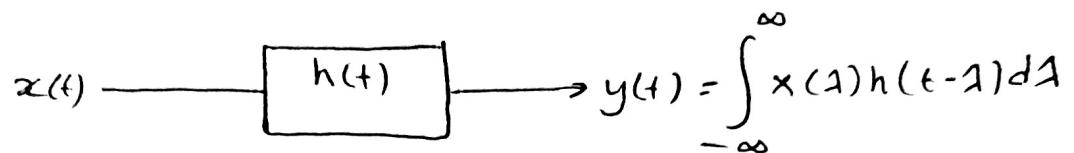


# System Analysis with the FT

## A Signal Transmission through LTI Systems

In Ch. 2, time-domain evaluation of the output is conducted using Convolution Integral



In Ch. 4,



$h(t)$  is the impulse response

$H(f)$  is the frequency response (Transfer function)

Either  $h(t)$  or  $H(f)$  are equally good characterizations of the system.

since  $H(f)$ , is in general, a complex quantity,

$$\Rightarrow H(f) = |H(f)| e^{j \angle H(f)}$$

$|H(f)|$ : amplitude Response fun.

$\angle H(f)$  : phase = s.

$$|Y(f)| = |X(f)| |H(f)|$$

$$\angle Y(f) = \angle H(f) + \angle X(f)$$

Three ways to obtain  $H(f)$ :

- ① Fourier - Transforming the differential equation relating input and output

- apply KVL:-

$$x(t) = Ri(t) + y(t)$$

$$i(t) = C \frac{dy(t)}{dt}$$

$$\Rightarrow RC \frac{dy(t)}{dt} + y(t) = x(t)$$

- Assuming the system to be initially at rest, the diff. equation becomes in freq. domain:-

$$RC \left\{ j2\pi f Y(f) \right\} + Y(f) = X(f)$$

$$(j2\pi f RC + 1) Y(f) = X(f)$$

$$\begin{aligned} \Rightarrow H(f) &= \frac{Y(f)}{X(f)} = \frac{1}{1 + j(2\pi f RC)} = \frac{1}{1 + j\left(\frac{f}{f_3}\right)} \\ &= \frac{1}{\sqrt{1 + \left(\frac{f}{f_3}\right)^2}} e^{-j \tan^{-1}\left(\frac{f}{f_3}\right)} \end{aligned}$$

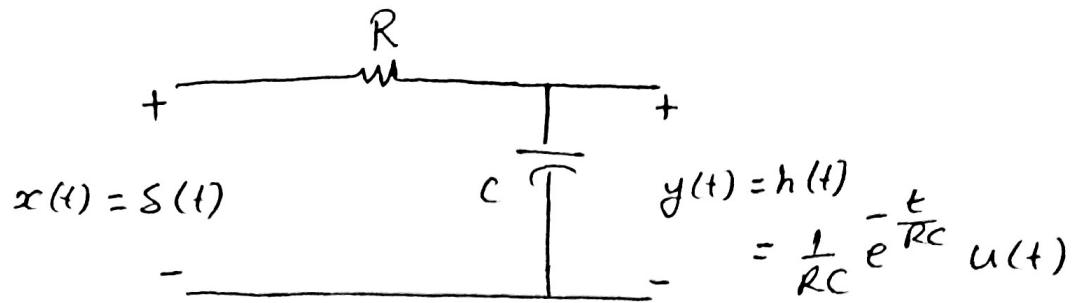
where  $f_3 = \frac{1}{2\pi RC}$  is called the 3-dB or Half-power frequency.

The Half-power freq. of a two-port system is defined as a freq. of an input sine wave which results in a steady-state sinusoidal output of amplitude ( $\frac{1}{\sqrt{2}}$ ) of the max. possible amplitude of the output sinusoid.

The Power of the output is then  $\frac{1}{2}$  of the max. possible output power.  $\left(\frac{P_{out}}{P_{max}}\right) dB = 10 \log \frac{1}{2} = -3dB$

- equivalently, we can use Laplace Transform theory by replacing  $j2\pi f$  by  $s$ .

- Second method, obtaining the impulse response of the system and finding its FT.

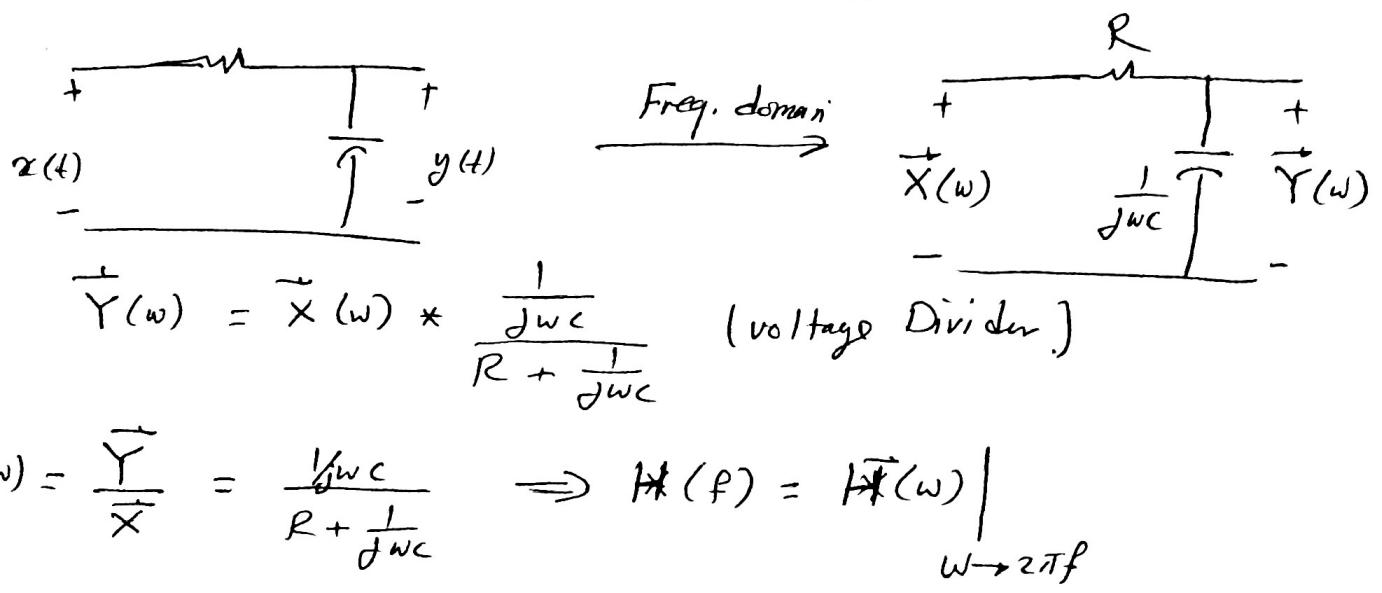


From FT table :-

$$e^{-\alpha t} u(t), \alpha > 0 \longleftrightarrow \frac{1}{s + j2\pi f}$$

$$\Rightarrow H(f) = \frac{1/RC}{\frac{1}{RC} + j2\pi f} = \frac{1}{1 + j(\frac{1}{RC})f} = \frac{1}{1 + j(\frac{f}{f_3})}$$

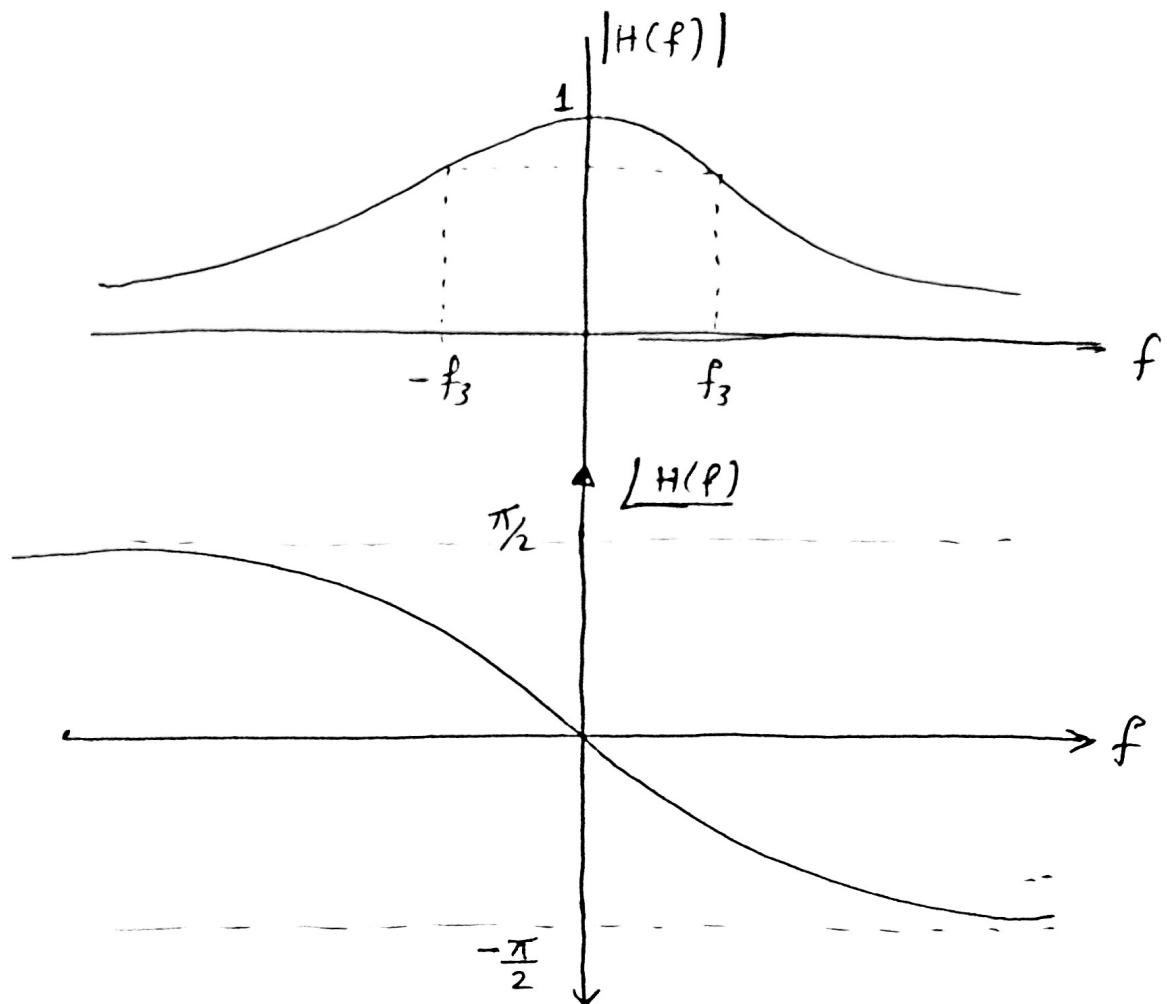
- A third method is to use ac sinusoidal steady-state analysis as shown in the figure, below, and find the ratio of output to input phasors  $\frac{\bar{Y}}{\bar{X}}$



the amplitude and phase response for a low-pass RC filter

$$H(f) = \frac{1}{1+j(f/f_3)} = \frac{1}{\sqrt{1+(f/f_3)^2}} e^{-j \tan^{-1}(f/f_3)}$$

$$H(f) = \left[1 + \left(\frac{f}{f_3}\right)^2\right]^{-\frac{1}{2}} \quad \text{and} \quad \underline{H(f)} = -\tan^{-1}\left(\frac{f}{f_3}\right)$$



# Distortion less Transmission

- Distortion less systems are loved by communication engineers.



- The conditions for distortion less (in time-domain)
  - fixed-amplitude scale ( $K$ )
  - constant delay ( $t_d$ )

$$Y(f) = K X(f) e^{-j 2\pi f t_d}$$

$$\frac{Y(f)}{X(f)} = H(f) = K e^{-j 2\pi f t_d}$$

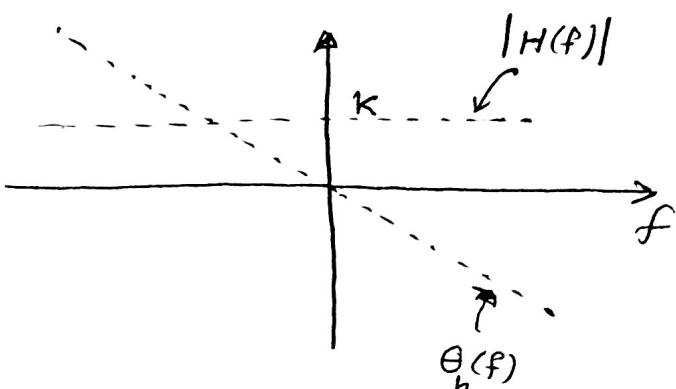
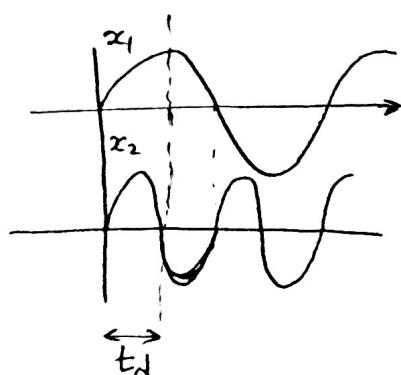
$$\Rightarrow |H(f)| = K$$

$$\cancel{\theta_H(f)} = -2\pi f t_d = \Theta_h(f)$$

$$\Rightarrow t_d = -\frac{1}{2\pi} \frac{d\Theta_h}{df}$$

- This translates in frequency-domain to
  - constant amplitude response  $|H(f)|$
  - Linear phase  $\Theta_h(f)$

- Why linear phase requirements? (physical explanation)
- let  $x(t) = x_1 + x_2$



If we shift by  $t_d$  amplitude wise  $\rightarrow$  no problem  
 phase wise  $\theta_{x_1} = 90^\circ$ ,  $\theta_{x_2} = 180^\circ \rightarrow$  doubled since  $f$  is double.

- There are two forms of distortion :-

### ① Amplitude Distortion

Audio applications are sensitive to amplitude distortion

### ② Phase Distortion

Video applications are sensitive to phase change

(Read text p. 94-95 Lathi 4<sup>th</sup> ed.)

Example Consider the system characterized by  $H(f)$ .

find the response of the system to the input

$$x(t) = A e^{-\alpha t} u(t), \quad \alpha > 0, \quad H(f) = \frac{1}{1 + j f/f_3}, \quad f_3 = 2\pi RC$$

Sol. using FT table:-

$$X(f) = \frac{A}{\alpha + j 2\pi f}$$

$$\Rightarrow Y(f) = H(f) X(f) = \frac{A/RC}{(\alpha + j 2\pi f)(\frac{1}{RC} + j 2\pi f)}$$

• let  $\alpha \neq \frac{1}{RC}$  (distinct Roots.)

using Partial Fraction Expansion (PFE):-

$$Y(f) = \frac{M_1}{\alpha + j 2\pi f} + \frac{M_2}{\frac{1}{RC} + j 2\pi f}$$

$$M_1 \Big|_{j 2\pi f = -\alpha} = \frac{A/RC}{\frac{1}{RC} - \alpha} = \frac{-A}{\alpha RC - 1}$$

$$M_2 \Big|_{j 2\pi f = -\frac{1}{RC}} = \frac{A/RC}{\alpha - \frac{1}{RC}} = \frac{A}{\alpha RC - 1}$$

$$\Rightarrow Y(f) = \frac{A}{\alpha RC - 1} \left[ \frac{1}{j RC + j 2\pi f} - \frac{1}{\alpha + j 2\pi f} \right]$$

$$\Rightarrow y(t) = \frac{A}{(\alpha RC - 1)} \left[ e^{-\frac{t}{RC}} - e^{-\alpha t} \right] u(t)$$

Exercise:

Find the response when  $\alpha = \frac{1}{RC}$  (Repeated Root)

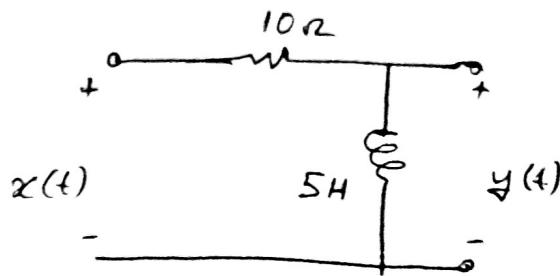
then  $Y(f) = \frac{A/RC}{\left(\cancel{\frac{1}{RC}} + j2\pi f\right)^2}$

Sol.

$$y(t) = \frac{A}{RC} t e^{-\frac{1}{RC} \cdot t} u(t).$$

---

### Example



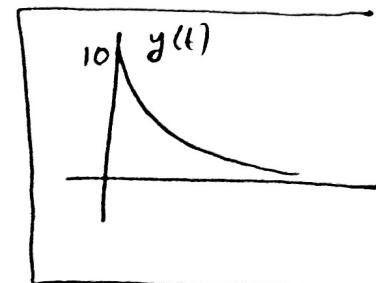
A) let  $x(t) = 10 u(t)$ , find the step response.

$$\text{Sol. } H(\omega) = \frac{Y(\omega)}{X(\omega)} = \frac{j\omega L}{j\omega L + R} = \frac{j\omega}{j\omega + R/L}$$

$$H(f) = H(\omega) \Big|_{\omega=2\pi f} = \frac{j2\pi f}{j2\pi f + 2}$$

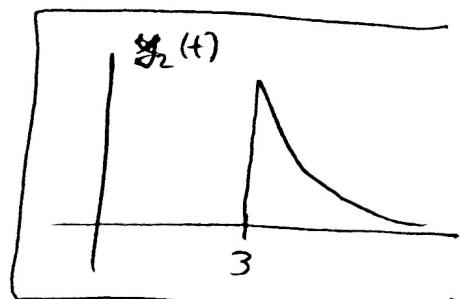
$$\begin{aligned} Y(f) &= H(f) \cdot X(f) \\ &= \frac{j2\pi f}{j2\pi f + 2} \cdot 10 \left[ \frac{1}{j2\pi f} + \frac{\delta(f)}{2} \right] \\ &= \frac{10 \cdot j2\pi f}{j2\pi f + 2} \cdot \frac{1}{j2\pi f} + \frac{10 \cdot j2\pi f}{j2\pi f + 2} \cdot \frac{\delta(f)}{2} \\ &= \frac{10}{j2\pi f + 2} + 0 \end{aligned}$$

$$y(t) = \mathcal{F}^{-1} \left\{ \frac{10}{j2\pi f + 2} \right\} = 10 e^{-2t} u(t)$$



Exercise show that when  $x_2(t) = 10 u(t-3)$ , the output will be

$$y_2(t) = 10 e^{-2(t-3)} u(t-3).$$



Example Consider the RL system given by

$$H(f) = \frac{j2\pi f}{j2\pi f + 2}$$

Find the system response for  $x(t) = 10 \Pi\left(\frac{t-3/2}{3}\right)$ ?

Sol.  $\Pi\left(\frac{t-3/2}{3}\right) = \begin{cases} 1 & -\frac{1}{2} < \frac{t-3/2}{3} \leq \frac{1}{2} \\ 0 & \text{else} \end{cases} = 0 \leq t \leq 3$

one can write  $x(t) = 10 [u(t) - u(t-3)]$

$$\begin{aligned} y(t) &= \mathcal{F}^{-1}\{H(f)x(f)\} \\ &= \mathcal{F}^{-1}\left\{\frac{j2\pi f}{j2\pi f + 2} \cdot 10 \left[ \left( \frac{1}{j2\pi f} + \frac{\delta(f)}{2} \right) - \left( \frac{1}{j2\pi f} + \frac{\delta(f)}{2} \right) e^{-j2\pi f \cdot 3} \right] \right\} \\ &= 10 \left[ e^{jt} - e^{-2(t-3)} u(t-3) \right] \\ &= \begin{cases} 0 & t < 0 \\ 10 e^{-2t} & 0 < t < 3 \\ 10 [e^{-2t} - e^{-2(t-3)}], & t > 3 \end{cases} \end{aligned}$$

Summary:- Among many applications of the FT,

1) we define the freq. response of a system as the FT of the impulse Response (namely Transfer Function)

2) The Transfer function Describes the relationship between the input and the output signal of a system in freq. Domain.

# Signal Transmission Through LT I system ( periodic signals case ).

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- we have shown earlier that when the input is sinusoidal, the output is sinusoidal with the same frequency but could have different amplitude & different phase. ( in terms of phasors )
- In this section, we will use FT to investigate the relationship between the output and the input when the input is periodic signal.
- a periodic signal  $x(t)$  can be represented in terms of FS as :-

$$x(t) = \sum_{n=-\infty}^{\infty} X_n e^{j2\pi f_0 t}$$

- using the FT pair  $e^{j2\pi f_0 t} \longleftrightarrow \delta(f - n f_0)$
- The FT term by term yield

$$X(f) = \sum_{n=-\infty}^{\infty} X_n \delta(f - n f_0)$$



• in evaluating  $Y(f)$ ,  $H(f) \delta(f - n f_0) = H(n f_0) \delta(f - n f_0)$

$$\begin{aligned} \Rightarrow Y(f) &= \sum X_n H(n f_0) \delta(f - n f_0) \\ &= \sum |X_n| |H(n f_0)| e^{j(\underline{X_n} + \underline{H(n f_0)})} \delta(f - n f_0) \end{aligned}$$

$$y(t) = \sum_{n=-\infty}^{\infty} |X_n| |H(n f_0)| e^{j(2\pi n f_0 + \underline{X_n} + \underline{H(n f_0)})}$$

$$\text{Now, } \begin{cases} x(t) = \sum_{n=-\infty}^{\infty} |X_n| e^{j \angle X_n} e^{j 2\pi f_0 t} \\ y(t) = \sum_{n=-\infty}^{\infty} |X_n| |H(nf_0)| e^{j(\angle X_n + \angle H(nf_0))} e^{j 2\pi f_0 t} \end{cases}$$

The significance of these two equations:-

- the  $n^{\text{th}}$  spectral component  $|X_n|$  appears at the output with amplitude scaled by the amplitude response function  $|H(nf_0)|$
- the phase ~~at~~  $\angle X_n$  is also shifted by the system phase response  $\angle H(nf_0)$

$$|Y_n| = |X_n| |H(nf_0)|$$

$$\angle Y_n = \angle X_n + \angle H(nf_0)$$

### Exercise

Show that, when the input  $x(t) = A \cos(\omega_0 t + \theta_x)$

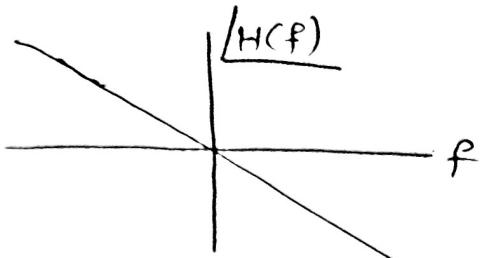
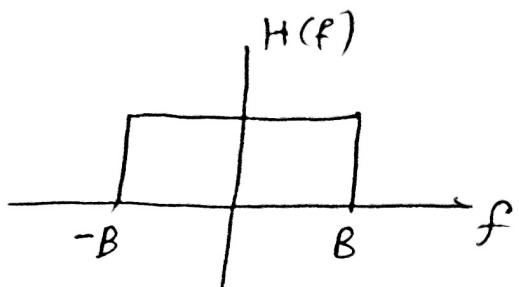
the output  $y(t) = A |H(f_0)| \cos(\omega_0 t + \theta_x + \angle H(f_0))$

Example Consider a system with amplitude- and phase-response functions given by :-

$$|H(f)| = \begin{cases} K & |f| \leq B \\ 0 & \text{o} \end{cases}$$

$$= K \pi \left( \frac{f}{2B} \right)$$

$$\angle H(f) = -2\pi t_0 f$$



Note :-

A filter with this transfer function is referred to as an Ideal Low Pass Filter (LPF) and it is a Distortionless system.

If  $x(t) = A \cos(2\pi f_0 t + \theta_0)$ , find  $y(t)$  ?

Sol one can write  $x(t) = \frac{A}{2} e^{j\theta_0} e^{j2\pi f_0 t} + \frac{A}{2} e^{-j\theta_0} e^{-j2\pi f_0 t}$   
 and  $\Rightarrow x_i = \frac{A}{2} e^{j\theta_0} = x_i^*$ , also  $x_n = 0 \quad \forall n \neq 1, -1$

and use  $y(t) = \sum_{n=-\infty}^{\infty} |x_n| |H(n f_0)| e^{j(\angle x_n + \angle H(n f_0))} e^{jn2\pi f_0 t}$

OR  $y(t) = A |H(f_0)| \cos(2\pi f_0 t + \theta_0 + \angle H(f_0))$

$$= A K \cos(2\pi f_0 t + \theta_0 - 2\pi t_0 f_0)$$

$$= \begin{cases} A K \cos(2\pi f_0(t-t_0) + \theta_0) & f_0 \leq B \\ 0 & f_0 \geq B \end{cases}$$

then, an ideal LPF completely rejects all spectral components with frequencies greater than some cutoff frequency ( $B$ ), and passes all input spectral components below this cutoff frequency except that their amplitudes are multiplied by a constant  $K$  and they are phase shifted by  $(-2\pi t_0 f_0)$  or delayed in time by  $t_0$ .