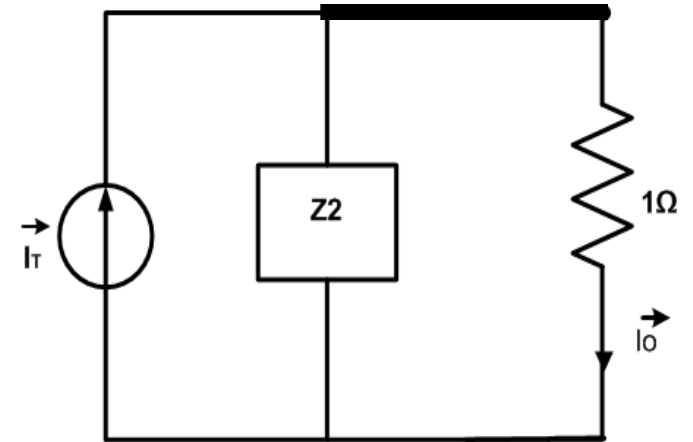
$$Z1 = 1 \parallel (j1) = \left(\frac{1}{2} + j\frac{1}{2}\right) \Omega$$

$$V1 = 12\angle 0^\circ. Z1 = 6(1+j1) \text{ volt}$$



$$\vec{I1} = \frac{\vec{V1}}{Z2} = \frac{12(1+j1)}{1-j1}$$

$$Z2 = -j1 + Z1 = \left(\frac{1}{2} - j\frac{1}{2}\right) \Omega$$



$$\vec{I}_T = \vec{I1} - 2\angle 0^\circ$$

$$\vec{I}_T = \left(\frac{10+j4}{1-j1}\right) A$$

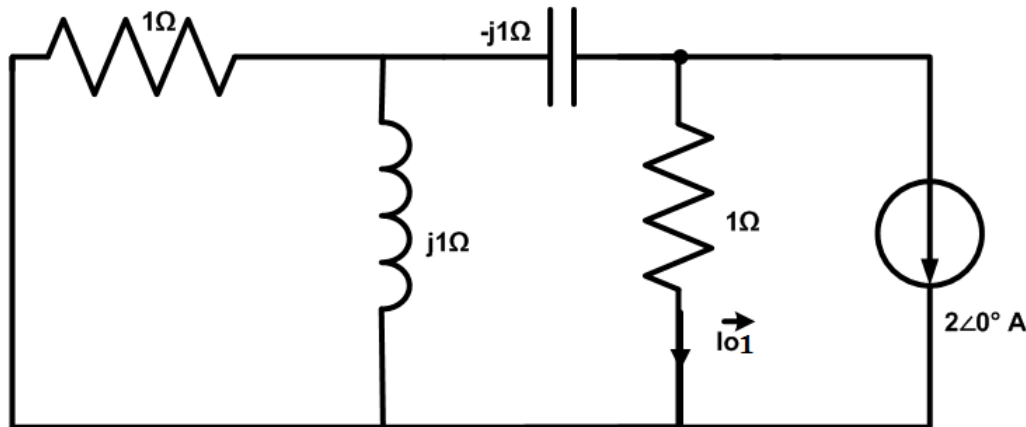
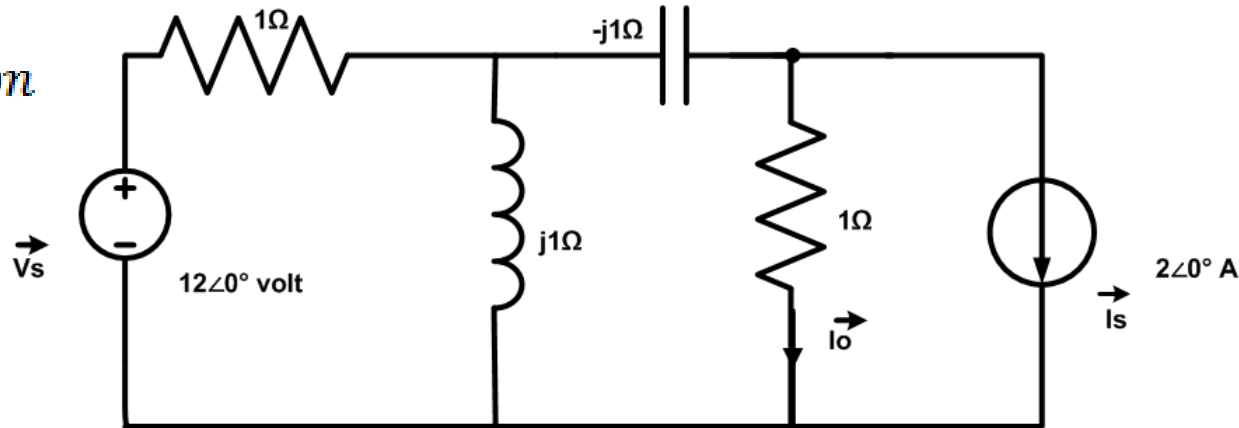
$$\vec{I}_o = \frac{Z2}{Z2+1} \cdot \vec{I}_T = \left(\frac{8}{5} + j\frac{26}{5}\right) A^{57}$$

Superposition

find \vec{I}_o using super position

$$\vec{I}_o = \vec{I}_{o1} + \vec{I}_{o2}$$

1) let \vec{V}_s off, and \vec{I}_s on.



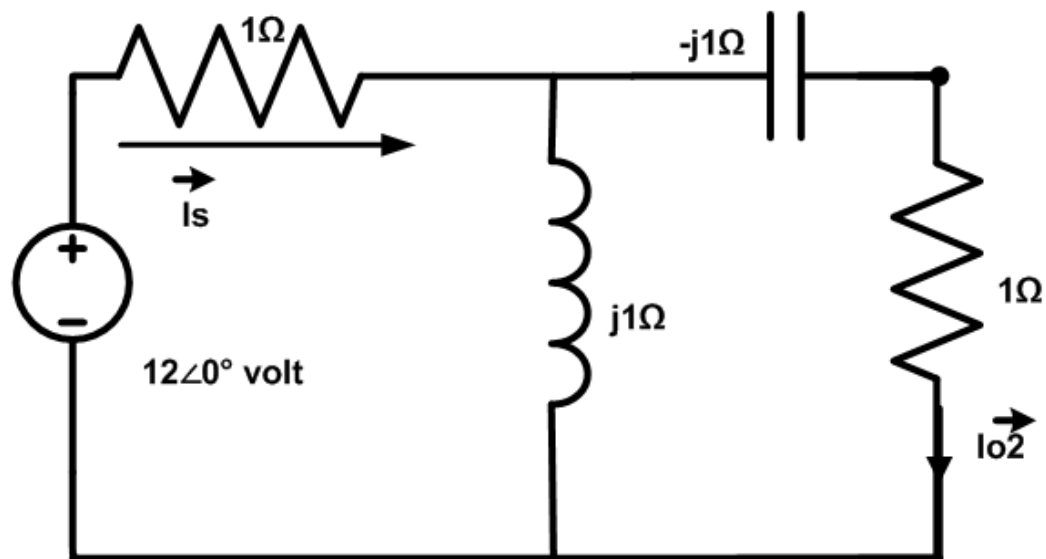
$$\vec{I}_{o1} = -2\angle 0^\circ \cdot \frac{Z_1}{Z_1 + 1}$$

$$Z_1 = -j1 + (1 \parallel j1) = -j1 + \frac{j1}{1 + j1}$$

$$\vec{I}_{o1} = \frac{-2}{2 + j1} \text{ A}$$

2) let \vec{I}_s off, and \vec{V}_s on.

$$\vec{I}_s = \frac{12\angle 0^\circ}{Z_{eq}}$$



$$Z_{eq} = 1 + (j1 \parallel (1 - j1)) = 2 + j1 \Omega$$

$$\therefore \vec{I}_s = \frac{12\angle 0^\circ}{2 + j1} A$$

$$\vec{I}_{o2} = \vec{I}_s \cdot \frac{j1}{j1 + 1 - j1}$$

$$\vec{I}_{o2} = \vec{I}_s \cdot j1 = \frac{12}{1 - j2} A$$

$$\therefore \vec{I}_o = \vec{I}_{o1} + \vec{I}_{o2}$$



$$\vec{I}_o = \left(\frac{8}{5} + j \frac{26}{5} \right) A$$

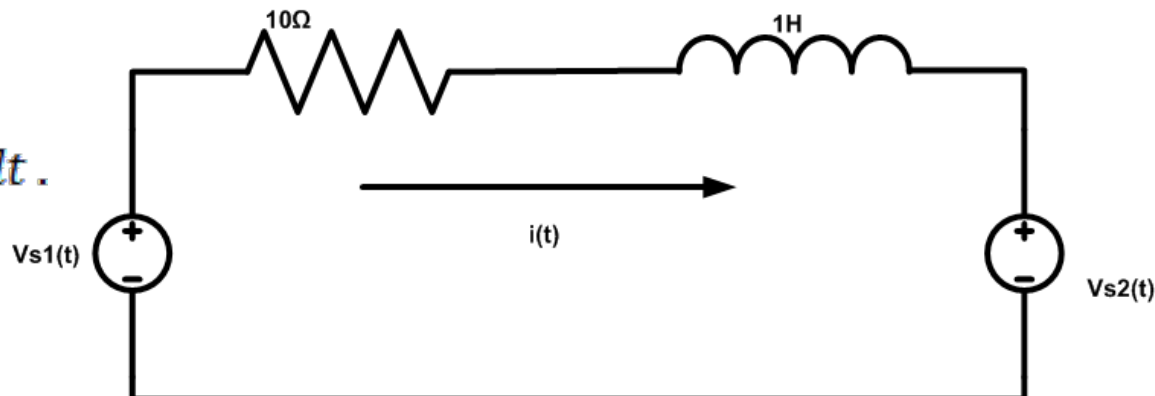
Power of super position :

$$V_{s1}(t) = 100 \cos 10t \text{ volt}$$

$$V_{s2}(t) = 50 \cos(20t - 10^\circ) \text{ volt.}$$

$$\text{note that } \omega_1 = 10 \text{ rad/sec}$$

$$\text{and } \omega_2 = 20 \text{ rad/sec}$$



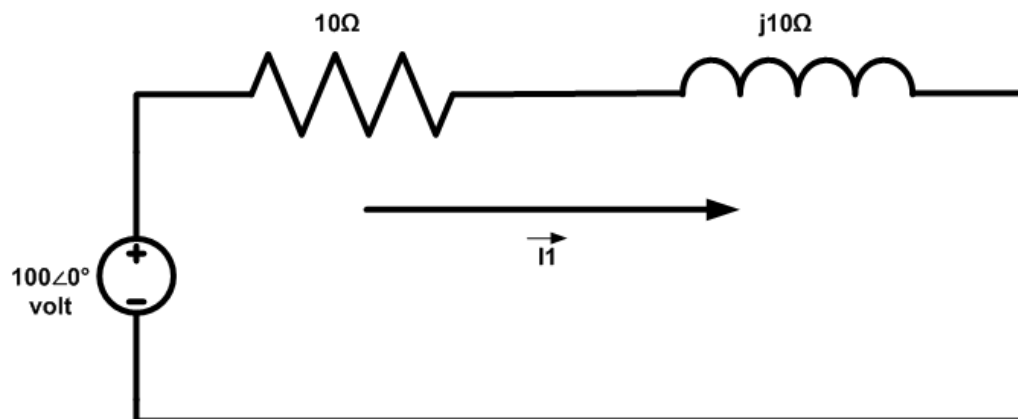
\therefore super position is the only method of analysis .

$$i(t) = i_1(t) + i_2(t).$$

1) let $V_{s2}(t)$ off, and $V_{s1}(t)$ on.

$$\vec{I}_1 = \frac{100\angle 0^\circ}{10 + j10} = 7.07\angle -45^\circ \text{ A}$$

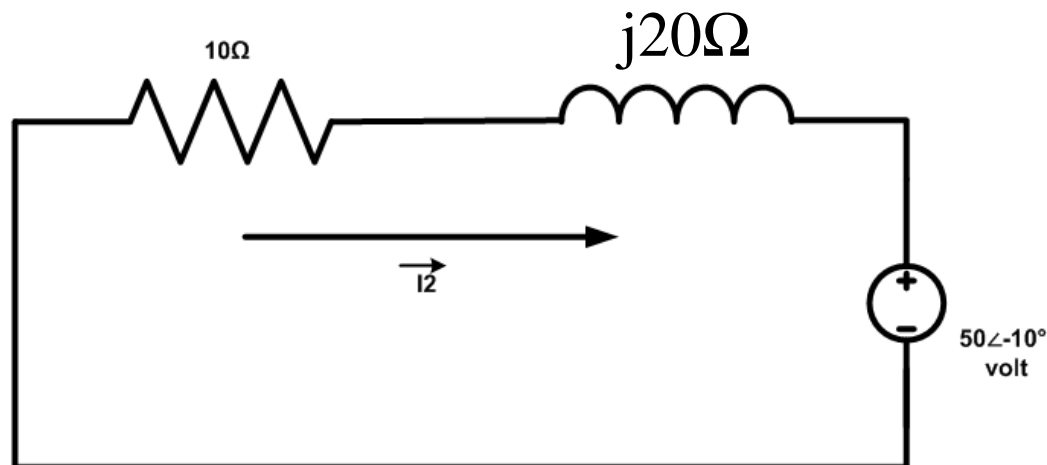
$$\therefore i_1(t) = 7.07 \cos(10t - 45^\circ) \text{ A.}$$



2) let $V_{s1}(t)$ off, and $V_{s2}(t)$ on.

$$\vec{I}_2 = \frac{-50\angle -10^\circ}{10 + j20} = \frac{50\angle 170^\circ}{10 + j20}$$

$$\vec{I}_2 = 2.24\angle 106.57^\circ \text{ A}$$

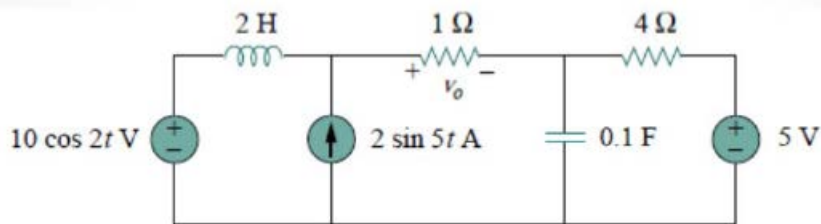


$$\therefore i_2(t) = 2.24 \cos(20t + 106.57^\circ) \text{ A.}$$

$$\therefore i(t) = i_1(t) + i_2(t)$$

$$i(t) = 7.07 \cos(10t - 45^\circ) + 2.24 \cos(20t + 106.57^\circ) \text{ A}$$

Superposition (dc+ac) sources



Find $V_o(t)$ using the superposition theorem

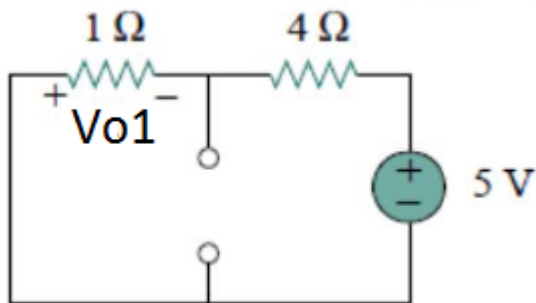
The steady state $V_o(t)$

Solution:

❖ The circuit operates at three different frequencies

$$V_o(t) = V_{o1}(t) + V_{o2}(t) + V_{o3}(t)$$

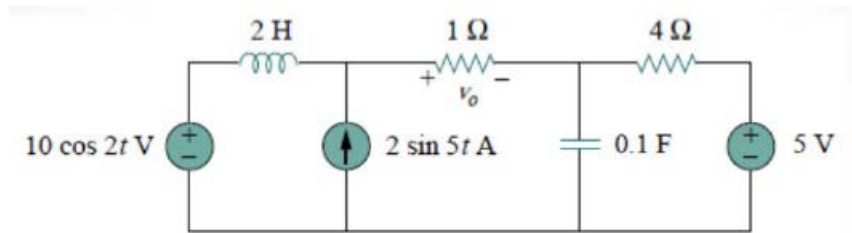
1. To find $V_{o1}(t)$ (due to dc source)



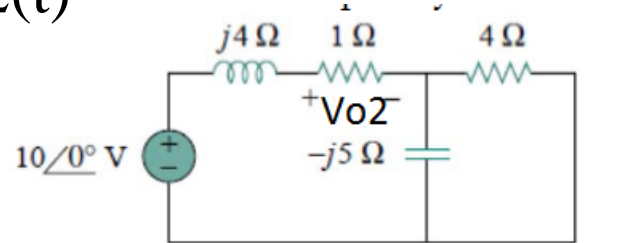
$$V_{o1}(t) = -1 \text{ V}$$

Inductor becomes short
Capacitor becomes open
The sinusoidal sources are off

Superposition (dc+ac) sources



2. To find $V_{o2}(t)$



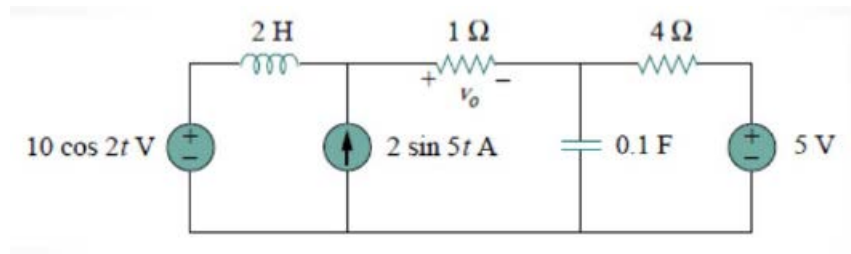
$10 \cos 2t \rightarrow 10 \angle 0^\circ, \quad \omega = 2 \text{ rad/s}$

$2 \text{ H} \rightarrow j\omega L = j4 \Omega$

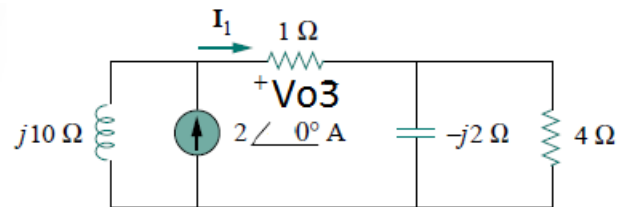
$0.1 \text{ F} \rightarrow \frac{1}{j\omega C} = -j5 \Omega$

$V_{o2}(t) = 2.498 \cos (2t - 30.79) \text{ V}$

Superposition (dc+ac) sources



3 . To find $V_{o3}(t)$



$$2 \sin 5t \quad \rightarrow \quad 2 \angle 0^\circ, \quad \omega = 5 \text{ rad/s}$$

$$2 \text{ H} \quad \rightarrow \quad j\omega L = j10 \Omega$$

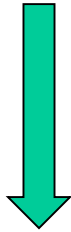
$$0.1 \text{ F} \quad \rightarrow \quad \frac{1}{j\omega C} = -j2 \Omega$$

$$V_{o3}(t) = 2.33 \sin(5t+10) \text{ V}$$

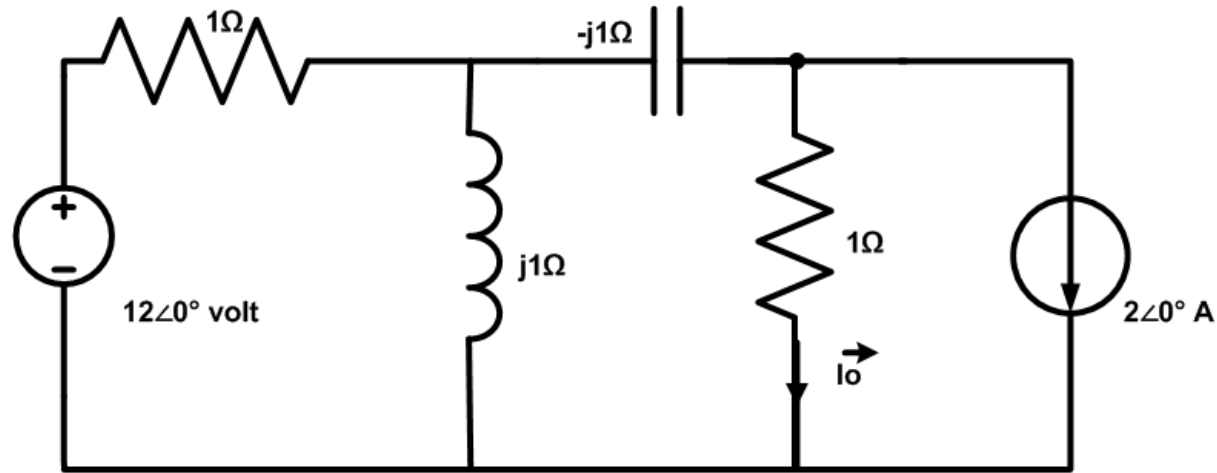
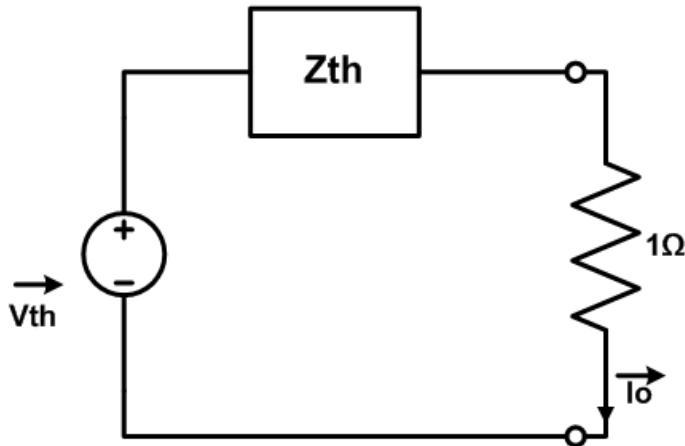
$$V_o(t) = -1 + 2.498 \cos(2t-30.79) + 2.33 \sin(5t+10)$$

Thevenin's and Norton's theorems

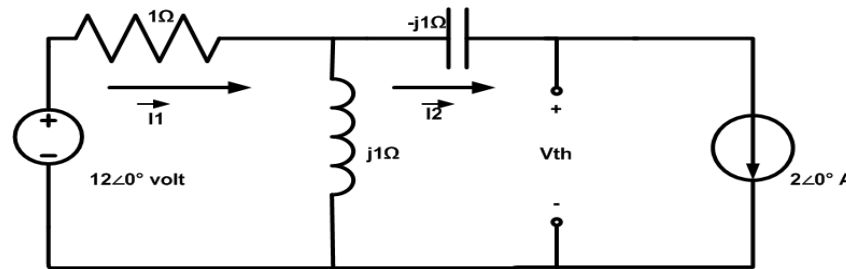
find \vec{I}_o using thevenin's theorem



$$\vec{I}_o = \frac{V_{TH}}{Z_{TH} + 1 \Omega}$$



to find \vec{V}_{TH}



$$\vec{V}_{TH} = -(-j1)\vec{I}_2 + j1(\vec{I}_1 - \vec{I}_2)$$

$$\vec{I}_2 = 2\angle 0^\circ \quad \text{Constraint equation}$$

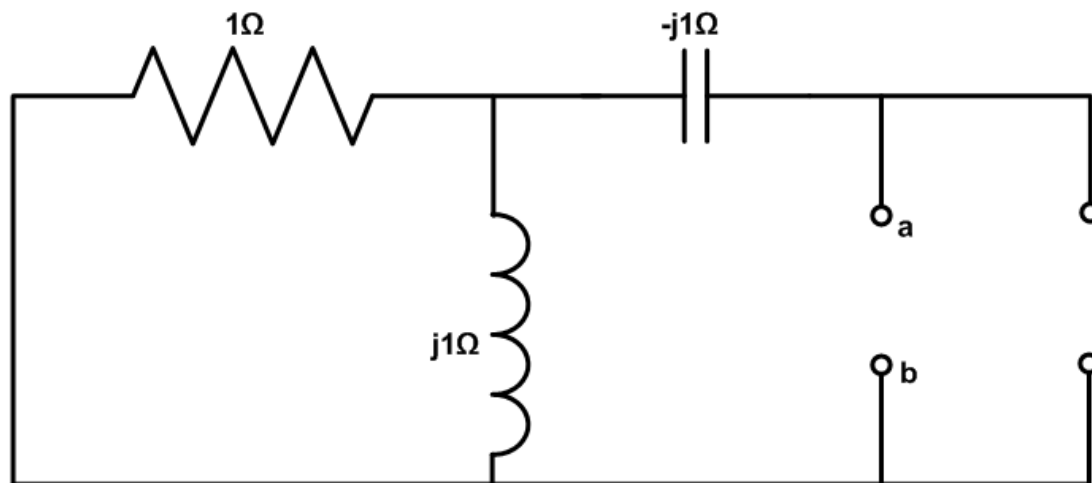
KVL for mesh 1:

$$12\angle 0^\circ = (1 + j1)\vec{I}_1 - j1\vec{I}_2$$

$$\therefore \vec{I}_1 = \left(\frac{12 + j2}{1 + j1}\right)A$$

$$\therefore \vec{V}_{TH} = \left(\frac{-2 + j12}{1 + j1}\right) \text{ volt}$$

to find Z_{TH} , set all the independent source to zero.



$$Z_{TH} = -j1 + (1 || j1)$$

$$Z_{TH} = \left(\frac{1}{2} - j\frac{1}{2}\right) \Omega$$

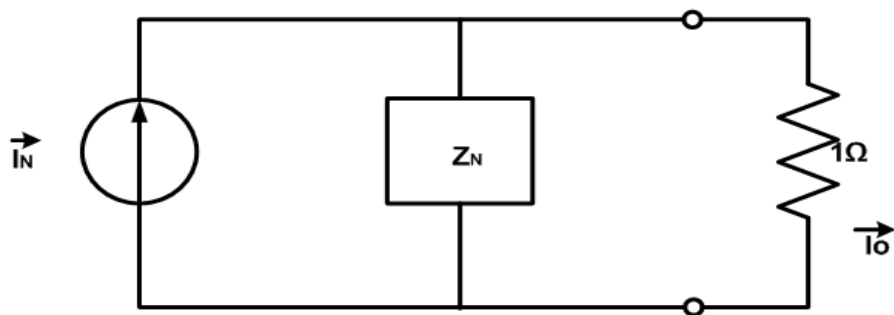
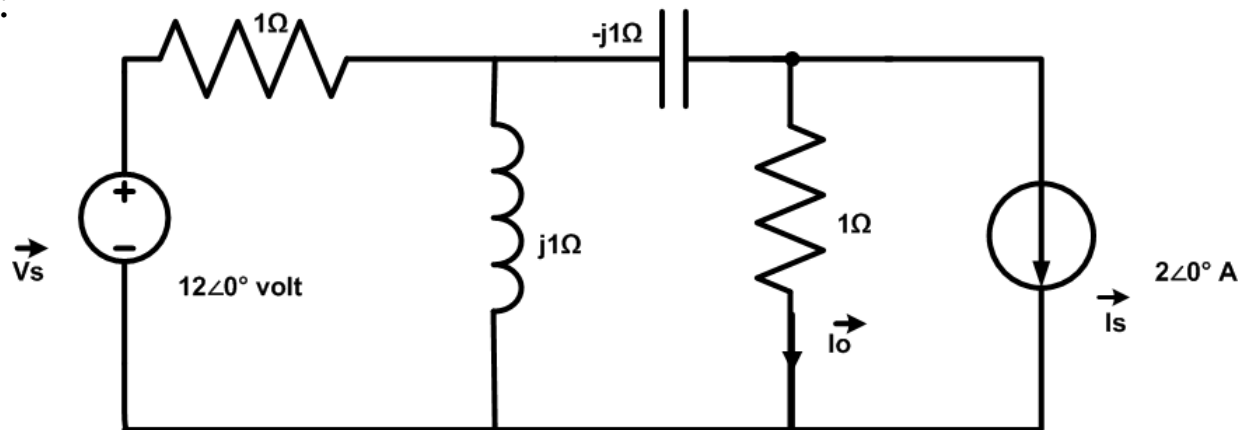
$$\vec{I}_O = \frac{\vec{V}_{TH}}{Z_{TH} + 1 \Omega}$$



$$I_o = \left(\frac{8}{5} + j\frac{26}{5}\right) A$$

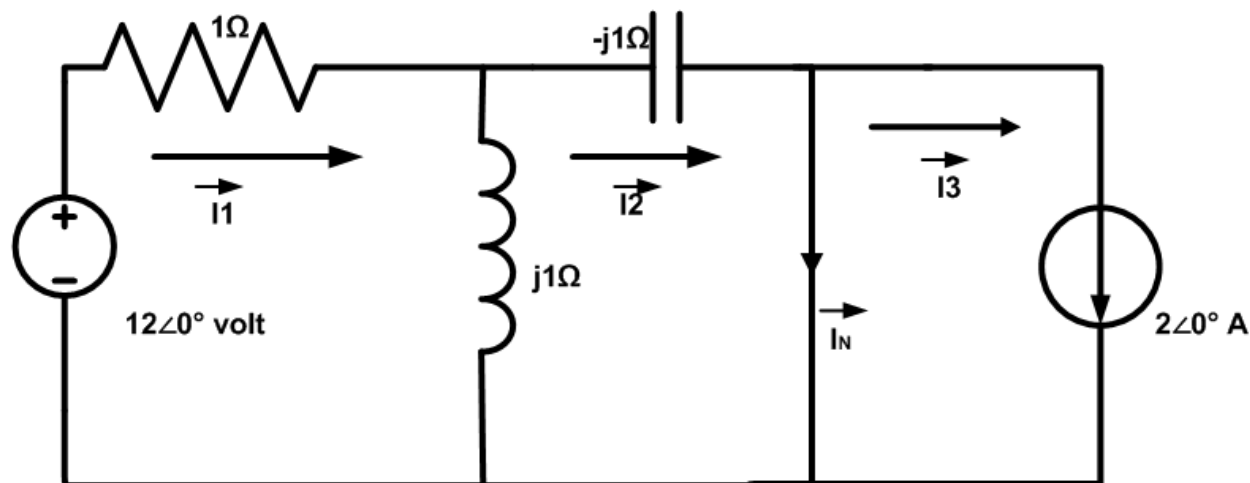
Norton's Theorem :

find \vec{I}_o using Norton's theorem



$$\vec{I}_o = \vec{I}_N \cdot \frac{Z_N}{Z_N + 1\Omega}$$

1) to find I_N



$$\vec{I}_N = \vec{I}_2 - \vec{I}_3$$

$$\vec{I}_3 = 2\angle 0^\circ \text{ A constraint equation}$$

KVL for mesh 1:

$$12\angle 0^\circ = (1 + j1)\vec{I}_1 - j1 \vec{I}_2$$

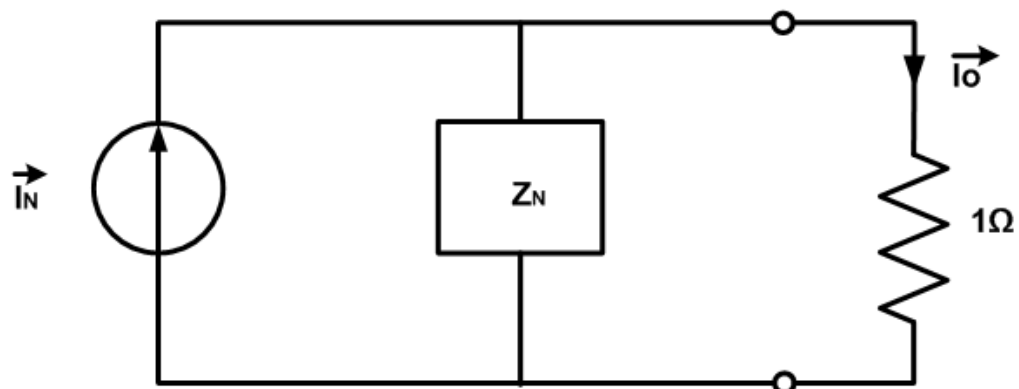
KVL for mesh 2:

$$0 = -j1 \vec{I}_1 + (j1 - j1)\vec{I}_2 \quad \longrightarrow \quad 0 = -j1 \vec{I}_1 \quad \longrightarrow \quad \therefore \vec{I}_1 = 0$$

$$\therefore \vec{I}_2 = 12\angle 90^\circ \text{ A}$$

$$\vec{I}_N = \vec{I}_2 - \vec{I}_3 = -2 + j12 \text{ A}$$

2) $Z_N = Z_{TH} = \left(\frac{1}{2} - j\frac{1}{2}\right) \Omega$

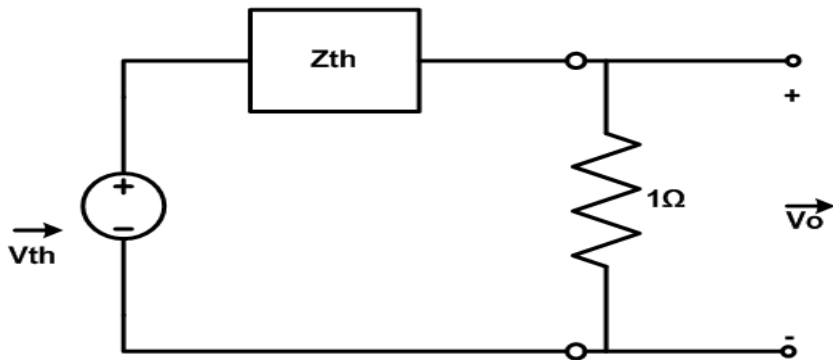
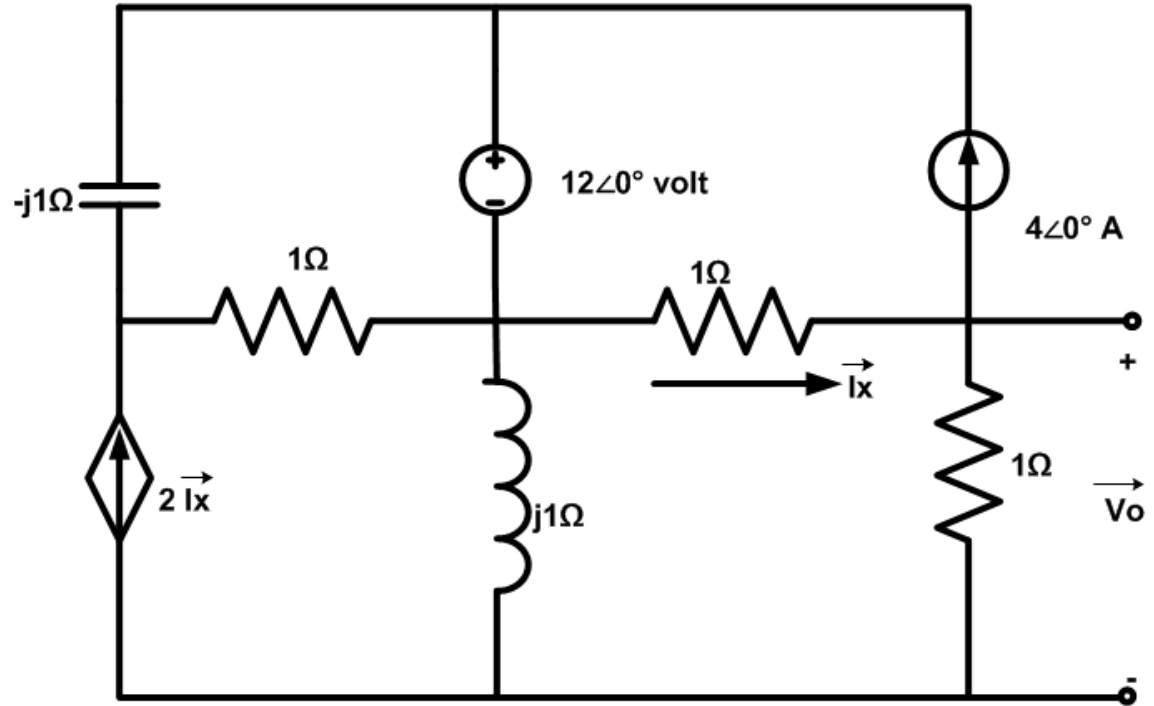
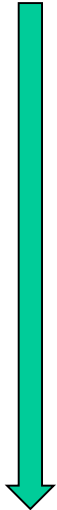


$$\vec{I}_o = \vec{I}_N \cdot \frac{Z_N}{Z_N + 1\Omega}$$

$$\vec{I}_o = \left(\frac{8}{5} + j\frac{26}{5} \right) A$$

ENEE2301 – Network Analysis 1

find \vec{V}_o using Thevenin's theorem



$$\vec{V}_o = \frac{1\Omega}{1\Omega + Z_{TH}} \cdot \vec{V}_{TH}$$

1) to find $\overline{V_{TH}}$

$$V_{TH} = -1\Omega \overline{I_x} + j1\Omega (2\overline{I_x})$$

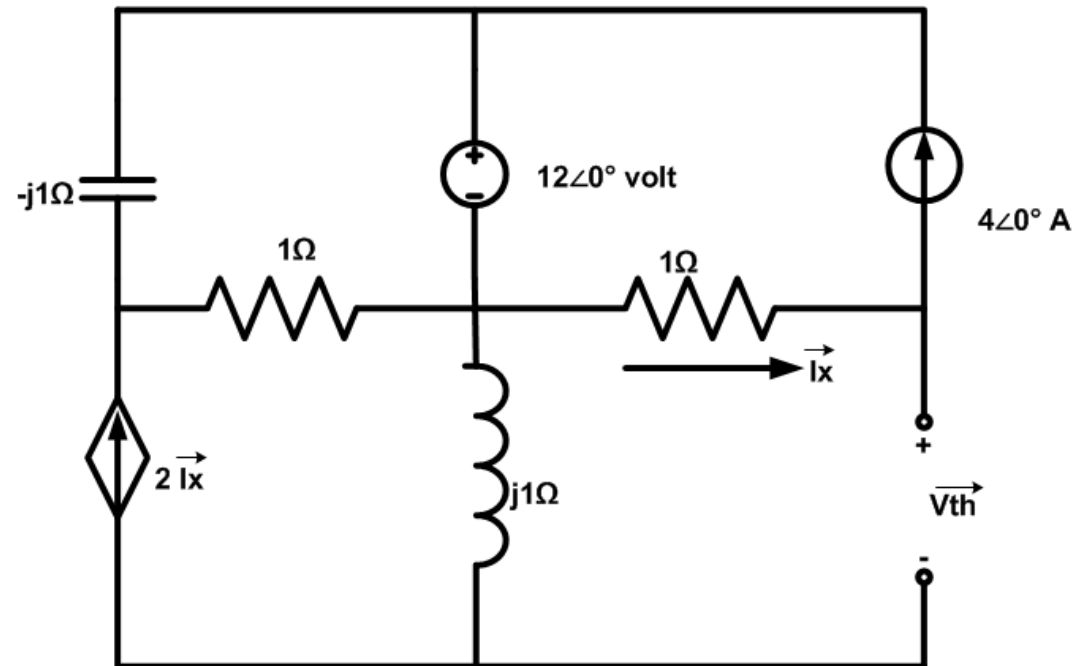
$$\overline{I_x} = 4\angle 0^\circ A$$

$$\therefore \overline{V_{TH}} = (-4 + j8) \text{ volt.}$$

2) to find Z_{TH}

$$Z_{TH} = \frac{\overline{V_{TH}}}{\overline{I_N}}$$

$$Z_{TH} = \left. \frac{\overline{V_T}}{\overline{I_T}} \right| \text{ all independent sources are set to zero.}$$



to find \vec{I}_N

$$\vec{I}_N = \vec{I}_x - 4\angle 0^\circ$$

$$\vec{I}_x = \frac{\vec{V}_3}{1\Omega} = \vec{V}_3$$

Nodal analysis

$$\vec{V}_1 - \vec{V}_3 = 12\angle 0^\circ \quad \text{constrain equation}$$

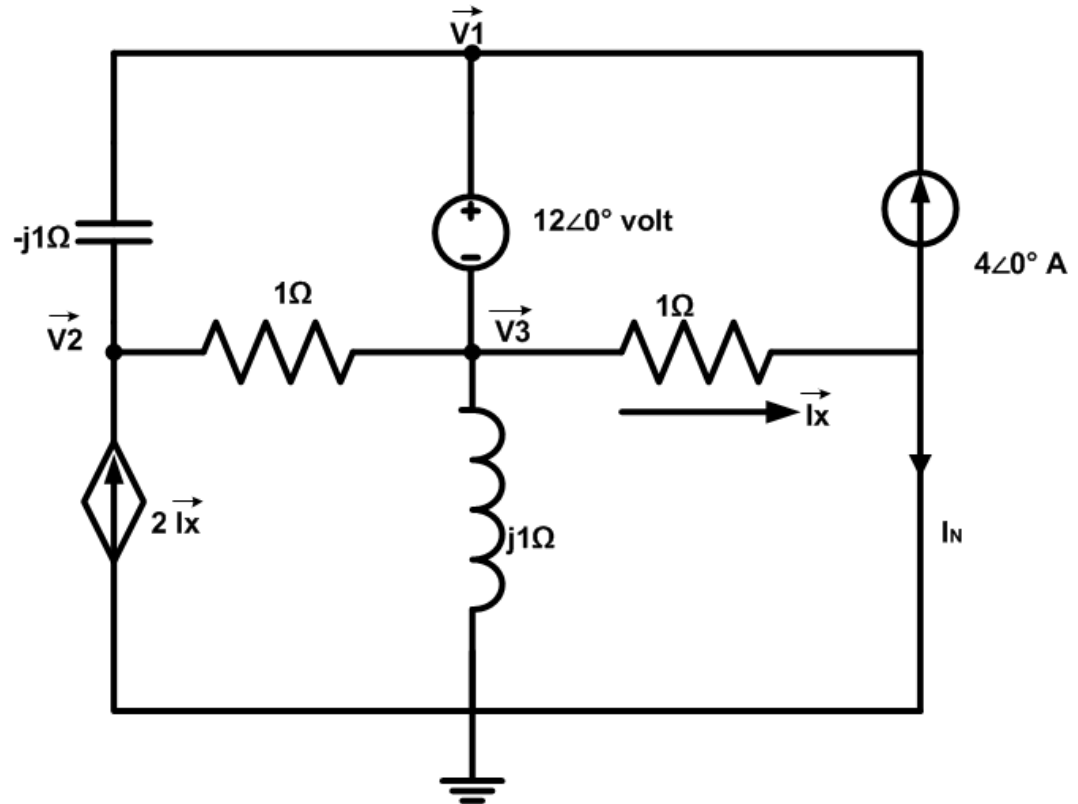
KCL at node 2:

$$2\vec{I}_x = \left(1 + \frac{1}{-j1}\right)\vec{V}_2 + j1\vec{V}_1 - 1\vec{V}_3$$

KCL at super node (1,3)

$$4\angle 0^\circ = \left(\frac{1}{-j1}\right)\vec{V}_1 + \left(1 + 1 + \frac{1}{j1}\right)\vec{V}_3 - \left(1 + \frac{1}{-j1}\right)\vec{V}_2$$

Solving for $\vec{V}_3 \longrightarrow \vec{V}_3 = \left(\frac{j4}{1-j1}\right)$



$$\therefore I_N = -\left(\frac{8+j4}{1+j1}\right) A$$

$$\therefore Z_{TH} = \frac{\vec{V}_{TH}}{\vec{I}_N}$$

$$Z_{TH} = (1-j1)\Omega$$

$$\vec{V}_O = \frac{-4+j8}{1+1-j1} = 4\angle 143.13^\circ \text{ volt} \quad 72$$

$$Z_{TH} = \frac{\vec{V}_T}{\vec{I}_T} \Big|_{\text{all independent sources are set to zero.}}$$

$$\vec{V}_T = -1 \vec{I}_x + j1 \vec{I}_x$$

$$\vec{V}_T = (-1 + j1) \vec{I}_x$$

$$\vec{I}_x = -\vec{I}_T$$

$$\vec{V}_T = -(-1 + j1) \vec{I}_T$$

$$Z_{TH} = \frac{\vec{V}_T}{\vec{I}_T} = (1 - j1) \Omega$$

