

# L10: Introduction to FET's

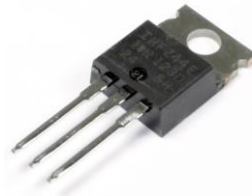
**Analog Electronics**  
**ENEE236**

Instructor: Nasser Ismail

## FET Vs conventional Transistors (BJT)

### Advantages

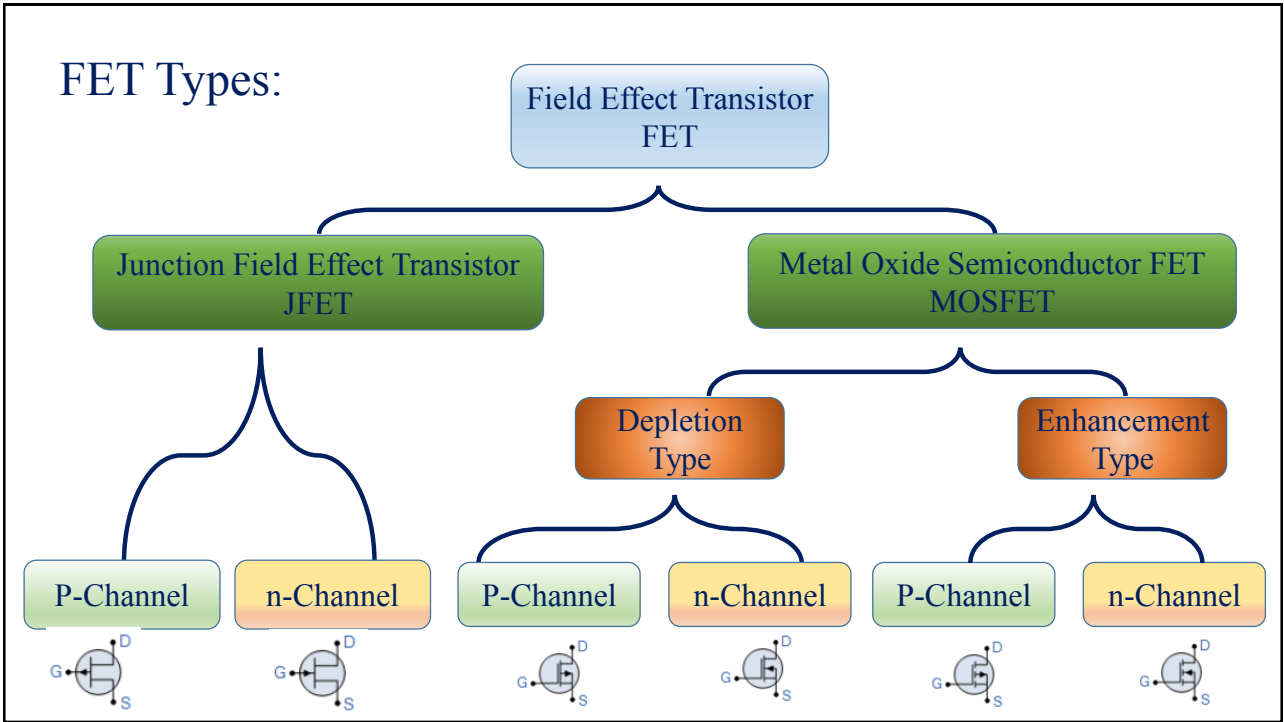
- 1- High input impedance ;  $\sim 100\text{ M}!$
- 2- Fewer steps in manufacturing process.
- 3- More devices can be packaged into smaller area for integrated circuit IC



### Disadvantages

- 1- Low values of voltage gain.
- 2- Poor high frequency performance.

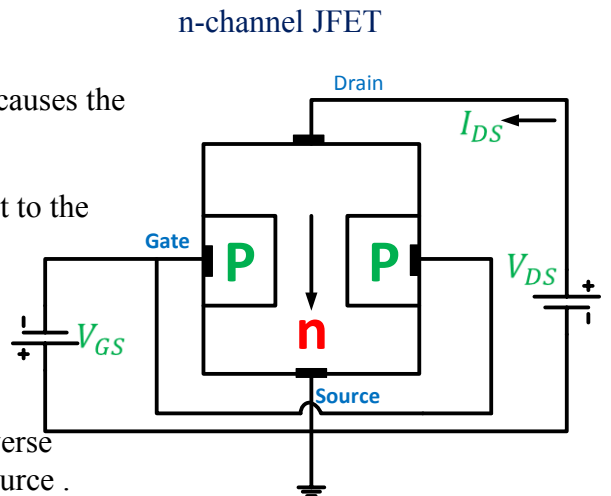




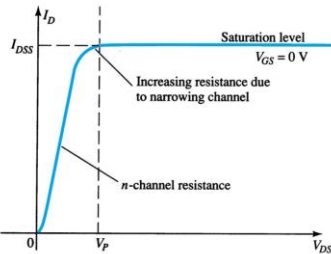
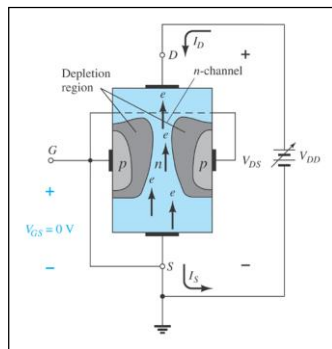
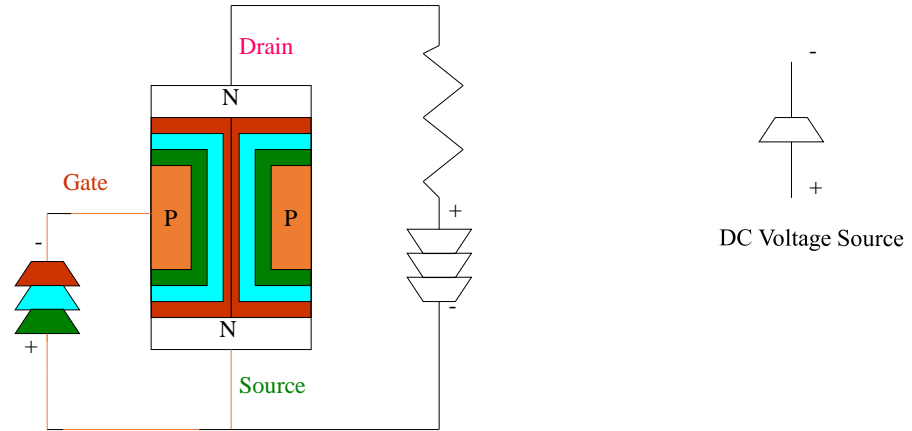
## Junction Field Effect Transistor JFET

### JFET construction:

- ✓ Reverse biasing the gate to source junctions causes the formation of the depletion region
- ✓ The drain has the proper polarity with respect to the source to establish the drain current  $I_{DS}$
- ✓ The value of  $I_{DS}$  depends on the width of the channel.
- ✓ The width of the channel is controlled by reverse biasing the pn-junctions between gate and source .
- ✓ If the channel width increases  $I_{DS}$  increases .

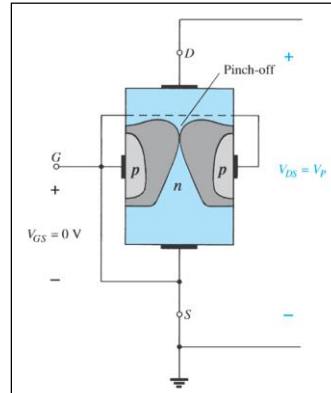
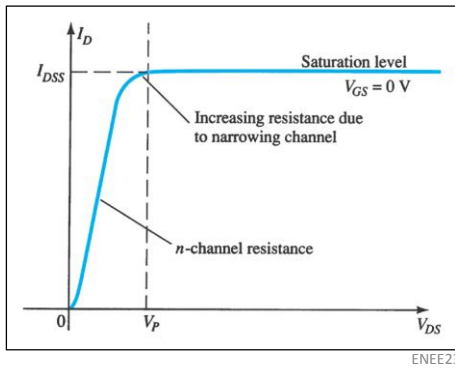


## Operation of a JFET



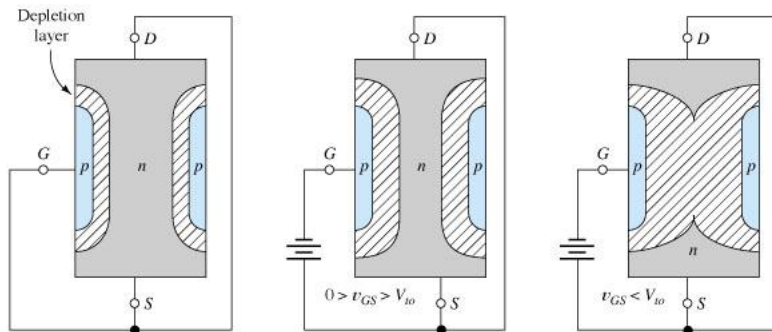
- When  $V_{DD}$  is applied, electrons are drawn to the drain terminal establishing drain current  $I_D$
- Drain and source currents are equivalent ( $I_D = I_S$ )
- $I_D$  is limited by the resistance of the n-channel between the drain and source
- $I_G = 0$  (due to the fact that the pn junction is reverse biased)
- As  $V_{DS}$  is increased,  $I_D$  will also increase according to Ohm's law

- As  $V_{DS}$  is increased towards a value  $V_P$  (pinch off voltage), the depletion region is widened and channel width is reduced increasing resistance to  $I_D$  and the two depletion regions will appear as touching each other
- These two effects result in  $I_D$  being kept almost constant



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### N-Channel JFET Operation



(a) Bias is zero and depletion layer is thin; low-resistance channel exists between the drain and the source  
 (b) Moderate gate-to-channel reverse bias results in narrower channel  
 (c) Bias greater than pinch-off voltage; no conductive path from drain to source

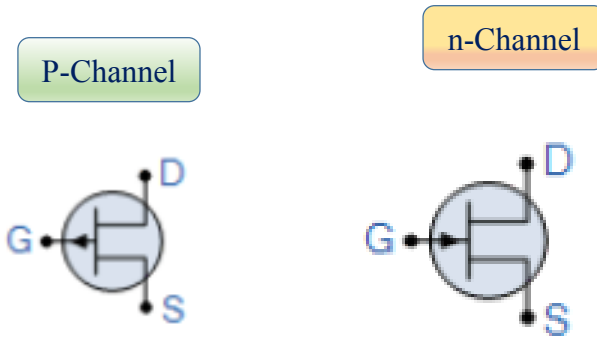
The nonconductive depletion region becomes thicker with increased reverse bias.

(Note: The two gate regions of each FET are connected to each other.)

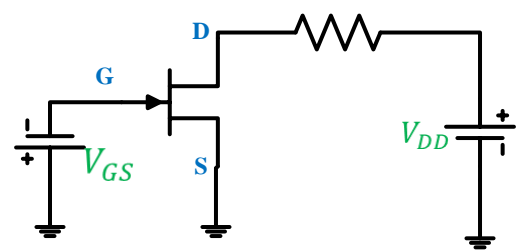
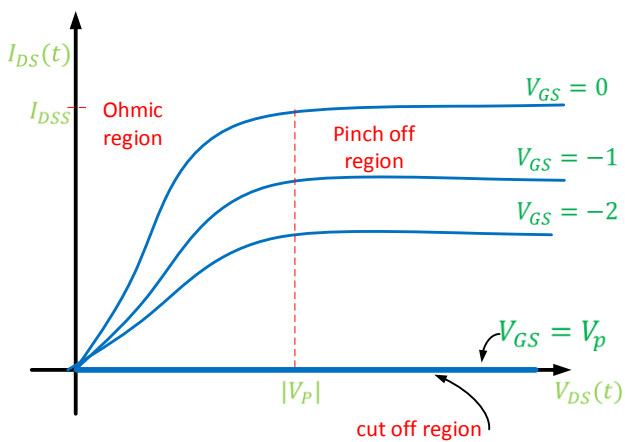
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### JFET Circuit Symbol:



### JFET output characteristic:



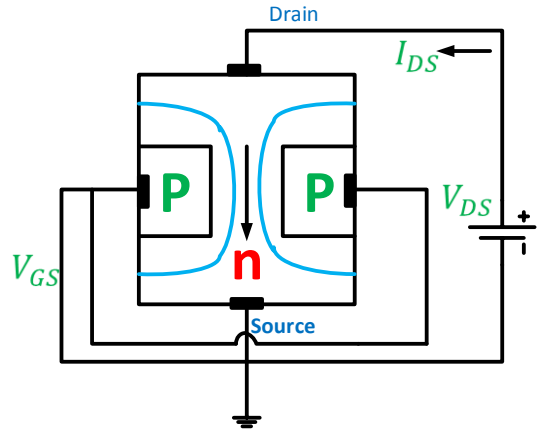
### Pinch of voltage $V_P$ :

For  $V_{GS} = 0$ , the value of  $V_{DS}$  at which  $I_{DS}$  becomes essentially constant  
Is the absolute of the pinch of voltage

$$V_{DS} = |V_P|$$

Some literature refer to  $V_P$  as  $V_{GS(off)}$

$$V_P = \begin{cases} \text{negative value for } n\text{-channel} \\ \text{positive value for } p\text{-channel} \end{cases}$$



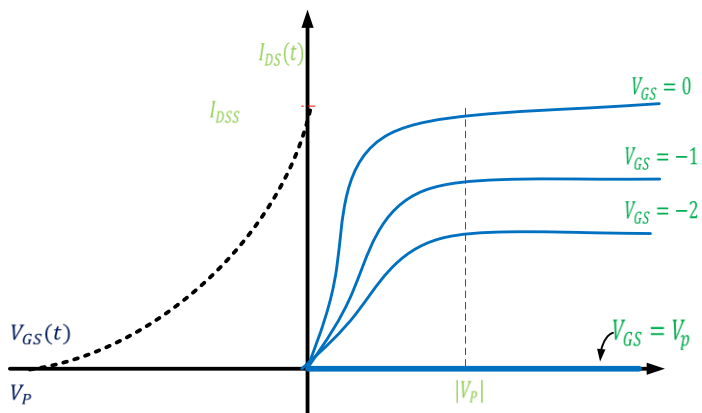
### JFET Transfer characteristic curve:

$$I_{DS}(t) = I_{DSS} \left( 1 - \frac{V_{GS}(t)}{V_P} \right)^2$$

In pinch off region:

$$V_P < V_{GS} \leq 0$$

$$|V_{DS}| > |V_P| - |V_{GS}|$$



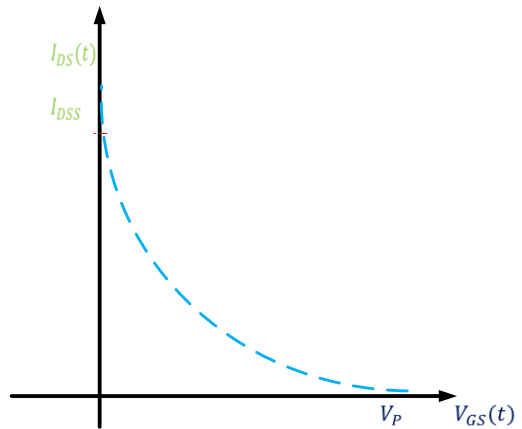
## P-channel JFET

$$I_{DS}(t) = I_{DSS} \left(1 - \frac{V_{GS}(t)}{V_P}\right)^2$$

In pinch off region:

$$|V_{DS}| > |V_P| - |V_{GS}|$$

$$V_P > V_{GS} \geq 0$$



## Pinch off voltage:

✓ The voltage that causes the depletion region to touch and close the channel is called **pinch off voltage**

✓ For the **n-channel** JFET to be in the pinch off region:

$$V_P < V_{GS} \leq 0$$

$$|V_{DS}| > |V_P| - |V_{GS}|$$

✓ For the **p-channel** JFET to be in the pinch off region:

$$|V_{DS}| > |V_P| - |V_{GS}|$$

$$V_P > V_{GS} \geq 0$$

## Common JFET Biasing Circuits

- Fixed-Bias
- Self-Bias
- Voltage-Divider Bias

## Basic Current Relationships

For all FETs:

$$I_G \cong 0 \text{ A}$$

$$I_D = I_S = I_{DS}$$

For JFETS

$$I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$$



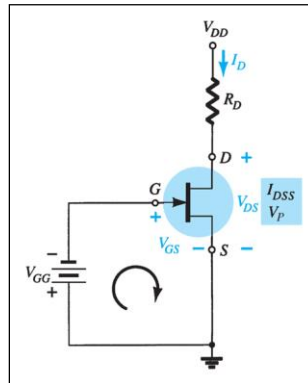
## Fixed-Bias Configuration

$$V_{DS} = V_{DD} - I_D R_D$$

$$V_S = 0 \text{ V}$$

$$\therefore V_D = V_{DS}$$

$$\therefore V_{GS} = -V_{GG}$$



## Example

$$V_{GS} = V_G - V_S = -1.5 - 0 = -1.5 \text{ V}$$

Assuming JFET is in pinch off region

$$1) I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$$

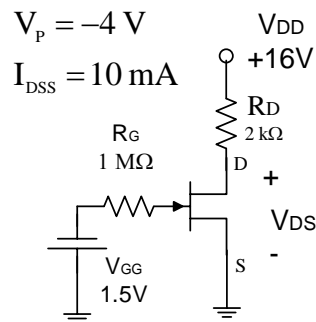
$$= 10 \text{ mA} \left( 1 - \frac{-1.5}{-4} \right)^2$$

$$= 3.9 \text{ mA}$$

$$2) V_{DS} = V_{DD} - I_D R_D$$

$$= 16 - ((2\text{k})(3.9 \text{ mA}))$$

$$= 8.2 \text{ V}$$



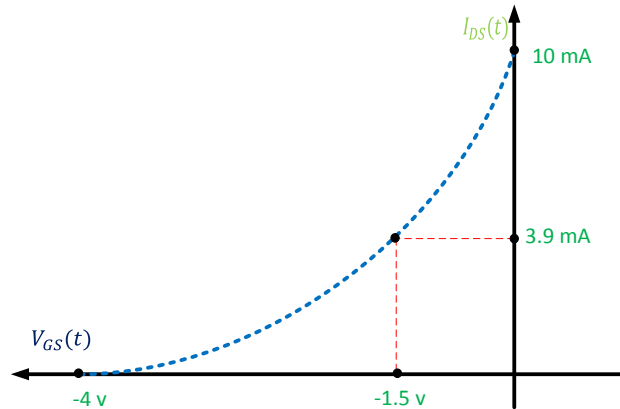
3) check for  $|V_{DS}| > |V_P| - |V_{GS}|$  ?

$$|8.2| > |-4| - |-1.5|$$

assumption is true

## Graphical method:

- $I_{DS} = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$
- $V_{GS} = -1.5 \text{ v}$  Fixed



## Self-Bias Configuration

$$V_{GS} = V_G - V_S = 0 - V_S = -V_S$$

$$V_S = I_D R_S$$

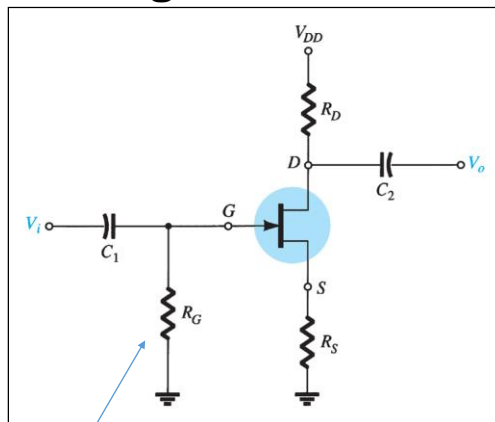
$$V_{GS} = -I_D R_S$$

$$V_D = V_{DD} - I_D R_D$$

$$V_{DS} = V_D - V_S$$

$$= V_{DD} - I_D R_D - I_D R_S$$

$$= V_{DD} - I_D (R_S + R_D)$$



$R_G$  is important to isolate the bac signal from ground in amplifier circuits

## Example

$$V_{GS} = V_G - V_S = 0 - V_S = -V_S$$

$$V_S = I_D R_S = 600 I_D$$

$$V_{GS} = -600 I_D$$

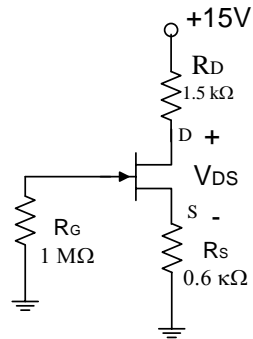
$$1) I_D = 10 \text{ mA} \left( 1 - \frac{-600 I_D}{-4} \right)^2$$

$$ax^2 + bx + c = 0$$

$$x_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$V_P = -4 \text{ V}$$

$$I_{DSS} = 10 \text{ mA}$$



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## Example-continued

solving for  $I_D$  :

$I_{D1} = 14.77 \text{ mA} > I_{DSS}$  and this solution is not possible

$I_{D2} = 3 \text{ mA} \leftarrow$  this is the correct solution

$$2) \therefore V_{GS} = -600 I_D = -600 \times 3 \text{ mA} = -1.8 \text{ V}$$

$$V_D = V_{DD} - I_D R_D$$

$$V_{DS} = V_{DD} - I_D (R_S + R_D) \\ = 15 - 3 \text{ mA} (1 \text{ k} + 0.6 \text{ k}) = 10.2 \text{ V}$$

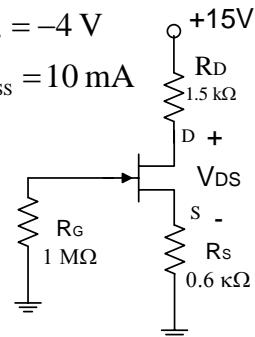
3) check for  $|V_{DS}| > |V_P| - |V_{GS}|$  ?

$$|10.2| > |-4| - |-1.8|$$

assumption is true

$$V_P = -4 \text{ V}$$

$$I_{DSS} = 10 \text{ mA}$$



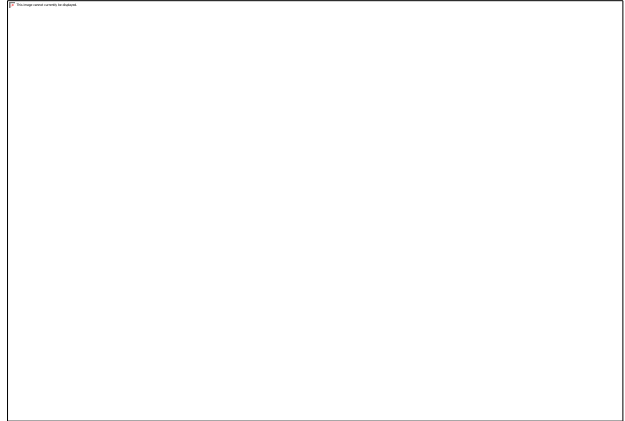
## Graphical method

- $I_{DS} = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$

- $V_{GS} = -(0.6K) I_{DS}$

when  $V_{GS} = 0 \rightarrow I_{DS} = 0 \text{ mA}$

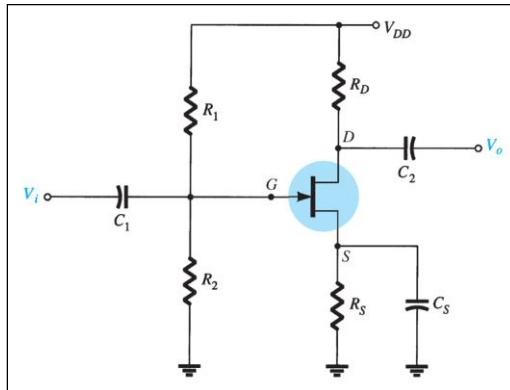
when  $V_{GS} = -3 \text{ V} \rightarrow I_{DS} = 5 \text{ mA}$



## Voltage-Divider Bias

$I_G = 0 \text{ A}$

$I_D$  responds to changes in  $V_{GS}$ .



## Voltage-Divider Bias Calculations

$$I_G = 0 \text{ A}$$

$V_G$  is equal to the voltage across divider resistor  $R_2$ :

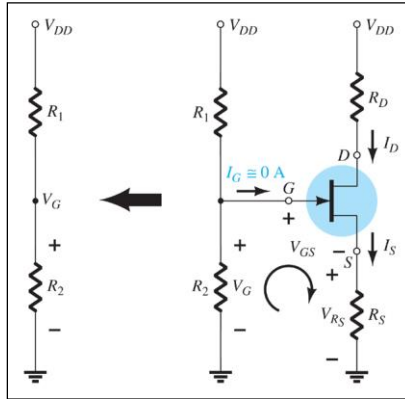
$$V_G = \frac{R_2 V_{DD}}{R_1 + R_2}$$

$$V_S = I_D R_S$$

Using Kirchoff's Law:

$$V_{GS} = V_G - I_D R_S$$

$$V_{GS} = \frac{R_2 V_{DD}}{R_1 + R_2} - I_D R_S$$



The Q-point is established by plotting a line that intersects the transfer curve.

## Example

$V_S$  must be more positive than  $V_G$

to keep the gate – source junction reverse biased

$$V_S = I_D R_S$$

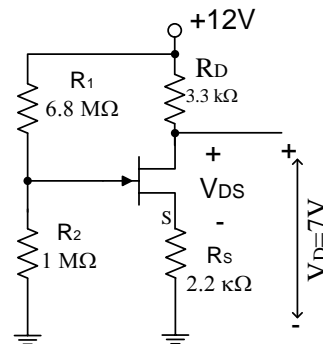
$$V_{GS} = \frac{R_2 V_{DD}}{R_1 + R_2}$$

$$V_{GS} = V_G - I_D R_S$$

$$V_{GS} = \frac{R_2 V_{DD}}{R_1 + R_2} - I_D R_S$$

$$V_D = V_{DD} - I_D R_D = 7 \text{ V}$$

$$I_D = \frac{V_{DD} - V_D}{R_D} = \frac{12 - 7}{3300} = 1.52 \text{ mA}$$



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## Example

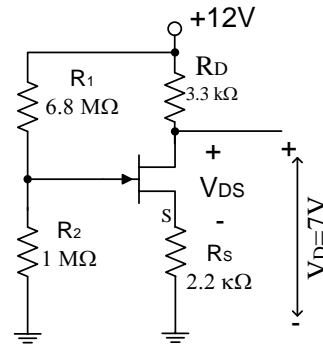
$$V_s = I_D R_s = (1.52 \text{ mA}) (2.2 \text{ k}\Omega) = 3.34 \text{ V}$$

$$V_G = \frac{1 \text{ M}}{1 \text{ M} + 6 \text{ M}} 15 = 1.54 \text{ V}$$

$$V_{GS} = 1.54 - 3.34 = -1.8 \text{ V} < 0 \quad \Leftarrow \text{OK}$$

also

$$I_D = \frac{V_s}{R_s} = \frac{3.34}{2200} = 1.52 \text{ mA}$$



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## Example- $V_D$ unknown

For the same example, if  $V_D$  was not given,

then we use the square law rule  $I_D = f(V_{GS})$

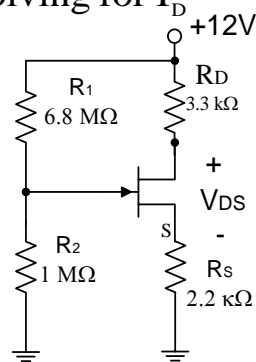
to find  $I_D$  and  $V_{GS}$  by substituting the expression

for  $V_{GS} = \frac{R_2 V_{DD}}{R_1 + R_2} - I_D R_s$  in it and solving for  $I_D$

$$V_{GS} = 1.54 - I_D R_s$$

$$I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$$

$$= I_{DSS} \left( 1 - \frac{1.54 - I_D R_s}{V_P} \right)^2$$



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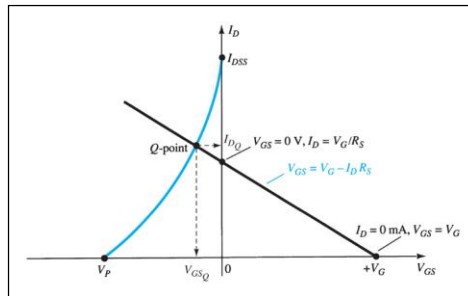
## Voltage-Divider Q-Point

Plot the line that is defined by these two points:

$$V_{GS} = V_G, I_D = 0 \text{ A}$$

$$V_{GS} = 0 \text{ V}, I_D = V_G / R_S$$

Plot the transfer curve by plotting  $I_{DSS}$ ,  $V_P$  and the calculated values of  $I_D$



The Q-point is located where the line intersects the transfer curve

## Example p-channel

$$V_{GS} = \frac{R_2}{R_1 + R_2} (-20) + I_D R$$

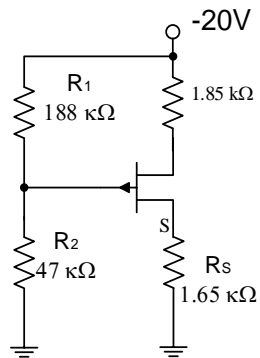
$$V_{GS} = -4 + I_D R_S$$

$$I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$$

$$= I_{DSS} \left( 1 - \frac{-4 + I_D R_S}{V_P} \right)^2$$

$$V_P = 5 \text{ V}$$

$$I_{DSS} = 18 \text{ mA}$$



$$I_D = 18 \text{ mA} \left( 1 - \frac{-4 + 1650 I_D}{5} \right)^2$$

- Solving the quadratic equation and finding its roots yields:

$$I_{D1} = 4.7 \text{ mA}$$

$$I_{D2} = 7.4 \text{ mA}$$

both values of  $I_D < I_{DSS}$  and are possible solutions

so we verify value of  $V_{GS}$  :

$$V_{GS1} = -4 + (4.7 \text{ mA})(1.65 \text{ k}\Omega) = 3.75 \text{ V} < V_p \checkmark \text{ correct solution}$$

$$V_{GS2} = -4 + (7.4 \text{ mA})(1.65 \text{ k}\Omega) = 8.21 \text{ V} > V_p \times \text{ wrong solution}$$

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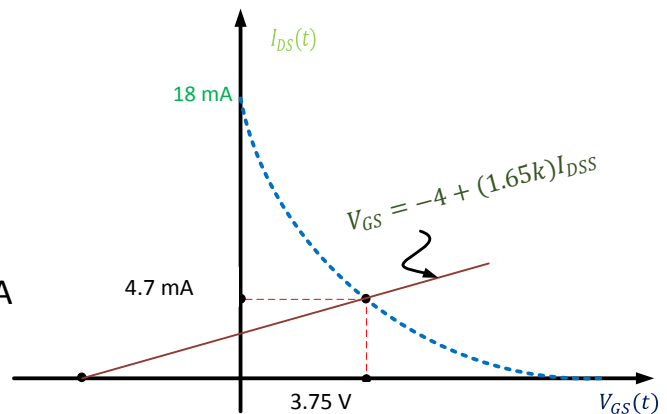
## Graphical method

- $I_{DS} = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$

- $V_{GS} = -4 + (0.6 \text{ K}) I_{DS}$

when  $V_{GS} = -4 \text{ v} \rightarrow I_{DS} = 0 \text{ mA}$

when  $V_{GS} = 0 \text{ v} \rightarrow I_{DS} = 2.42 \text{ mA}$





## Midpoint Bias

### For maximum Symmetrical Swing

- Place Q-point in the middle point of the transfer characteristic to allow for maximum swing between  $I_{DSS}$  and zero

1) let  $I_D = 0.5I_{DSS}$

$$0.5I_{DSS} = I_{DSS} \left( 1 - \frac{V_{GS}}{V_P} \right)^2$$

$$0.5 = \left( 1 - \frac{V_{GS}}{V_P} \right)^2$$

2) let  $V_D = 0.5V_{DD}$



$$\sqrt{\frac{1}{2}} = 1 - \frac{V_{GS}}{V_P}$$

$$\frac{V_{GS}}{V_P} = 1 - \sqrt{\frac{1}{2}}$$

$$V_{GS} = V_P (1 - 0.707)$$

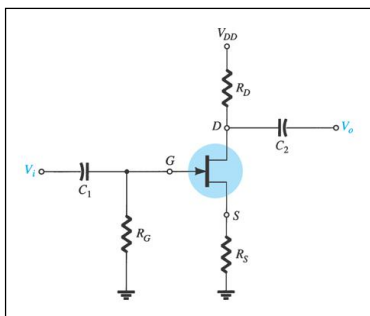
$$= V_P (0.2928)$$

$$\therefore V_{GS} \cong \frac{V_P}{3.41}$$

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## Example



$$V_P = V_{gs(off)} = -3 \text{ V}$$

$$I_{DSS} = 12 \text{ mA}$$

Choose  $R_D$  and  $R_S$  for mid point bias

$$I_D = 0.5I_{DSS} = 6 \text{ mA}$$

$$V_D = 0.5V_{DD} = 6 \text{ V}$$

$$V_{GS} = \frac{V_{GS(off)}}{3.4} = \frac{-3}{3.4} = -0.882 \text{ V}$$

$$R_S = \frac{V_S}{I_S} = \frac{0.882}{6 \text{ mA}} = 147 \Omega$$

$$V_{DD} - I_D R_D - V_D = 0$$

$$R_D = \frac{V_{DD} - V_D}{I_D} = 1 \text{ k}\Omega$$

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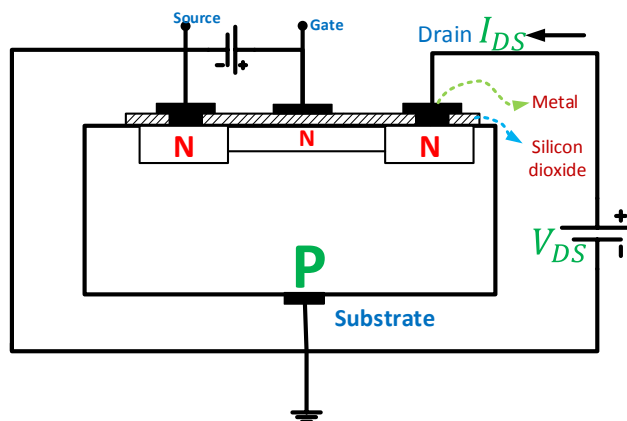
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## Metal Oxide Semiconductor Field Effect Transistor MOSFET

- 1) Depletion type MOSFET: DMOSFET
- 2) Enhancement type MOSFET: EMOSFET
- The MOSFET differs from the JFET in that it has no pn junction structure; instead, the gate of the MOSFET is insulated from the channel by a silicon dioxide ( $SiO_2$ ) layer.
- Due to this the input resistance of MOSFET is greater than JFET.

### Depletion type MOSFET:

- Construction of n-channel DMOSFET:

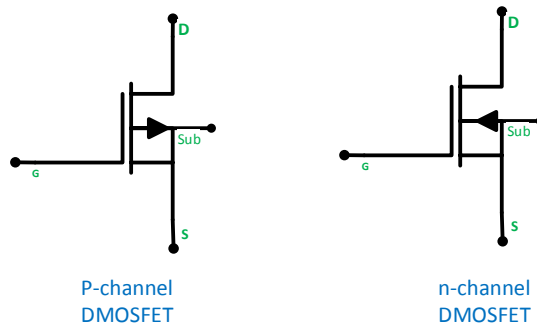


## Operation , characteristic and parameters of DMOSFET

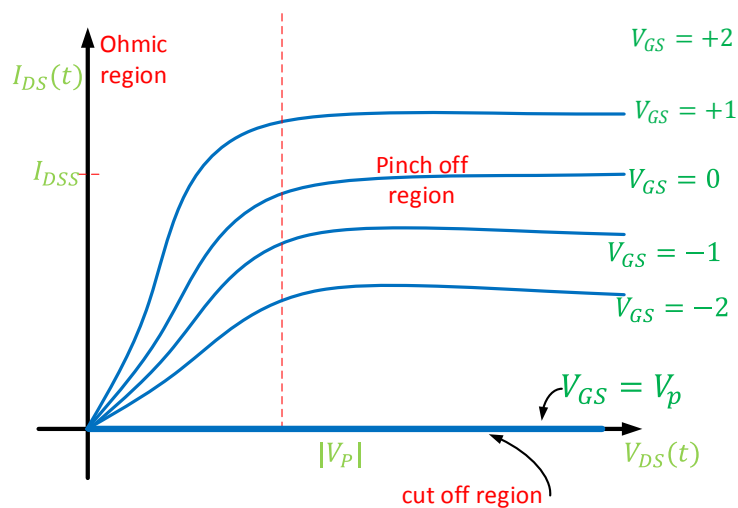
### ◆ n-channel DMOSFET

- On the application of  $V_{DS}$  and keeping  $V_{GS}=0$  electrons from the n-channel are attracted towards positive potential of the drain terminal .
- This establishes current through the channel to be denoted as  $I_{DSS}$  at  $V_{GS}=0$  .
- If we apply negative gate voltage ( $V_{GS} < 0$ ) the negative charge on the gate repel electrons from the channel . The number of repelled electrons depends on the magnitude of the negative voltage  $V_{GS}$ .
- The greater the negative voltage applied at the gate , the level of drain current will reduce until it reaches zero ;  $V_{GS} = V_P$  .

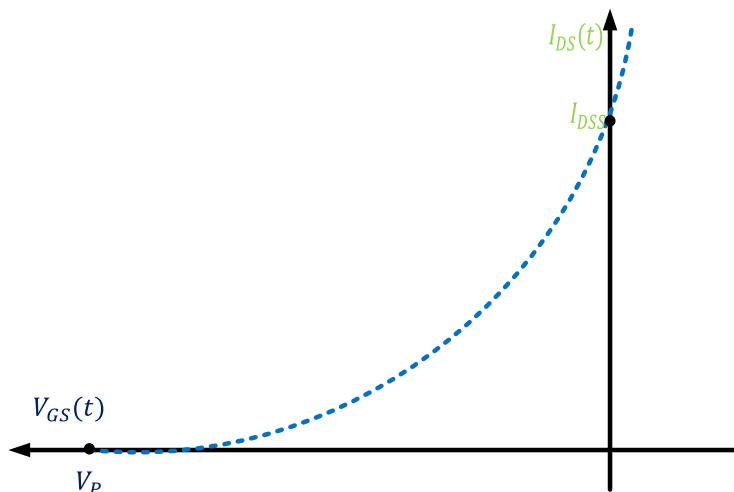
- For positive value of  $V_{GS}$ , the positive gate will draw additional electrons from the p-type substrate and the drain current increases .



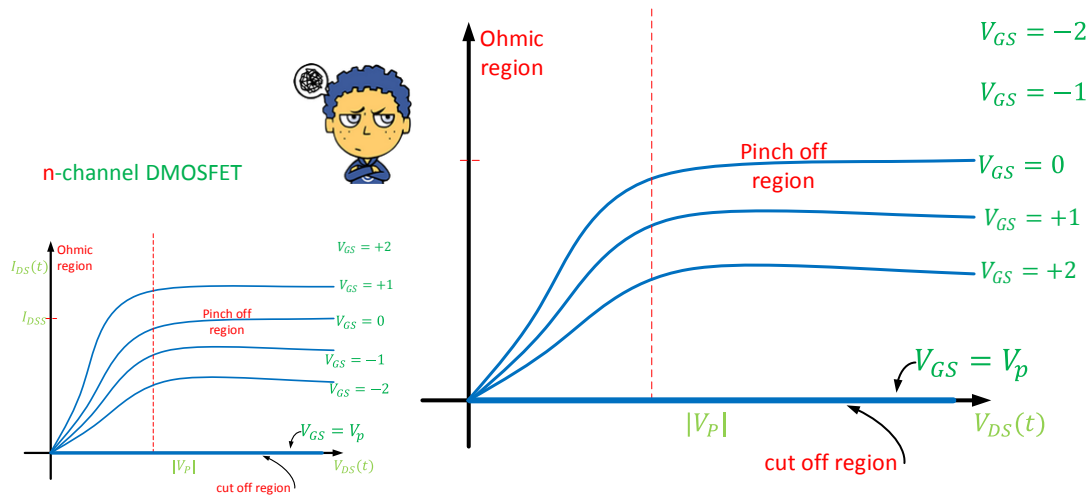
### Drain characteristics for an n-channel DMOSFET



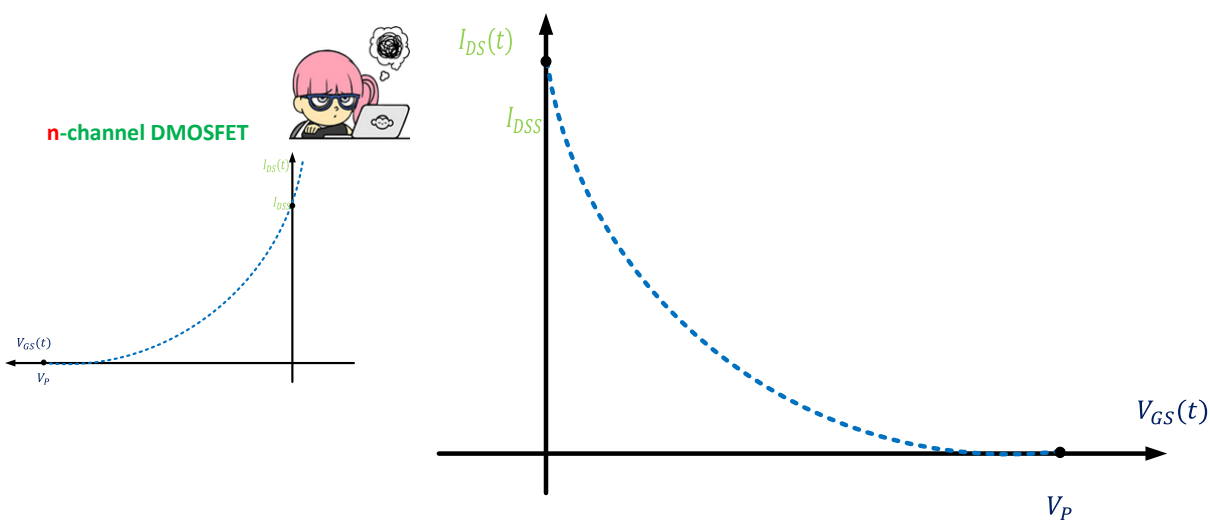
### Transfer characteristics for an n-channel DMOSFET



## Drain characteristics for an p-channel DMOSFET



## Transfer characteristics for an p-channel DMOSFET



## In the pinch off region

$$i_{DS}(t) = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2$$

### ◆ For the n- channel

$$V_{GS} > V_P \text{ (negative)}$$

$$V_{DS} > V_{GS} - V_P$$

### ◆ For the p- channel

$$V_{GS} < V_P \text{ (positive)}$$

$$V_{DS} < V_{GS} - V_P$$

## Example



Suppose that the DMOSFET is in the pinch off region

$$I_{DS} = I_{DSS} \left(1 - \frac{V_{GS}}{V_P}\right)^2 \dots\dots\dots 1$$

$$V_{GS} = V_G - V_S = V_G$$

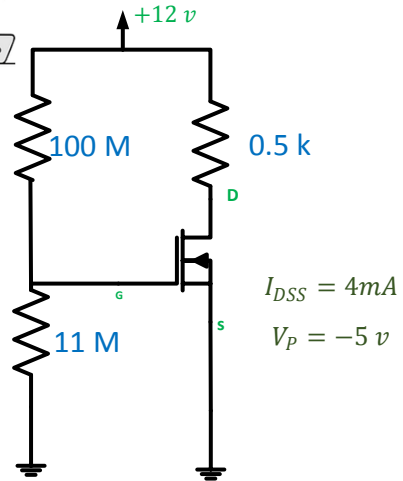
$$V_G = \frac{11M}{11M+100M}(12) = 1.19 \text{ v} \dots\dots\dots 2$$

sub 2 into 1 , we obtain

$I_{DS} = 6.13\text{mA} > I_{DSS}$  !! THIS IS POSSIBLE AND DMOSFET WILL OPERATE IN ENHANCEMENT MODE

$$V_{DS} = V_{DD} - 0.5K I_{DS} = 8.93 \text{ v}$$

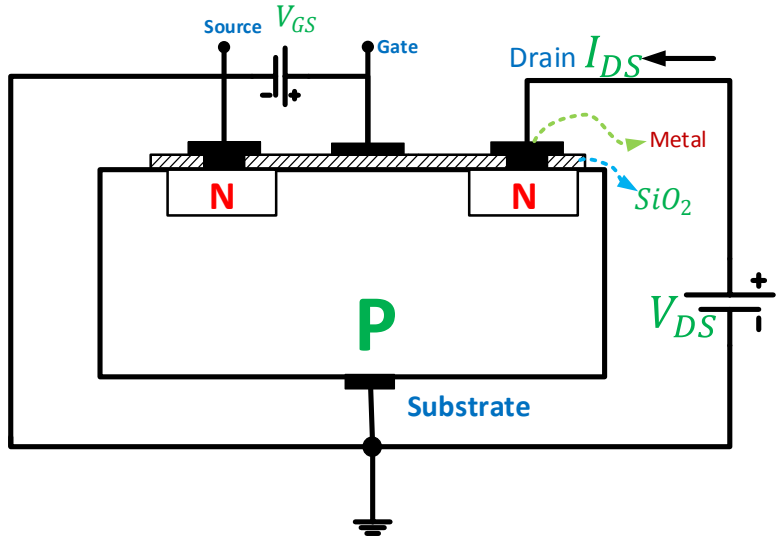
$$V_{DS} > V_{GS} - V_P = 6.19 \text{ v}$$



$$I_{DSS} = 4\text{mA} \quad V_P = -5 \text{ v}$$

## Enhancement Type MOSFET

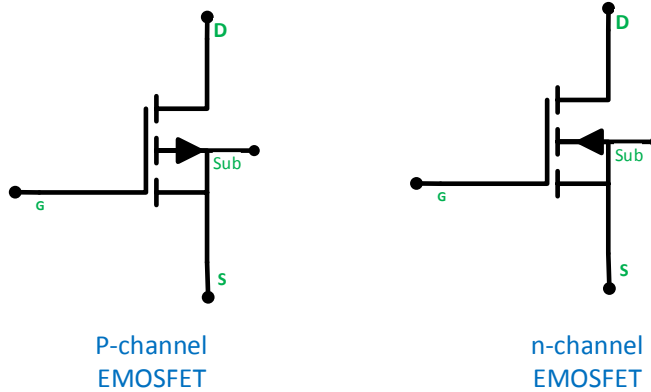
- Construction of n-channel EMOSFET:



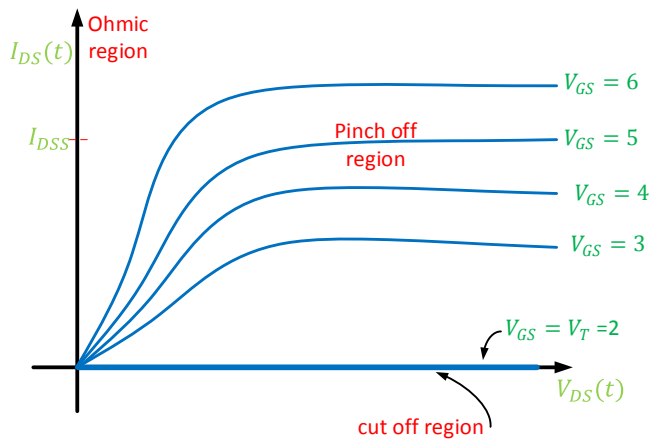
## Operation , characteristic and parameters of EMOSFET

- On the application of  $V_{DS}$  and keeping  $V_{GS}=0$  practically zero current flows .
- If we increase  $V_{GS}$  in the positive direction the concentration of electrons near the  $SiO_2$  surface increases ,
- At particular value of  $V_{GS}$  there is a measurable current flow between drain and source ;  $I_{DS}$  .
- This value of  $V_{GS}$  is called threshold voltage denoted by  $V_T$  or  $V_{GS(TH)}$
- A positive  $V_{GS}$  above  $V_T$  induce a channel and hence the drain current ( $I_{DS}$ ) by creating a thin layer of negative charges (electrons) in the substrate adjacent to the  $SiO_2$  large .

The conductivity of the channel is enhanced by increasing  $V_{GS}$  and thus pulling more electrons into the channel .

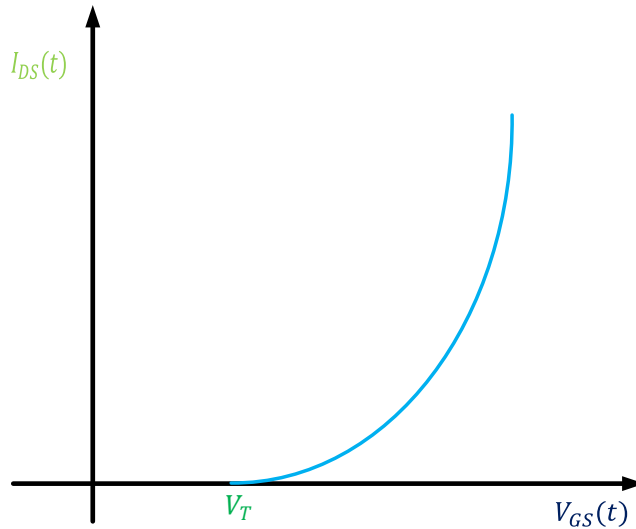


### Drain characteristics for an n-channel EMOSFET



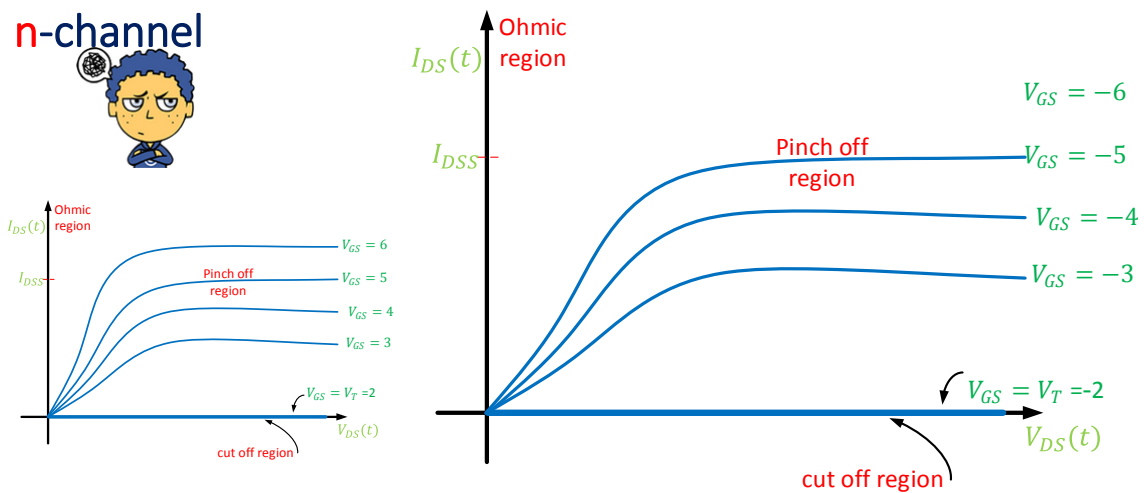


## Transfer characteristics for an n-channel EMOSFET

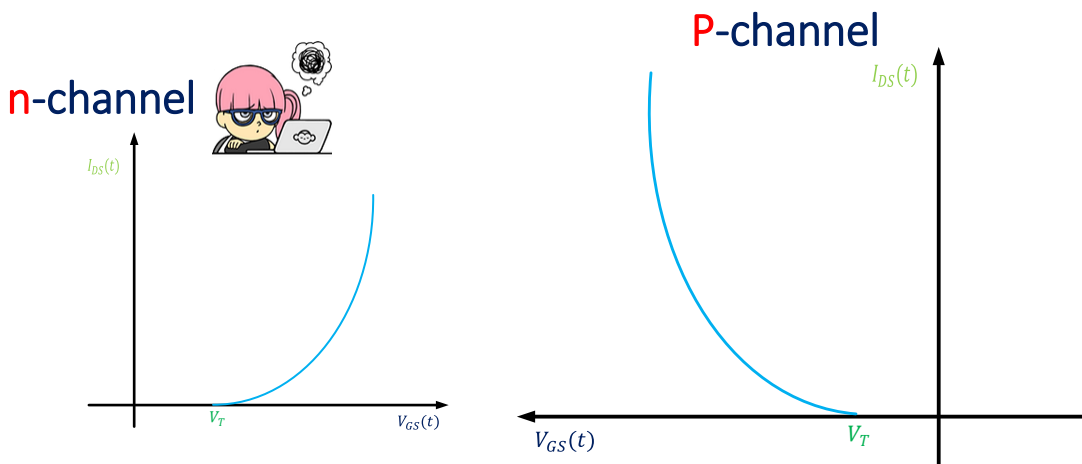


## Drain characteristics for an p-channel EMOSFET

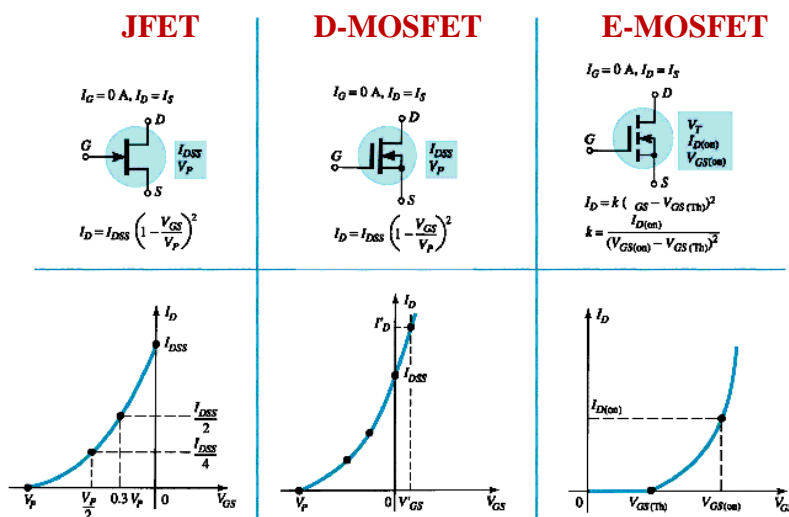
n-channel



## Transfer characteristics for an p-channel EMOSFET



### Summary Table



In the pinch off region

$$i_{DS}(t) = K_n (V_{GS}(t) - V_T)^2$$



$$|V_{DS}| > |V_{GS} - V_T|$$

$V_{GS} > V_T$  ; n- channel  
 $V_{GS} < V_T$  ; p- channel

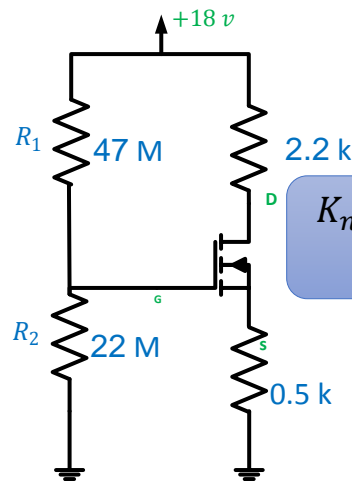
## Example



$$I_{DS} = K_n (V_{GS} - V_T)^2 \dots\dots\dots 1$$

$$V_{GS} = V_G - V_S$$

$$V_G = \frac{22M}{22M + 47M} (18) = 5.74v$$



$K_n = 0.25 \times 10^{-3} \text{ A/V}^2$   
 $V_T = 2 \text{ v}$

$$V_S = (0.5K) I_{DS}$$

$$V_{GS} = 5.74 - (0.5K) I_{DS} \dots \dots \dots 2$$

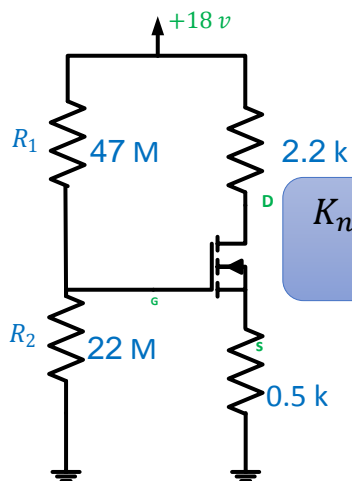
solving for  $V_{GS}$ :

$$V_{GS} = 4.78V \quad \checkmark$$

$$= -8.78V \quad \times$$

$$I_{DS} = 1.92m A$$

$$V_{DS} = 12.82 > |V_{GS} - V_T|$$



$$K_n = 0.25 \times 10^{-3} A/V^2$$

$$V_T = 2V$$