

**Question 1. [25 MARKS]**

All parts of this question consider the discrete-time linear time-invariant system with impulse response:

$$h[n] = 2^{-n}u[n]$$

**Part (a) [4 MARKS]**

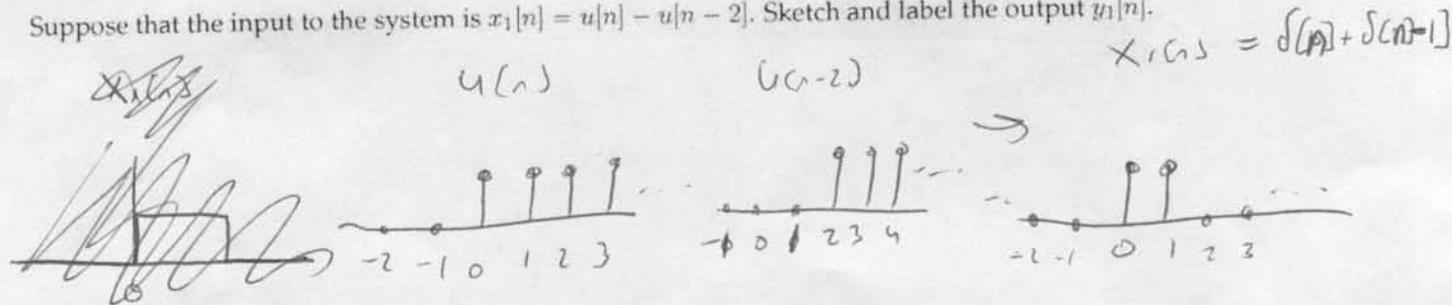
Is the LTI system stable? Causal? Give brief explanations.

Stability  $\sum_{n=-\infty}^{\infty} |h[n]| < \infty \rightarrow \sum_{n=0}^{\infty} 2^{-n} = \sum_{n=0}^{\infty} \left(\frac{1}{2}\right)^n = \frac{1}{1-\frac{1}{2}} = \frac{1}{\frac{1}{2}} = 2$  Yes Stable ✓

Causal:  $h[n] = 0 \quad n < 0$  Here  $h[n] = \begin{cases} 2^{-n} & n \geq 0 \\ 0 & n < 0 \end{cases}$  Yes, Causal ✓

**Part (b) [6 MARKS]**

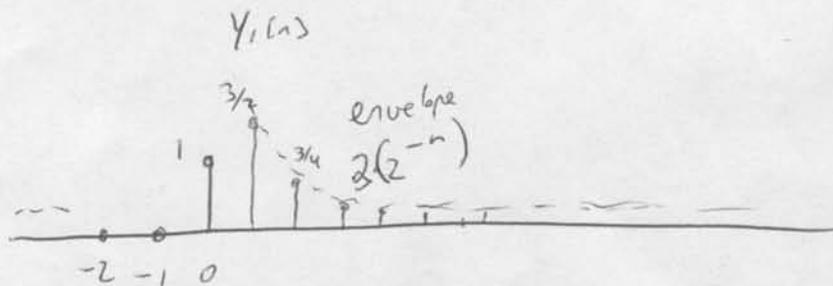
Suppose that the input to the system is  $x_1[n] = u[n] - u[n-2]$ . Sketch and label the output  $y_1[n]$ .



$$y_1[n] = x_1[n] * h_1[n] = \sum_{k=-\infty}^{\infty} x_1[k] h_1[n-k]$$

$$2^{-n} + 2^{-(n-1)} = 2^{-n} + 2 \cdot 2^{-n} = 3 \cdot 2^{-n}$$

$$= \sum_{k=-\infty}^{\infty} (\delta[k] + \delta[k-1]) h_1[n-k] = h_1[n] + h_1[n-1] = 2^{-n} u[n] + 2^{-(n-1)} u[n-1]$$



## Part (c) [10 MARKS]

Construct an input signal  $x_2[n]$  such that the output  $y_2[n] = \delta[n]$ .

Time domain

To get  $\delta[n]$ , put in  $\delta[n] \rightarrow z^{-n} u[n]$   
at  $n=0$ Need to cancel  $z^{-n-1} u[n-1] \rightarrow$  use  $-\frac{1}{2} \delta[n-1]$ 

$$x_2[n] = \delta[n] - \frac{1}{2} \delta[n-1]$$

$$y_2[n] = \sum_{k=0}^{\infty} (\delta[k] - \frac{1}{2} \delta[k-1]) z^{-(n-k)} u[n-k]$$

$$= z^{-n} u[n] - \frac{1}{2} z^{-(n-1)} u[n-1]$$

$$= \delta[n] + z^{-n} u[n-1] - z^{-n} u[n-1] =$$

## Part (d) [5 MARKS]

Construct an input signal  $x_3[n]$  such that the output  $y_3[n] = u[n]$ .From part c, we know that  $\delta[n] - \frac{1}{2} \delta[n-1]$  gives us  $\delta[n]$  as outputSince LTI,  $\delta[n-n_0] - \frac{1}{2} \delta[n-1-n_0]$  gives us  $\delta[n-n_0]$  as output

$$\text{But } u[n] = \sum_{k=0}^{\infty} \delta[n-k] \rightarrow \text{input is } \sum_{k=0}^{\infty} \delta[n-k] - \frac{1}{2} \delta[n-k-1]$$

$$= \delta[n] - \frac{1}{2} \delta[n-1] + \delta[n-2] - \frac{1}{2} \delta[n-2-1] + \delta[n-3] + \dots$$

$$= \delta[n] + \frac{1}{2} \sum_{k=1}^{\infty} \delta[n-k]$$

$$x_3[n] = \begin{cases} 1 & n=0 \\ \frac{1}{2} & n \geq 1 \\ 0 & \text{otherwise} \end{cases}$$

Freq Domain

$$H(e^{j\omega}) = \frac{1}{1 - \frac{1}{2} e^{-j\omega}} = \frac{Y(e^{j\omega})}{X(e^{j\omega})}$$

$$X(e^{j\omega}) = (1 - \frac{1}{2} e^{-j\omega}) Y(e^{j\omega})$$

 $\rightarrow$  in inverse system, put in  $\delta[n]$ , get out IFT of

$$1 - \frac{1}{2} e^{-j\omega} = \delta[n] - \frac{1}{2} \delta[n-1]$$

$$\begin{aligned} x_3[n] &= y_3[n] - \frac{1}{2} y_3[n-1] \\ &= \delta[n] - \frac{1}{2} \delta[n-1] \end{aligned}$$

**Question 2.** [25 MARKS]

Note: In some classes, the frequency variable in the discrete time Fourier transform was written as  $\Omega$ , not  $\omega$ . Use the protocol you are comfortable with. In this question, it is written as  $\omega$ .

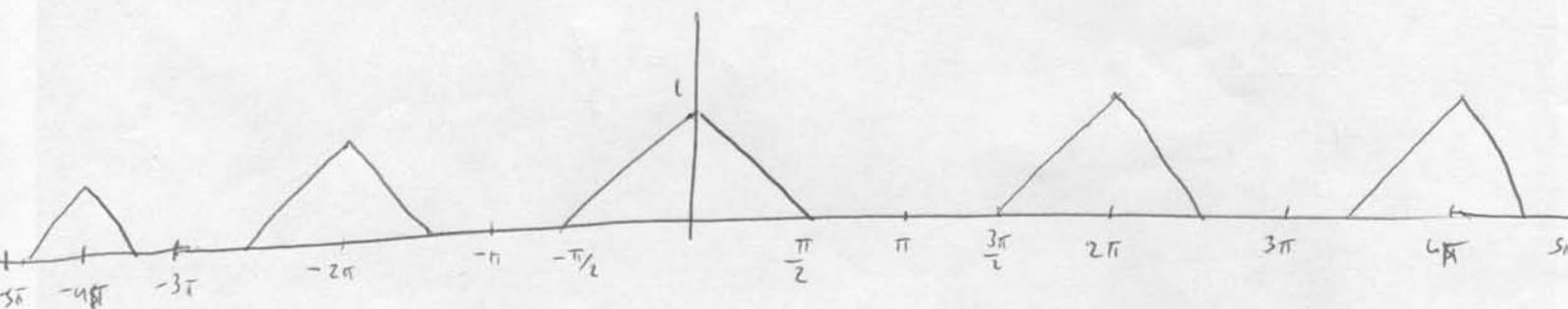
**Part (a)** [4 MARKS]

A discrete time low pass filter is designed such that, in the region  $\omega \in (-\pi, \pi)$ , its transfer function (frequency response)  $H(e^{j\omega})$  is defined by

$$H(e^{j\omega}) = \begin{cases} 1 - \frac{2|\omega|}{\pi} & \text{if } |\omega| \leq \pi/2 \\ 0 & \text{if } |\omega| > \pi/2 \end{cases}$$

Sketch the transfer function (frequency response) in the region  $\omega \in (-5\pi, 5\pi)$ .

$H(e^{j\omega})$  - remember periodic with <sup>period</sup>  $2\pi$

**Part (b)** [3 MARKS]

Is the system described in part (a) causal, i.e.,  $h[n] = 0$  for  $n < 0$ ? Briefly explain your answer.

Tricky - For  $H(e^{j\omega})$  to be real,  $h[n]$  must have even symmetry  
 $\rightarrow h[n]$  is not causal, since even symmetry gives it  $h[n] \neq 0$  for  $n < 0$   
 if  $h[n] \neq 0$  for  $n > 0$

## Part (c) [10 MARKS]

The figure below illustrates a discrete time system composed of two individual systems. The output,  $y[n]$ , is the sum of the two individual outputs, i.e.  $y[n] = y_1[n] + y_2[n]$ .

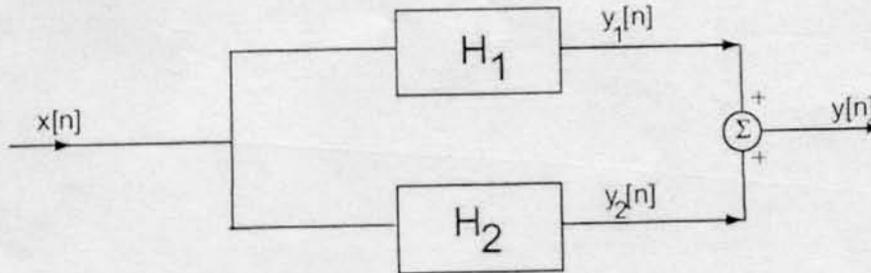


Figure 1: Block diagram for Question 2, Part (c).

The two individual system transfer functions are:

$$H_1(e^{j\omega}) = \frac{1}{1 - 0.5e^{-j(\omega+\pi/3)}}$$

$$H_2(e^{j\omega}) = \frac{1}{1 - 0.5e^{-j(\omega-\pi/3)}}$$

Find the linear constant-coefficient difference equation relating the input  $x[n]$  and the overall output  $y[n]$ . The coefficients are real and must be written as such. Note:  $e^{j\pi/3} = \cos(\pi/3) + j\sin(\pi/3) = 0.5 + j\sqrt{3}/2$ .

$$Y(z) = Y_1(z) + Y_2(z) = X(z) * h_1(z) + X(z) * h_2(z)$$

$$= X(z) * [h_1(z) + h_2(z)]$$

$$\Rightarrow Y(e^{j\omega}) = X(e^{j\omega}) (H_1(e^{j\omega}) + H_2(e^{j\omega}))$$

$$= X(e^{j\omega}) \left( \frac{1}{1 - 0.5e^{-j(\omega+\pi/3)}} + \frac{1}{1 - 0.5e^{-j(\omega-\pi/3)}} \right)$$

$$= X(e^{j\omega}) \left( \frac{2 - 0.5e^{-j(\omega+\pi/3)} - 0.5e^{-j(\omega-\pi/3)}}{1 - 0.5e^{-j(\omega+\pi/3)} - 0.5e^{-j(\omega-\pi/3)} + 0.25e^{-2j\omega}} \right)$$

$$Y(e^{j\omega}) [1 - 0.5e^{-j(\omega-\pi/3)} - 0.5e^{-j(\omega+\pi/3)} + 0.25e^{-2j\omega}] = X(e^{j\omega}) [2 - 0.5e^{-j(\omega+\pi/3)} - 0.5e^{-j(\omega-\pi/3)}]$$

$$\text{OR } y[n] - 0.5e^{j\pi/3} y[n-1] - 0.5e^{-j\pi/3} y[n-1] + 0.25 y[n-2] = 2x[n] - 0.5e^{j\pi/3} x[n-1] - 0.5e^{-j\pi/3} x[n-1]$$

$$y(n) - \underbrace{\frac{1}{2}(e^{j\pi/3} + e^{-j\pi/3})}_{\cos \pi/3 = 1/2} y(n-1) + \frac{1}{4} y(n-2) = 2x(n) - \underbrace{\frac{1}{2}(e^{j\pi/3} + e^{-j\pi/3})}_{\cos \pi/3 = 1/2} x(n-1)$$

$$y(n) - \frac{1}{2} y(n-1) + \frac{1}{4} y(n-2) = 2x(n) - \frac{1}{2} x(n-1)$$

**Part (d) [8 MARKS]**

What is the impulse response  $h[n]$  for the overall system in part (c)?

$$H(e^{j\omega}) = H_1(e^{j\omega}) + H_2(e^{j\omega})$$

$$H_1(e^{j\omega}) = \frac{1}{1 - \frac{1}{2}e^{-j(\omega + \pi/3)}} \quad H_2(e^{j\omega}) = \frac{1}{1 - \frac{1}{2}e^{-j(\omega - \pi/3)}}$$

$$h(n) = h_1(n) + h_2(n)$$

$$G(e^{j\omega}) = \frac{1}{1 - \frac{1}{2}e^{-j\omega}} \rightarrow g(n) = \left(\frac{1}{2}\right)^n u(n)$$

~~h(n)~~

$$\rightarrow H_1(e^{j\omega}) = G(e^{j(\omega + \pi/3)}) \rightarrow h_1(n) = e^{-j\pi/3 n} g(n) = e^{-j\pi/3 n} \left(\frac{1}{2}\right)^n u(n)$$

$$\text{Similarly } H_2(e^{j\omega}) \rightarrow h_2(n) = e^{j\pi/3 n} \left(\frac{1}{2}\right)^n u(n)$$

$$\begin{aligned} h(n) &= (e^{j\pi/3 n} + e^{-j\pi/3 n}) \left(\frac{1}{2}\right)^n u(n) \\ &= 2 \cos\left(\frac{\pi n}{3}\right) \left(\frac{1}{2}\right)^n u(n) \end{aligned}$$

**Question 3.** [25 MARKS]

As sketched in Figure 2, the signal  $x(t)$  has a continuous-time Fourier transform

$$X(j\omega) = \begin{cases} 1 - \frac{|\omega|}{2\omega_M} & \text{if } |\omega| < \omega_M \\ 0 & \text{if } |\omega| \geq \omega_M \end{cases}$$

where  $\omega_M = 2\pi \times 10^4$  radians/second.

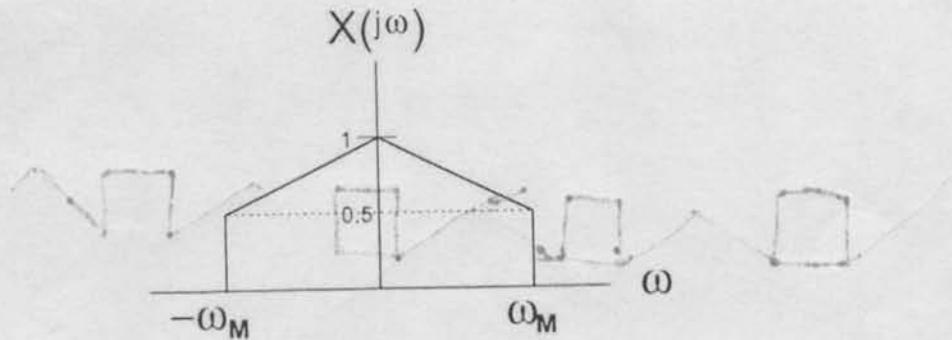


Figure 2: The spectrum of  $x(t)$ .

As shown in Figure 3, the signal  $x(t)$  is sampled by the impulse train  $p(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT)$ , producing  $x_p(t) = x(t)p(t)$ .

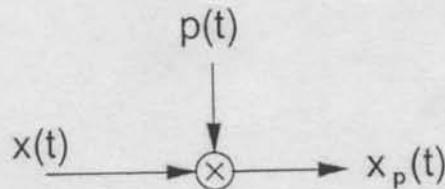


Figure 3: The impulse train sampler producing  $x_p(t) = x(t)p(t)$ .

**Part (a)** [4 MARKS]

In terms of seconds, indicate the range of  $T$  for which aliasing occurs.

Range of  $T$ :

Nyquist Sampling Theorem - For baseband signal bandlimited by  $\omega_M$ , need to sample at  $\omega_s \geq 2\omega_M$  for no aliasing

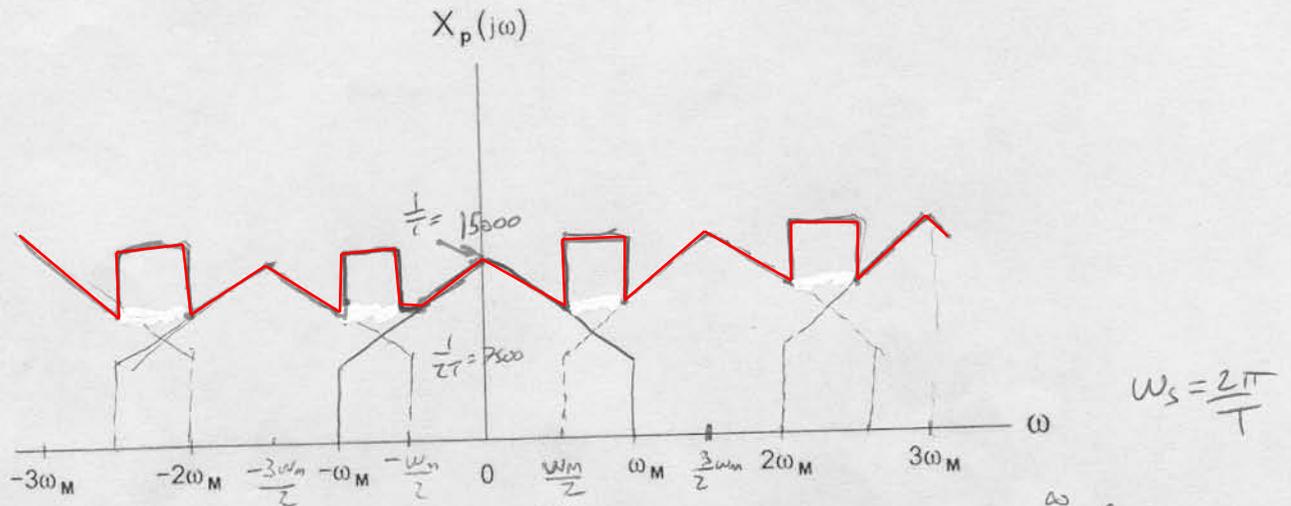
$$T_s = \frac{2\pi}{\omega_s} \leq \frac{2\pi}{2\omega_M} \leq \frac{\pi}{\omega_M} = \frac{\pi}{2\pi \times 10^4 \text{ rad/s}} = \frac{1}{2 \times 10^4} \text{ sec.}$$

$\rightarrow$  If  $T > 0.05 \text{ ms}$ , aliasing occurs

or  $0.05 \text{ msec}$

Part (b) [6 MARKS]

Make a detailed and labelled plot of  $X_p(j\omega)$  for  $-3\omega_M \leq \omega \leq 3\omega_M$ , when  $T = (2/3) \times 10^{-4}$  seconds.



$$X_p(t) = X(t) \sum_{n=-\infty}^{\infty} \delta(t-nT) \rightarrow \sum_{n=-\infty}^{\infty} \delta(t-nT) \text{ has FT } \frac{2\pi}{T} \sum_{k=-\infty}^{\infty} \delta(\omega - n\omega_s)$$

(even though one  $\delta(t)$  has FT of 1  $\rightarrow$  why? since  $\sum$  is periodic)

$$X_p(j\omega) = \frac{1}{2\pi} X(j\omega) * \left( \sum_{n=-\infty}^{\infty} \delta(\omega - n\omega_s) \right) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j(\omega - n\omega_s)) \quad \frac{1}{T} = 15000$$

Here,  $\omega_s = \frac{2\pi}{T} = \frac{2\pi}{\frac{2}{3} \times 10^{-4} \text{ sec}} = 3 \times 10^4 \text{ rad/sec}$  and  $\omega_m = 2\pi \times 10^4 \text{ rad/sec}$

$\rightarrow \omega_s = \frac{3}{2} \omega_m < 2\omega_m \rightarrow$  aliasing

Question 4. [25 MARKS]

Part (a) [13 MARKS]

The filter,

$$H(j\omega) = \begin{cases} j & \text{if } \omega \leq 0 \\ -j & \text{if } \omega > 0 \end{cases}$$

Single side band modulation  
 - more spectrally efficient than double side band  
 → more stations in same spectrum

is used as shown in Figure 5 to create a new signal  $p(t)$  from  $x(t)$ . Assume that  $x(t)$  is real and bandlimited to  $\omega_M$ , which is much less than  $\omega_c$ . Derive  $P(j\omega)$  in terms of  $X(j\omega)$ . Show your work.

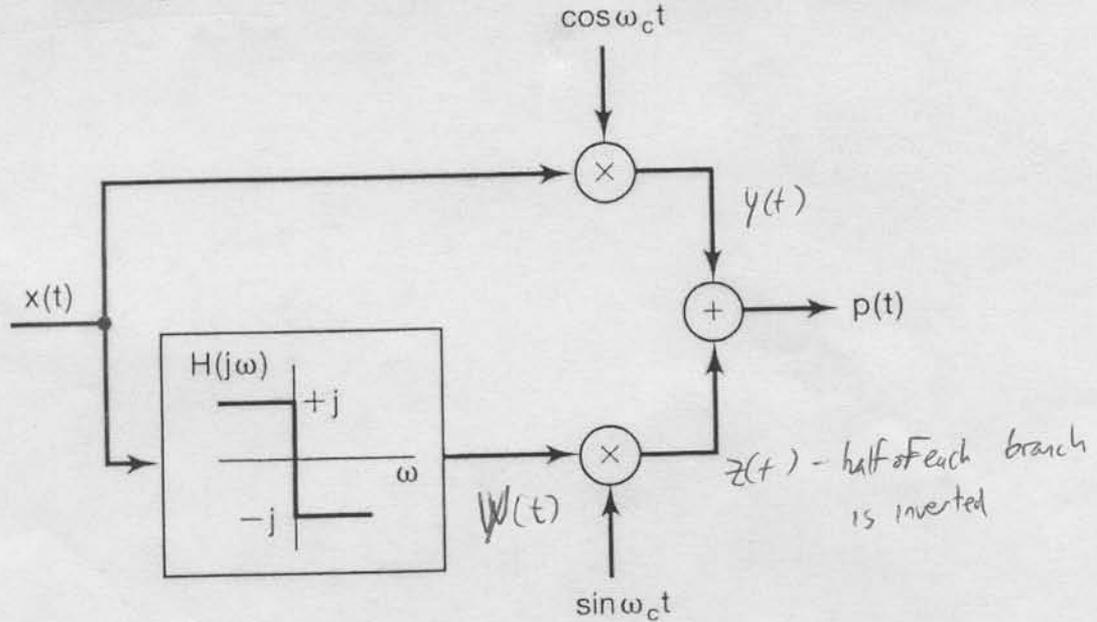


Figure 5: Block diagram for Question 4, Part (a).

$$W(j\omega) = X(j\omega) H(j\omega) = \begin{cases} X(j\omega) & \omega \leq 0 \\ -X(j\omega) & \omega > 0 \end{cases}$$

$$y(t) = x(t) \cos(\omega_c t)$$

$$\Rightarrow Y(j\omega) = \frac{1}{2\pi} X(j\omega) * (\pi \delta(\omega - \omega_c) + \pi \delta(\omega + \omega_c))$$

$$= \frac{1}{2} X(j(\omega - \omega_c)) + \frac{1}{2} X(j(\omega + \omega_c))$$

$$z(t) = w(t) \sin(\omega_c t)$$

$$Z(j\omega) = \frac{1}{2\pi} W(j\omega) * (\frac{\pi}{j} \delta(\omega - \omega_c) - \frac{\pi}{j} \delta(\omega + \omega_c)) = \frac{1}{2j} W(j(\omega - \omega_c)) - \frac{1}{2j} W(j(\omega + \omega_c))$$

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$$\text{Let } V(j\omega) = \begin{cases} X(j\omega) & \omega \leq 0 \\ -X(j\omega) & \omega > 0 \end{cases}$$

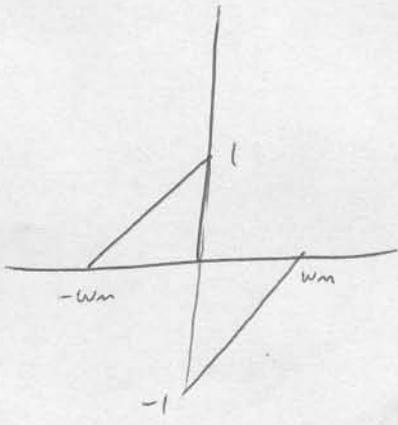
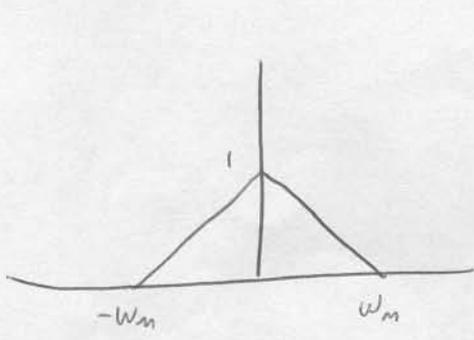
$$= \frac{1}{2} V(j(\omega - \omega_c)) - \frac{1}{2} V(j(\omega + \omega_c))$$

Response to 4a (cont)

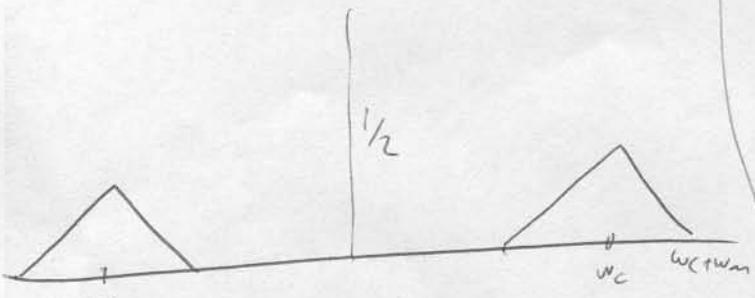
$$P(j\omega) = Y(j\omega) + Z(j\omega)$$

$$= \frac{1}{2} \left[ X(j(\omega - \omega_c)) + X(j(\omega + \omega_c)) + U(j(\omega - \omega_c)) - U(j(\omega + \omega_c)) \right]$$

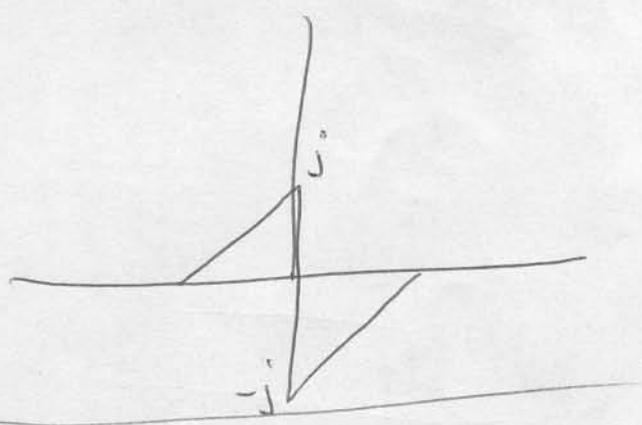
ie  $X(j\omega) \rightarrow W(j\omega)$



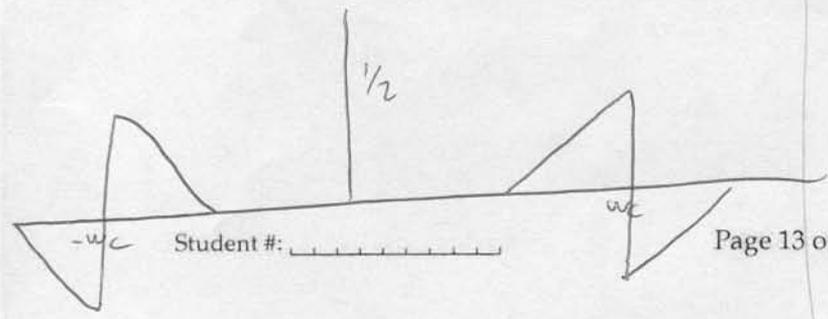
$Y(j\omega)$



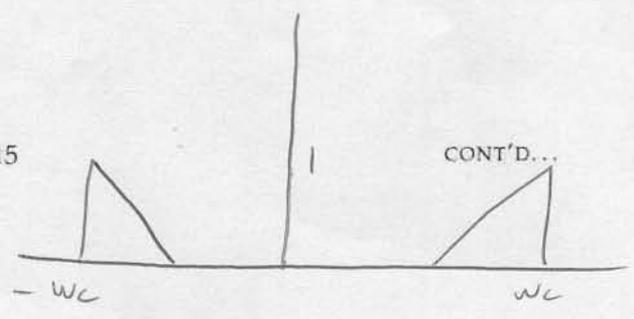
$W(j\omega)$



$Z(j\omega)$



$P(j\omega)$

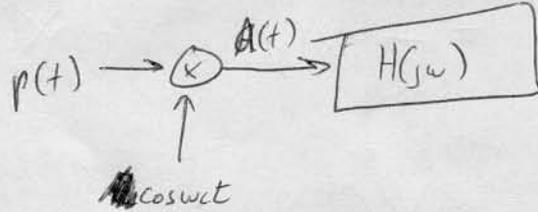
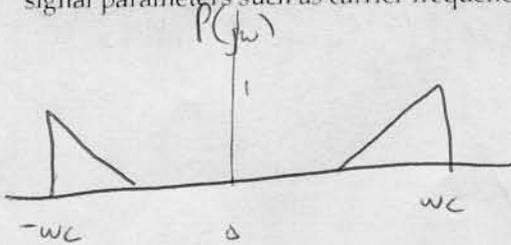


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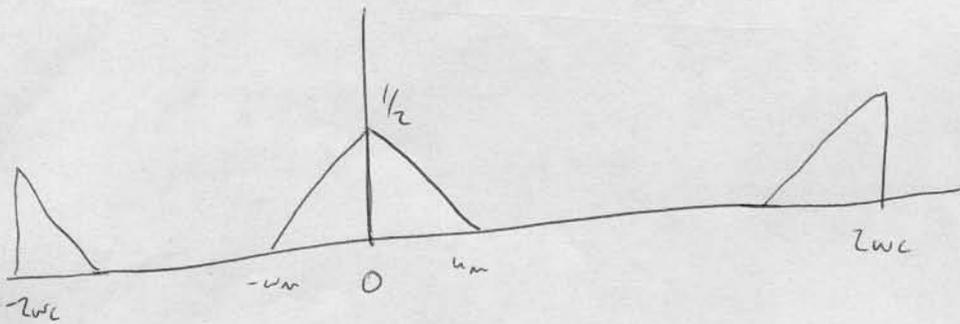
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Part (b) [8 MARKS]

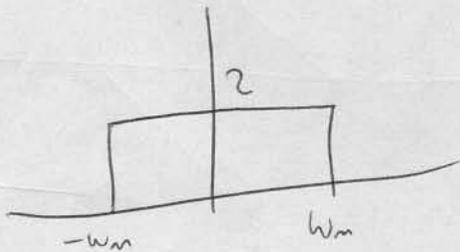
Devise a receiver to recover  $X(j\omega)$  from  $P(j\omega)$ , i.e., a system that takes  $p(t)$  as input and outputs  $x(t)$ . Draw a block diagram of your receiver. Clearly label key parameters of the receiver and relate them to signal parameters such as carrier frequency  $\omega_c$  and bandwidth  $\omega_M$ .



$A(j\omega)$



$H(j\omega)$



Part (c) [4 MARKS]

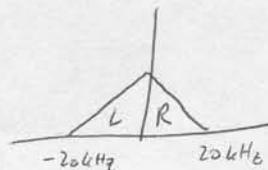
Assume that a real band-limited audio signal whose Fourier transform extends from -20 kHz to 20 kHz is to be transmitted by a radio station. Further, let that station share the radio spectrum from 10 MHz to 20 MHz with other stations transmitting different audio signals that are also real and band-limited with Fourier transforms extending from -20 kHz to 20 kHz. Each station employs a transmitting scheme as shown in Figure 5, but each uses a different carrier frequency  $\omega_c$ . What is the maximum number of stations that you can fit into the assigned spectrum without their spectra overlapping? Justify your answer.

$\omega_m = 20 \text{ kHz} \Rightarrow$  uses spectrum of 10 MHz (20-10)

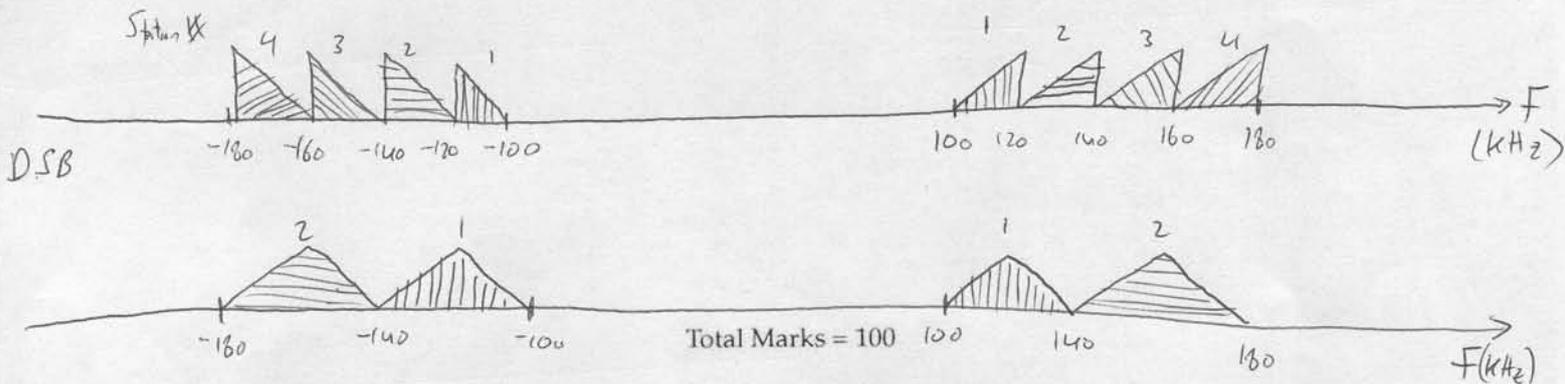
$\Rightarrow$  can fit in  $\frac{10 \times 10^6}{20 \times 10^3} = 500$  channels

As opposed to DSB - each would need 40 kHz  $\Rightarrow$  only 250 channels  
 $\uparrow$   
 Double sideband

Eg IF each station has spectrum  $X(f)$ , and 80 kHz available bandwidth from 100-180 kHz



SSB



Student #: \_\_\_\_\_