

Transmission Lines Parameters

T.L Resistance

T.L Inductance

T.L Capacitance

Transmission Line Capacitance :

» Capacitance of transmission line is the result of the potential difference between the conductors, it causes them to be charged in the same manner as the plates of a capacitor, when there is a potential difference between them the capacitance between conductors is the charge per unit of the potential difference.

1)) Electric Field and Voltage Calculation

2)) Transmission Line Capacitance for :-

A) Single-phase Line.

B) 3 ϕ Lines with equal spacing.

C) 3 ϕ Lines, bundled conductor, and unequal spacing.

1)) Gauss's Law \rightarrow Electric Field Strength (E)

Voltage between Conductors

Capacitance $C = Q/V$

Gauss's Law :- Total electric flux leaving a closed surface = Total charge within the volume enclosed by the closed surface.

\Downarrow Leads to

Normal Electric Flux density integrated over the closed surface = charge enclosed by this closed surface.

Surface integral over closed surface $\oiint D_{\perp} ds = \oiint \epsilon E_{\perp} ds = Q_{\text{enclosed}}$

Where,

$\epsilon \triangleq$ permittivity of the medium $= \epsilon_r \epsilon_0$

$\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$

$D_{\perp} \triangleq$ normal component of electric flux density.

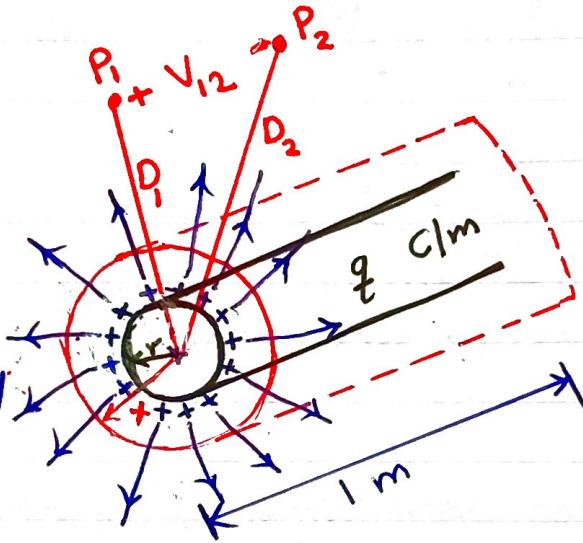
$E_{\perp} \triangleq$ normal component of electric field strength.

$ds =$ the differential surface area.

Note:-

Inside the perfect conductor, Ohm's Law give $E_{\text{int}} = 0$

That is, the internal electric field $E_{\text{int}} = 0$



$\oiint \epsilon E_{\perp} ds = Q_{\text{enclosed}}$
 $\epsilon E_x (2\pi x) (1) = q (1)$

1 m length

$E_x = \frac{q}{2\pi\epsilon x} \text{ V/m}$

$V_{12} = \int_{D_1}^{D_2} E_x dx = \int_{D_1}^{D_2} \frac{q}{2\pi\epsilon x} dx$

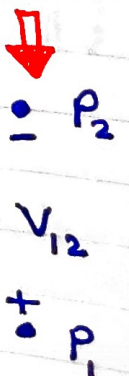
$V_{12} = \frac{q}{2\pi\epsilon} \ln \frac{D_2}{D_1} \text{ Volts}$

where,

$\epsilon = \epsilon_r \epsilon_0$

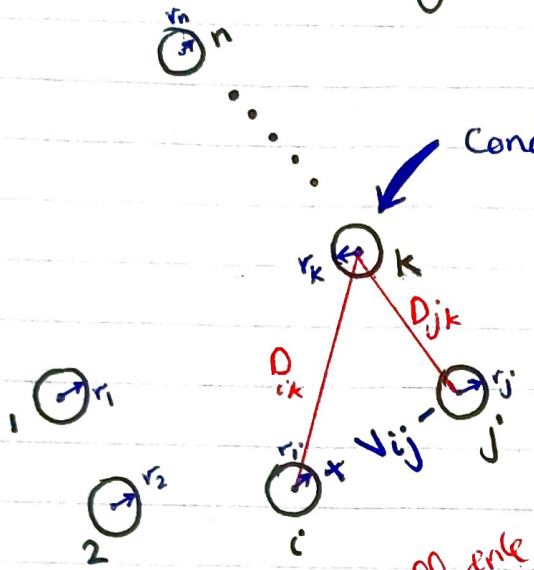
$\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$

note



$V_{12} = \frac{q}{2\pi\epsilon} \ln \frac{D_2}{D_1} \text{ Volts}$

Multi-Conductor System :



Conductor k has radius r_k and charge q_k (per meter length of the conductor)

$$V_{ijk} = \frac{q_k}{2\pi\epsilon} \ln \frac{D_{jk}}{D_{ik}} \text{ Volts}$$

$$V_{ij} = \sum_{k=1}^n \frac{q_k}{2\pi\epsilon} \ln \frac{D_{jk}}{D_{ik}} \text{ Volts}$$

Voltage difference due to charges in all conductors

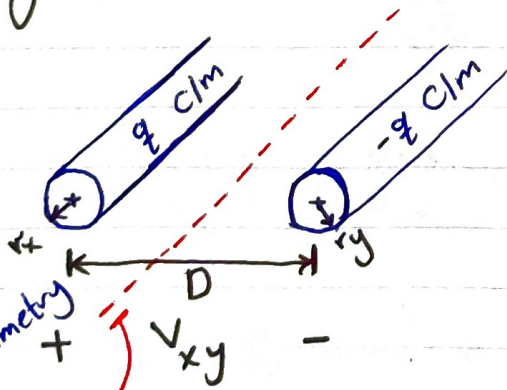
Super-position Theorem

Transmission Line Capacitance

Single-Phase Line [A]

Three-Phase Lines [B]

[A] Single-Phase Line



$$\begin{aligned} V_{xy} &= \frac{1}{2\pi\epsilon} \left[q \ln \frac{D_{yx}}{D_{xx}} - q \ln \frac{D_{yy}}{D_{xy}} \right] \\ &= \frac{q}{2\pi\epsilon} \ln \frac{D_{yx} D_{xx}}{D_{xx} D_{yy}} \\ &= \frac{q}{\pi\epsilon} \ln \frac{D}{\sqrt{r_x r_y}} \text{ Volts} \end{aligned}$$

$$C_{xy} = \frac{q}{V_{xy}} = \frac{\pi\epsilon}{\ln \left(\frac{D}{\sqrt{r_x r_y}} \right)} \text{ F/m}$$

ooo Notes ooo

$$\Rightarrow V_{12}(q_1) = \frac{q_1}{2\pi\epsilon} \ln \frac{D}{r}$$

$$\Rightarrow V_{12}(q_2) = \frac{q_2}{2\pi\epsilon} \ln \frac{r}{D}$$

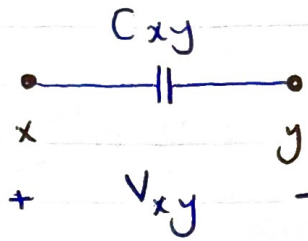
$$\Rightarrow V_{21}(q_2) = \frac{q_2}{2\pi\epsilon} \ln \frac{D}{r} = -V_{12}$$

$$\begin{aligned} \Rightarrow V_{12} &= V_{12}(q_1) + V_{12}(q_2) \\ q_2 &= -q_1 \end{aligned}$$

due to symmetry
→ zero-voltage
→ zero-potential
→ potential neutral

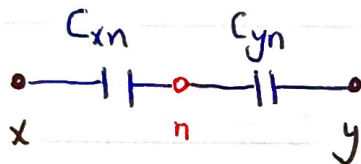
$$C_{xy} = \frac{\pi \epsilon}{\ln\left(\frac{D}{\sqrt{r_x r_y}}\right)} \quad \text{if } r_x = r_y$$

$$C_{xy} = \frac{\pi \epsilon}{\ln\left(\frac{D}{r}\right)}$$

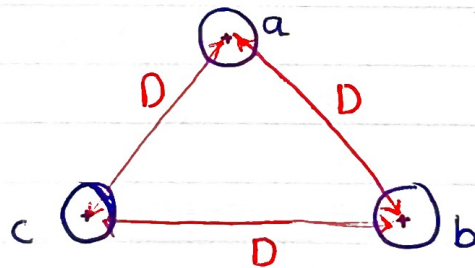


$$V_{xn} = V_{yn} = \frac{V_{xy}}{2}$$

$$C_n = C_{xn} = C_{yn} = \frac{q}{V_{xn}} = 2 C_{xy} = \frac{2 \pi \epsilon}{\ln\left(\frac{D}{r}\right)} \quad \text{F/m}$$



B Three-Phase Line with Equilateral Spacing:



$$q_a + q_b + q_c = 0$$

$$\Rightarrow V_{ab} = \frac{1}{2\pi\epsilon} \left[q_a \ln \frac{D_{ba}}{D_{aa}} + q_b \ln \frac{D_{bb}}{D_{ab}} + q_c \ln \frac{D_{bc}}{D_{ac}} \right]$$

$$= \frac{1}{2\pi\epsilon} \left[q_a \ln \frac{D}{r} + q_b \ln \frac{r}{D} + q_c \ln \frac{D}{D} \right]$$

$$= \frac{1}{2\pi\epsilon} \left[q_a \ln \frac{D}{r} + q_b \ln \frac{r}{D} \right] \quad \text{Volts}$$

$$\Rightarrow V_{ac} = \frac{1}{2\pi\epsilon} \left[q_a \ln \frac{D_{ca}}{D_{aa}} + q_b \ln \frac{D_{cb}}{D_{ab}} + q_c \ln \frac{D_{cc}}{D_{ac}} \right]$$

$$= \frac{1}{2\pi\epsilon} \left[q_a \ln \frac{D}{r} + q_b \ln \frac{D}{D} + q_c \ln \frac{r}{D} \right]$$

$$= \frac{1}{2\pi\epsilon} \left[q_a \ln \frac{D}{r} + q_c \ln \frac{r}{D} \right]$$

$$V_{q_b} + V_{q_c}$$

$$V_{ab} + V_{ac} = \left(\frac{1}{2\pi\epsilon} \right) \left[2q_a \ln \frac{D}{r} + \underbrace{(q_b + q_c)}_{-q_a} \ln \frac{r}{D} \right]$$

$$V_{an} = \frac{1}{3} (V_{ab} + V_{ac})$$

$$\downarrow = \frac{1}{3} \left(\frac{1}{2\pi\epsilon} \right) \left[2q_a \ln \frac{D}{r} + q_a \ln \frac{D}{r} \right]$$

$$= \frac{q_a}{2\pi\epsilon} \ln \frac{D}{r}$$

$$C_{an} = \frac{2\pi\epsilon}{\ln \frac{D}{r}} \quad \text{F/m} \quad \text{line to neutral}$$

Notes □

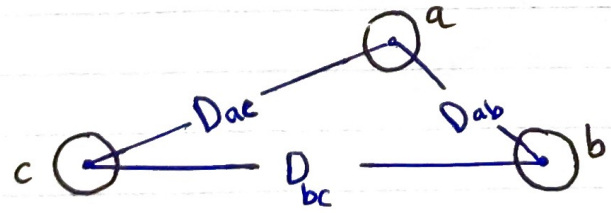
$$V_{ab} = \sqrt{3} V_{an} \angle +30^\circ = \sqrt{3} V_{an} \left[\frac{\sqrt{3}}{2} + j \frac{1}{2} \right]$$

$$V_{ac} = -V_{ca} = \sqrt{3} V_{an} \angle -30^\circ = \sqrt{3} V_{an} \left[\frac{\sqrt{3}}{2} - j \frac{1}{2} \right]$$

$$V_{ab} + V_{ac} = 3 V_{an}$$

$$\uparrow V_{an} = \frac{1}{3} (V_{ab} + V_{ac})$$

□ 3φ with asymmetrical Spacing



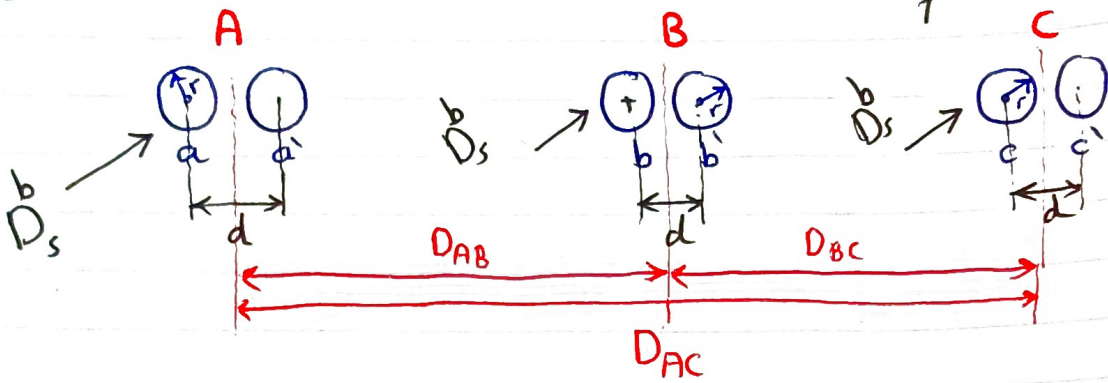
$$C_{an} = \frac{2\pi\epsilon}{\ln \left(\frac{D_{eq}}{r} \right)}, \quad D_{eq} = \sqrt[3]{D_{ab} D_{ac} D_{bc}}$$

(r) solid

(outside diameter)
2

stranded

□ 3φ Bundled Conductor with unequal spacing

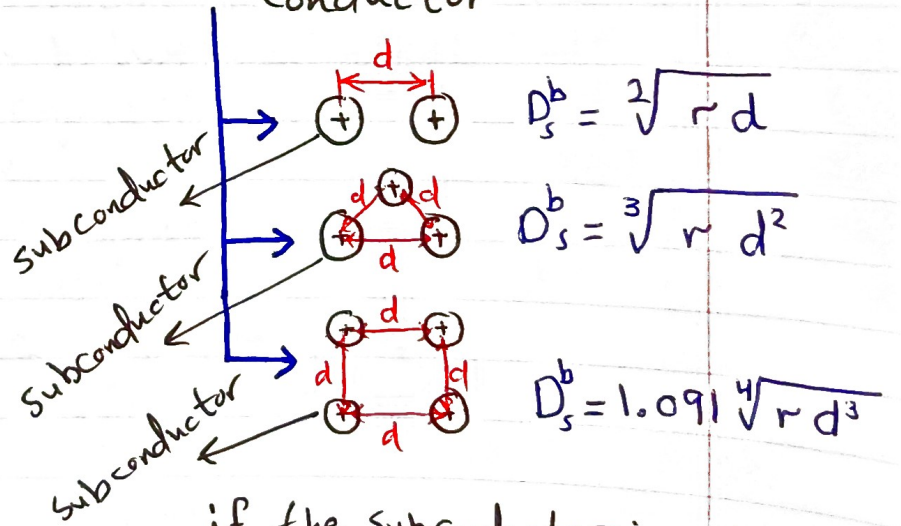


$$D_{AB} = GMD_{A,B} \quad , \quad D_{BC} = GMD_{B,C} \quad , \quad D_{AC} = GMD_{A,C}$$

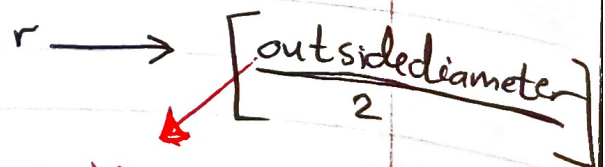
$$C_{an} = \frac{2\pi\epsilon}{\ln\left(\frac{D_{eq}}{D_s^b}\right)}$$

$$D_{eq} = \sqrt[3]{D_{AB} D_{BC} D_{AC}}$$

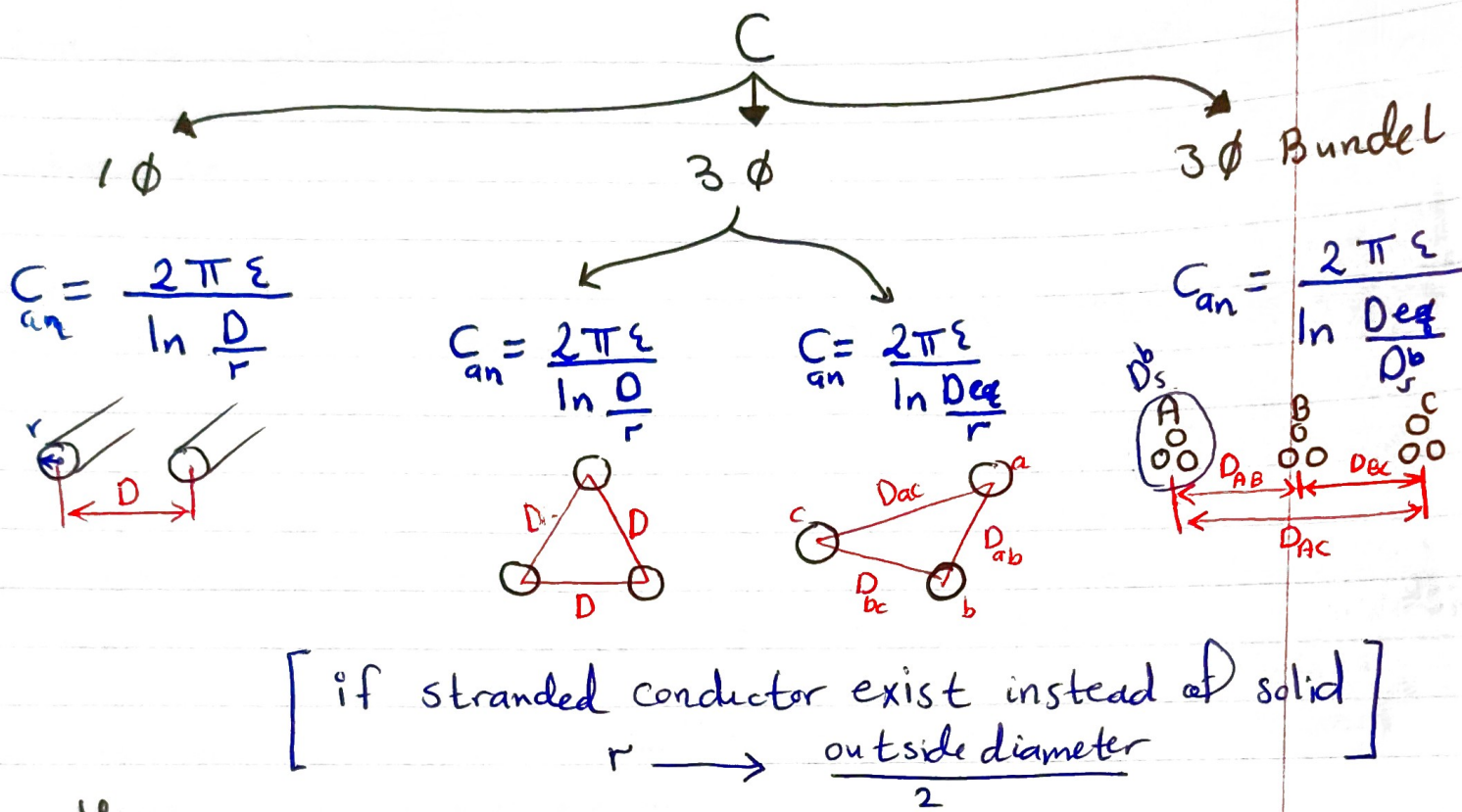
$D_s^b \triangleq$ GMR for the bundled conductor



if the subconductor is stranded



From manufacturer's data (Tables)

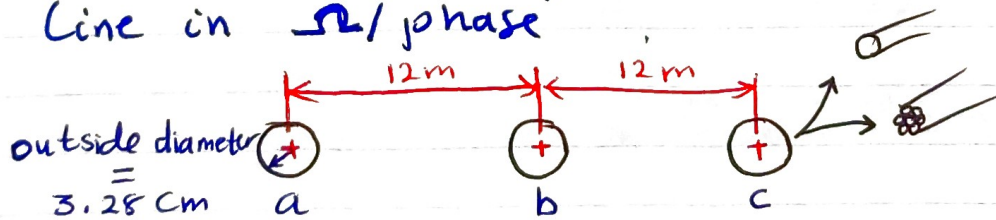


Example

A three-phase, 400 kV, 50 Hz, 350 km overhead T.L. has flat horizontal spacing with three identical conductors. The conductors have an outside diameter of 3.28 cm with 12 m between adjacent conductors.

- >> Determine the capacitive reactance - to - neutral in $\Omega/m/\text{phase}$
- >> Determine the capacitive reactance for the line in Ω/phase

Solution



$$D_{eq} = \sqrt[3]{D_{ab} D_{ac} D_{bc}} = \sqrt[3]{(12)(24)(12)} = 15.119 \text{ m}$$

$$C_{an} = \frac{2\pi\epsilon}{\ln\left(\frac{D_{eq}}{r}\right)} = 8.163 \times 10^6 \mu\text{F/m}$$

note: $Z_c = \frac{1}{j\omega C}$
 $Y_c = \omega C$

$$Y_n = 2\pi \times 50 \times C_n = 2.565 \times 10^9 \text{ } \Omega^{-1}/\text{m}/\text{phase}$$

Length = 350 km

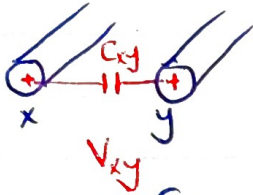
$$Y_n = 8.978 \times 10^4 \text{ } \Omega^{-1}/\text{phase}$$

$$\text{Reactance} = X_n = \frac{1}{Y_n} = 1.1138 \times 10^{-3} \Omega/\text{phase}$$

Line charging current:-

The current supplied to the transmission line capacitance is called charging current.

For a single-phase circuit operating at line-to-line voltage $V_{xy} = V_{xy} \angle 0^\circ$.



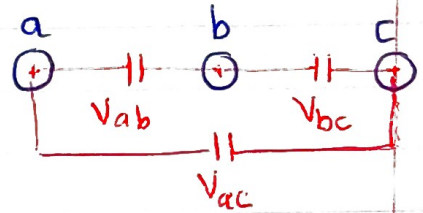
The charging current is

$$I_{chg} = Y_{xy} V_{xy} = j\omega C_{xy} V_{xy} \text{ Amp}$$

The capacitor delivers reactive power, the reactive power delivered by this line-to-line capacitance is

$$Q_c = \frac{V_{xy}^2}{X_c} = Y_{xy} V_{xy}^2 = \omega C_{xy} V_{xy}^2 \text{ var}$$

For a completely transposed 3 ϕ line that has $V_{an} = \frac{V_{LL}}{\sqrt{3}}$



The phase a charging current is

$$I_{chg} = Y_{an} V_{an} = j\omega C_{an} \frac{V_{LL}}{\sqrt{3}}$$

The reactive power delivered by phase a is

$$Q_{C1\phi} = Y_{an} V_{an}^2 = \omega C_{an} \frac{V_{LL}^2}{3}$$

The total reactive power supplied by the 3 ϕ line is

$$Q_{C3\phi} = 3Q_{C1\phi} = 3\omega C_{an} \frac{V_{LL}^2}{3} = \sqrt{3}\sqrt{3} \omega C_{an} V_{LL} \frac{V_{LL}}{\sqrt{3}}$$

$$Q_{C3\phi} = \omega C_{an} V_{LL}^2 \text{ var}$$