



Faculty of Engineering and Technology

Department of Mechanical and Mechatronics Engineering

Refrigeration and Air Conditioning

ENME 432

Cooling load calculations

Prepared by:

Sanad Abu Shama: 1150701

Suhaib Abu Raidah: 1150004

Ahmad Al- Jundi:1150665

Instructor: Dr. Adel Dweik

Indoor Conditions: 24 C, 50% RH and $\omega_{in} = 0.009 \text{ kg/kg}$

Outdoor Conditions: 35 C, 40% RH and $\omega_{out} = 0.014 \text{ kg/kg}$

Supply Temperature: 13 C.

For the supermarket:

1) Transmission with solarload:

▪ **Northern side:**

$$q_{wall} = U_{wall} * A_{wall} * CLTD$$

$$A_{wall} = \text{hieght} * \sum \text{wall lengths} = 4 * 31.24 = 125 \text{ m}^2$$

$$R_{wall} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{wall} = \frac{1}{\sum R_{wall}} = 0.49 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{wall} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$CLTD = 12$$

$$q_{wall} = U_{wall} * A_{wall} * CLTD = 0.49 * 125 * 12 = \boxed{735\text{W}}$$

▪ **Western side:**

$$A_{wall} = \text{hieght} * \sum \text{wall lengths} = 4 * 31.1 = 124.5 \text{ m}^2$$

$$R_{wall} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{wall} = \frac{1}{\sum R_{wall}} = 0.49 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{wall} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$CLTD = 27$$

$$q_{wall} = U_{wall} * A_{wall} * CLTD = 0.49 * 124.5 * 27 = \boxed{1650\text{W}}$$

▪ **Southern side:**

$$A_{wall} = \text{hieght} * \sum \text{wall lengths} = 4 * 31.24 = 125 \text{ m}^2$$

$$R_{wall} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{wall} = \frac{1}{\sum R_{wall}} = 0.49 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{wall} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$CLTD = 19$$

$$q_{wall} = U_{wall} * A_{wall} * CLTD = 0.49 * 125 * 19 = \boxed{1164\text{W}}$$

▪ **Roof:**

$$q_{roof} = U_{roof} * A_{roof} * CLTD$$

$$A_{roof} = 31.24 * 31.1 = 972 \text{ m}^2$$

$$R_{roof} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{roof} = \frac{1}{\Sigma R_{roof}} = 0.49 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{roof} = T_o - T_i = 35 - 24 = 11\text{C.}$$

$$CLTD = 21$$

$$q_{roof} = U_{roof} * A_{roof} * CLTD = 0.49 * 972 * 21 = \boxed{10000 \text{ W}}$$

▪ **Floor:**

$$q_{floor} = U_{floor} * A_{floor} * \Delta T_{floor}$$

$$A_{floor} = 972 \text{ m}^2$$

$$R_{floor} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 1.33$$

$$U_{floor} = \frac{1}{\Sigma R_{floor}} = 0.75 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{floor} = T_o - T_i = 35 - 24 = 11\text{C.}$$

$$q_{floor} = U_{floor} * A_{floor} * \Delta T_{floor} = 0.75 * 972 * 11 = \boxed{8020 \text{ W}}$$

2) Ventilation load:

$$q_{ventilation} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega$$

$$(\#people) = A_s * (occupation) = 972 \text{ (m}^2) * 0.08 \text{ (people/ m}^2) = \underline{78 \text{ people.}}$$

$$\dot{V}_{vent} = (\text{air requierments/ person}) * (\#people) = 8 \text{ (liters/person)} * 78 = \underline{642 \text{ litres.}}$$

$$\Delta T = T_i - T_o = 35 - 24 = 11\text{C.}$$

$$\Delta \omega = \omega_i - \omega_o = 0.014 - 0.009 = 0.005.$$

$$q_{ventilation} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega = 1.23 * 642 * 11 + 3000 * 642 * 0.005 = \boxed{18316 \text{ W.}}$$

3) Infiltration load:

$$q_{infiltration} = 1.23 * \dot{V}_{infil} * \Delta T + 3000 * \dot{V}_{infil} * \Delta \omega$$

$$\dot{V}_{infil} = V * (\text{air changes per second}) = 972 * 4 * (0.5/3600) = \underline{540 \text{ litres.}}$$

$$\Delta T = T_i - T_o = 35 - 24 = 11 \text{C.}$$

$$\Delta \omega = \omega_i - \omega_o = 0.014 - 0.009 = 0.005.$$

$$q_{infiltration} = 1.23 * \dot{V}_{infil} * \Delta T + 3000 * \dot{V}_{infil} * \Delta \omega = 1.23 * 540 * 11 + 3000 * 540 * 0.005 = \underline{\underline{15406 \text{ W.}}}$$

4) Internal load:

- **Lights:**

$$q_{lights} = \text{lamp rating} * Fu * Fb * CLF$$

$$\text{lamp rating} = 25 \left(\frac{\text{watt}}{\text{m}^2} \right) * \text{area} = 25 \left(\frac{\text{watt}}{\text{m}^2} \right) * 972 \text{ m}^2 = 24300 \text{ W}$$

$$q_{lights} = \text{lamp rating} * Fu * Fb * CLF = 24300 * .97 * 1 * 1.2 = \underline{\underline{28285 \text{ W}}}$$

- **People:**

$$q_{s_{people}} = \text{sensible heat gain} * CLF * \# \text{ of people}$$

$$q_{l_{people}} = \text{latent heat gain} * CLF * (\# \text{ of people})$$

$$(\# \text{ people}) = A_s * (\text{occupation}) = 972 \text{ (m}^2) * 0.08 \text{ (people/ m}^2) = \underline{78 \text{ people.}}$$

$$q_{s_{people}} = \text{sensible heat gain} * CLF * \# \text{ of people} = 92.5 * 1 * 78 = \underline{7215 \text{ W.}}$$

$$q_{l_{people}} = \text{latent heat gain} * (\# \text{ of people}) = 92.5 * 78 = \underline{7215 \text{ W.}}$$

$$q_{people} = 7215 * 2 = \underline{\underline{14430 \text{ W}}}$$

▪ **Equipment:**

$$3 \text{ refrigerators, } 1000 \text{ watt each} = 3 * 1000 = \underline{\underline{3000 \text{ W.}}}$$

$$\begin{aligned} q_{TOTAL \text{ room load of the supermarket}} &= q_{Transmission} + q_{Internal} + q_{infiltration} \\ &= \underline{\underline{82690 \text{ W}}} \end{aligned}$$

$$q_{Sensible \text{ of the supermarket}} = \underline{\underline{67375 \text{ W}}}$$

🚦 **Main Duct #1 for the supermarket:**

$$SHR_1 = \frac{67375}{82690} = 0.814$$

$$h_{s1} = 33.5 \text{ Kj/Kg}$$

$$h_i = 47.5 \text{ Kj/Kg}$$

$$q_{Room \text{ of Supermarket}} = \dot{m}_{s1} \times (h_i - h_{s1})$$

$$\dot{m}_{s1} = \frac{q_{Room \text{ of the Supermarket}}}{(h_i - h_{s1})} = \frac{82.690 \text{ KW}}{(47.5 - 33.5)} = 5.9 \text{ Kg/s.}$$

$$v_{s1} = 0.82 \text{ m}^3/\text{Kg}$$

$$\dot{V}_{s1} = \dot{m}_{s1} \times v_{s1} = 5.9 \times 0.82 = 4.84 \text{ m}^3/\text{s} = 10255 \text{ CFM}$$

$$\dot{V}_{grill} = \frac{\dot{V}_{s1}}{9}$$

$$\dot{V}_{grill} = \frac{4.84}{9} = 0.538 \text{ m}^3/\text{s.}$$

$$\text{Throw}_{horizontal} = \frac{L}{2 * n}$$

$$n = 3$$

$$\text{Throw}_{\text{horizontal}} = \frac{31}{2 * 3} = 5.17\text{m}$$

$$\text{Throw}_{\text{vertical}} = \frac{L}{2 * n}$$

$$n = 3$$

$$\text{Throw}_{\text{vertical}} = \frac{31}{2 * 3} = 5.17\text{m}$$

$$\text{Longest run} = (31 - 5.17) + (2 * 10.34) + 5.17 = 51.68\text{m}$$

$$\text{Let } V_{\text{main}} = 10\text{m/s}$$

$$\dot{V}_{ab} = 4840 \text{ l/s}$$

$$\frac{\Delta p}{L} = 1.2$$

$$D_{ab} = 800 \text{ mm}$$

$$a = 550\text{mm}$$

$$b = 1000\text{mm}$$

$$\dot{V}_{bc} = 3227 \text{ l/s}$$

$$D_{bc} = 720 \text{ mm}$$

$$a = 550\text{mm}$$

$$b = 800\text{mm}$$

$$\dot{V}_{bc} = 1613 \text{ l/s}$$

$$D_{bc} = 500 \text{ mm}$$

$$a = 550\text{mm}$$

$$b = 550\text{mm}$$

$$B - 1 = C - 1 = D - 1 = 500\text{mm}$$

$$a = 550\text{mm}$$

$$b = 550\text{mm}$$

For the gym:

1) Transmission with solar load:

▪ **East walls:**

$$A_{East\ Walls} = (3 + 3.69 + 0.63 + 2.48 + +3.13 + 3.13 + +1.78) \times 4$$
$$= 71.36\ m^2.$$

U_{walls} was found based on the Table in Example 5-1 (Outside wall):

$$U_{walls} = 0.49\ W/m^2\ C.$$

$$q_{East\ walls} = U_{walls} \times A_{East\ Walls} \times (CLTD)$$

$CLTD_{max} = 21$ from Table (4-15) in the book.

$$q_{East\ walls} = 0.49 \times 71.36 \times 21 = \boxed{734.3\ W}$$

▪ **South walls:**

$$A_{South\ Walls} = (0.53 + 1.24 + 1.26 + 0.91 + 0.84 + 0.77) \times 4 = 22.2\ m^2$$

$CLTD_{max} = 19$ from Table (4-15).

$$q_{South\ walls} = 0.49 \times 22.2 \times 19 = \boxed{206.7\ W}$$

- **East windows:**

$$q_{glass\ total} = U_g \times A_g \times (T_{out} - T_{in}) + A_g \times (SHGF) \times (S.C) \times (CLF)$$

$$A_{East\ Windows} = (0.81 + 0.81 + 1.88 + 1.88 + 1.88) \times 4 = 29.04\ m^2.$$

$$U_g = 3.3\ W/m^2\ C\ \text{for double glass.}$$

$$SHGF = 700\ W/m^2\ \text{from Table (4-10).}$$

$$S.C. (Shading\ Coefficient) = 0.4\ \text{for reflective double glass. (Table 4-11).}$$

$$CLF = 0.8\ \text{at 8 a.m. facing East from Table (4-12).}$$

$$\begin{aligned} q_{East\ windows} &= 3.3 \times 29.04 \times (35 - 24) + 29.04 \times (700) \times (0.4) \times (0.8) \\ &= \boxed{7560\ W} \end{aligned}$$

- **South windows:**

$$A_{South\ Windows} = (4.14 + 3.57 + 3.19 + 3.42 + 2.47) \times 4 = 67.16\ m^2.$$

$$SHGF = 355\ W/m^2\ \text{from Table (4-10) for May, Aug.}$$

$$S.C=0.4\ \text{reflective double glass.}$$

$$CLF = 0.83\ \text{from Table (4-12) at 12 noon facing south.}$$

$$\begin{aligned} q_{South\ Wins.} &= 3.3 \times 67.16 \times (35 - 24) + 67.16 \times (355) \times (0.4) \times (0.83) \\ &= \boxed{10353\ W} \end{aligned}$$

- **Roof:**

$$q_{Roof} = U_{Roof} \times A_{Roof} \times (CLTD_{Roof})$$

$$U_{Roof} = 0.48\ W/m^2\ C.$$

$$A_{Roof} = 312\ m^2.$$

$$CLTD_{Roof} = 21\ \text{From Table (4-14) at 20 solar time with suspended ceiling.}$$

$$q_{Roof} = 0.48 \times 312 \times (21) = \boxed{3145\ W}$$

- **Floor:**

$$q_{Floor} = U_{Floor} \times A_{Floor} \times (T_{out} - T_{in})$$

$$U_{Floor} = 0.757 \text{ W/m}^2\text{C}$$

$$A_{Floor} = 312 \text{ m}^2$$

$$q_{Floor} = 0.757 \times 312 \times (35 - 24) = \boxed{2600 \text{ W}}$$

$$q_{Transmission \text{ of the gym}} = \boxed{24600 \text{ W}}$$

2) Internal Loads:

▪ People:

- **In the Arena:** 75 people.

$$q_{People} = (SHG \times CLF \times People) + (LHG \times People)$$

$$SHG = 35\% \times 300 = 105 \text{ W. From Table (4-7).}$$

$$LHG = 300 - 105 = 195 \text{ W.}$$

$$CLF = 0.64 \text{ from Table (4-9) for 12 hours in space and 2 hours after each entry.}$$

$$q_{People} = (105 \times 0.64 \times 75) + (195 \times 75) = \boxed{19665 \text{ W}}$$

- **In the reception:** 27 people.

$$SHG = 60\% \times 100 = 60 \text{ W}$$

$$LHG = 100 - 60 = 40 \text{ W from Table (4-7) for seated people.}$$

$$CLF = 0.55 \text{ for 12 hours in space and 1 hour after each entry. Table (4-9)}$$

$$q_{People} = (60 \times 0.55 \times 27) + (40 \times 27) = \boxed{1971 \text{ W}}$$

- **In the lockers room:** 9 people.

$$SHG = 50\% \times 150 = 75 \text{ W}$$

$$LHG = 150 - 75 = 75 \text{ W Table (4-7) for standing people.}$$

$$CLF = 0.55 \text{ Table (4-9).}$$

$$q_{People} = (75 \times 0.55 \times 9) + (75 \times 9) = \boxed{1046 \text{ W}}$$

▪ Lights:

$$q_{Lights} = Lamp \text{ Rating} \times F_u \times F_b \times CLF$$

$$Lamp \text{ Rating} = 25 \text{ W/m}^2 \times 312 = 7800 \text{ W}$$

$CLF = 0.97$ for 10 hour operation at fixture Y in Table (4-6).

$$q_{Lights} = 7800 \times 1 \times 1.2 \times 0.97 = \boxed{9080 \text{ W}}$$

- **Equipment:**

- **Two domestic refrigerators:**

$$q_{Sensible} = 2 \times 120 = 240 \text{ kcal/hr} = 279 \text{ W}$$

$$q_{Latent} = 2 \times 80 = 160 \text{ kcal/hr} = 186 \text{ W}$$

- **Electric Coffee Maker (25 L):**

$$q_{Sensible} = 1000 \text{ kcal/hr} = 1162 \text{ W.}$$

$$q_{Latent} = 1000 \text{ kcal/hr} = 1162 \text{ W.}$$

$$q_{Sensible \text{ total}} = 1162 + 279 = 1441 \text{ W.}$$

$$q_{Latent \text{ total}} = 1162 + 186 = 1348 \text{ W.}$$

$$q_{Total} = \boxed{2789 \text{ W}}$$

$$q_{\text{internal of the gym}} = \boxed{34550 \text{ W}}$$

3) Ventilation Load:

$$q_{Ventilation} = 1.23 \times \dot{V}_{vent.} \times (T_{out} - T_{in}) + [3000 \times \dot{V}_{vent.} \times (\omega_{out} - \omega_{in})]$$

- **Arena:**

$\dot{V}_{vent.} = 750 \text{ L/s}$. From previous heating calculations.

$$q_{Vent. \text{ Arena}} = 1.23 \times 750 \times (35 - 24) + [3000 \times 750 \times (0.014 - 0.009)]$$

$$= 10150 + 11250 = \boxed{21400 \text{ W}}$$

- **Reception:**

$$\dot{V}_{vent. \text{ Recep.}} = 216 \text{ L/s}$$

$$q_{Vent. Recep.} = 1.23 \times 216 \times (35 - 24) + [3000 \times 216 \times (0.014 - 0.009)]$$

$$= 2922 + 3240 = \boxed{6162 \text{ W}}$$

- **Lockers room:**

$$\dot{V}_{vent. Lockers} = 112.5 \text{ L/s.}$$

$$q_{Vent.} = 1.23 \times 112.5 \times (35 - 24) + [3000 \times 112.5 \times (0.014 - 0.009)]$$

$$= 1522 + 1687 = \boxed{3209 \text{ W}}$$

4) Infiltration Load:

- **Arena:**

$$\dot{V}_{infil} = 415 \text{ L/s}$$

$$q_{Infil.} = 1.23 \times 415 \times (35 - 24) + [3000 \times 415 \times (0.014 - 0.009)]$$

$$= 5615 + 6225 = \boxed{11840 \text{ W}}$$

- **Reception:**

$$\dot{V}_{infil} = 99 \text{ L/s}$$

$$q_{Infil.} = 1.23 \times 99 \times (35 - 24) + [3000 \times 99 \times (0.014 - 0.009)]$$

$$= 1339 + 1485 = \boxed{2824 \text{ W}}$$

- **Lockers room:**

$$\dot{V}_{infil} = 18 \text{ L/s}$$

$$q_{Infil.} = 1.23 \times 18 \times (35 - 24) + [3000 \times 18 \times (0.014 - 0.009)]$$

$$= 243 + 270 = \boxed{513 \text{ W}}$$

$$Q_{TOTAL \text{ room load of the gym}} = Q_{Transmission} + Q_{Internal} + Q_{infiltration}$$

$$= 24017 + 31276 + 513 + 2824 + 11840$$

$$= \boxed{74325 \text{ W}}$$

$$q_{\text{Sensible of the gym}} = \boxed{48620 \text{ W}}$$

For shop 1:

1) Transmission with solar load:

▪ **Northern windows:**

$$q_{\text{glass}} = U_{\text{glass}} * A_{\text{glass}} * \Delta T_{\text{glass}} + A_{\text{glass}} * (SHGF) * (S.C) * (CLF)$$

$$A_{\text{glass}} = \text{hieght} * \sum \text{glass lengths} = 4 * 1.3 = 5.2 \text{ m}^2$$

$$U_{\text{glass}} = 3.3$$

$$\Delta T_{\text{glass}} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$q_{\text{glass}} = U_{\text{glass}} * A_{\text{glass}} * \Delta T_{\text{glass}} + A_{\text{glass}} * (SHGF) * (S.C) * (CLF) \\ = 3.3 * 5.2 * 11 + 5.2 * 140 * .3 * .91 = \boxed{387 \text{ W}}$$

▪ **Northern walls:**

$$\text{➤ } q_{\text{wall}} = U_{\text{wall}} * A_{\text{wall}} * CLTD$$

$$A_{\text{wall}} = \text{hieght} * \sum \text{wall lengths} = 4 * 4.76 = 19 \text{ m}^2$$

$$R_{\text{wall}} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{\text{wall}} = \frac{1}{\sum R_{\text{wall}}} = 0.49 \text{ KW/m}^2 \cdot \text{K}$$

$$\Delta T_{\text{wall}} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$q_{\text{wall}} = U_{\text{wall}} * A_{\text{wall}} * CLTD = 0.49 * 19 * 12 = \boxed{112 \text{ W}}$$

▪ **Roof:**

$$q_{roof} = U_{roof} * A_{roof} * CLTD$$

$$A_{roof} = 27.3 \text{ m}^2$$

$$R_{roof} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{roof} = \frac{1}{\Sigma R_{roof}} = 0.49 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{roof} = T_o - T_i = 35 - 24 = 11\text{C}.$$

$$q_{roof} = U_{roof} * A_{roof} * CLTD = 0.49 * 27.3 * 21 = \boxed{281 \text{ W}}$$

▪ **Floor:**

$$q_{floor} = U_{floor} * A_{floor} * \Delta T_{floor}$$

$$A_{floor} = 27.3 \text{ m}^2$$

$$R_{floor} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 1.33$$

$$U_{floor} = \frac{1}{\Sigma R_{floor}} = 0.75 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{roof} = T_o - T_i = 35 - 24 = 11\text{C}.$$

$$q_{floor} = U_{floor} * A_{floor} * \Delta T_{floor} = 0.75 * 27.3 * 11 = \boxed{225 \text{ W}}$$

2) **Ventilation load:**

$$q_{ventilation} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega$$

$$\# \text{ people} = 15 \text{ people}$$

$$\dot{V}_{vent} = (\text{air requirements/person}) * (\# \text{ people}) = 5 \text{ (L/s)} * 6 = 30 \text{ L/s}$$

$$\Delta T = T_i - T_o = 35 - 24 = 11\text{C}.$$

$$\Delta \omega = \omega_i - \omega_o = 0.014 - 0.009 = 0.005.$$

$$q_{ventilation} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega = 1.23 * 30 * 11 + 3000 * 30 * 0.005 = \boxed{856 \text{ W}}$$

3) **Infiltration load:**

$$q_{infiltration} = 1.23 * \dot{V}_{infil} * \Delta T + 3000 * \dot{V}_{infil} * \Delta \omega$$

$$\dot{V}_{infil} = V * (\text{air changes per second}) = 27.3 * 4 * (1/3600) = 30.3 \text{ L/s}$$

$$\Delta T = T_i - T_o = 35 - 24 = 11 \text{ C.}$$

$$\Delta \omega = \omega_i - \omega_o = 0.014 - 0.009 = 0.005.$$

$$q_{infiltration} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega = 1.23 * 30.3 * 11 + 3000 * 30.3 * 0.005 = \boxed{865 \text{ W.}}$$

4) Internal load:

- **Lights:**

$$q_{lights} = \text{lamp rating} * Fu * Fb * CLF$$

$$\text{lamp rating} = 25 \left(\frac{\text{watt}}{\text{m}^2} \right) * \text{area} = 25 \left(\frac{\text{watt}}{\text{m}^2} \right) * 27.3 \text{ m}^2 = 683 \text{ W}$$

$$q_{lights} = \text{lamp rating} * Fu * Fb * CLF = 683 * .97 * 1 * 1.2 = \boxed{795 \text{ W}}$$

- **People:**

$$q_{s_{people}} = \text{sensible heat gain} * CLF * \# \text{ of people}$$

$$q_{l_{people}} = \text{latent heat gain} * CLF * (\# \text{ of people})$$

$$(\# \text{ people}) = \underline{6 \text{ people.}}$$

$$q_{s_{people}} = \text{sensible heat gain} * CLF * \# \text{ of people} = 92.5 * 1 * 6 = \underline{555 \text{ W.}}$$

$$q_{l_{people}} = \text{latent heat gain} * (\# \text{ of people}) = 92.5 * 6 = \underline{555 \text{ W.}}$$

$$q_{people} = 555 + 555 = \boxed{1110 \text{ W.}}$$

$$Q_{TOTAL \text{ of Shop 1}} = Q_{Transmission} + Q_{Internal} + Q_{infiltration}$$

$$= \boxed{3775 \text{ W}}$$

$$q_{\text{Sensible of Shop 1}} = \boxed{2765 \text{ W}}$$

For shop 2:

1) Transmission with solar load:

▪ **Northern windows:**

$$q_{\text{glass}} = U_{\text{glass}} * A_{\text{glass}} * \Delta T_{\text{glass}} + A_{\text{glass}} * (SHGF) * (S.C) * (CLF)$$

$$A_{\text{glass}} = \text{hieght} * \sum \text{glass lengths} = 4 * 1.3 = 5.2 \text{ m}^2$$

$$U_{\text{glass}} = 3.3$$

$$\Delta T_{\text{glass}} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$q_{\text{glass}} = U_{\text{glass}} * A_{\text{glass}} * \Delta T_{\text{glass}} + A_{\text{glass}} * (SHGF) * (S.C) * (CLF) \\ = 3.3 * 5.2 * 11 + 5.2 * 140 * 0.3 * 0.91 = \boxed{387 \text{ W}}$$

▪ **Northern walls:**

$$q_{\text{wall}} = U_{\text{wall}} * A_{\text{wall}} * CLTD$$

$$A_{\text{wall}} = \text{hieght} * \sum \text{wall lengths} = 4 * 4.76 = 19 \text{ m}^2$$

$$R_{\text{wall}} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{\text{wall}} = \frac{1}{\sum R_{\text{wall}}} = 0.49 \text{ KW/m}^2 \cdot \text{K}$$

$$\Delta T_{\text{wall}} = T_o - T_i = 35 - 24 = 11 \text{ C.}$$

$$q_{\text{wall}} = U_{\text{wall}} * A_{\text{wall}} * CLTD = 0.49 * 19 * 12 = \boxed{112 \text{ W}}$$

- **Roof:**

$$q_{roof} = U_{roof} * A_{roof} * CLTD$$

$$A_{roof} = 27.3 \text{ m}^2$$

$$R_{roof} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 2.0166$$

$$U_{roof} = \frac{1}{\Sigma R_{roof}} = 0.49 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{roof} = T_o - T_i = 35 - 24 = 11\text{C}.$$

$$q_{roof} = U_{roof} * A_{roof} * CLTD = 0.49 * 27.3 * 21 = \underline{\underline{281 \text{ W}}}$$

- **Floor:**

$$q_{floor} = U_{floor} * A_{floor} * \Delta T_{floor}$$

$$A_{floor} = 27.3 \text{ m}^2$$

$$R_{floor} = R_o + R_{st} + R_c + R_{in} + R_B + R_{plas} + R_i = 1.33$$

$$U_{floor} = \frac{1}{\Sigma R_{floor}} = 0.75 \text{ KW/m}^2.\text{K}$$

$$\Delta T_{roof} = T_o - T_i = 35 - 24 = 11\text{C}.$$

$$q_{floor} = U_{floor} * A_{floor} * \Delta T_{floor} = 0.75 * 27.3 * 11 = \underline{\underline{225 \text{ W}}}$$

2) Ventilation load:

$$q_{ventilation} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega$$

$$\# \text{ people} = 15 \text{ people}$$

$$\dot{V}_{vent} = (\text{air requirements/person}) * (\# \text{ people}) = 5 \text{ (L/s)} * 6 = 30 \text{ L/s}$$

$$\Delta T = T_i - T_o = 35 - 24 = 11\text{C}.$$

$$\Delta \omega = \omega_i - \omega_o = 0.014 - 0.009 = 0.005.$$

$$q_{ventilation} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta \omega = 1.23 * 30 * 11 + 3000 * 30 * 0.005 = \underline{\underline{856 \text{ W}}}$$

3) Infiltration load:

$$q_{infiltration} = 1.23 * \dot{V}_{infil} * \Delta T + 3000 * \dot{V}_{infil} * \Delta\omega$$

$$\dot{V}_{infil} = V * (\text{air changes per second}) = 27.3 * 4 * (1/3600) = 30.3 \text{ L/s}$$

$$\Delta T = T_i - T_o = 35 - 24 = 11 \text{ C.}$$

$$\Delta\omega = \omega_i - \omega_o = 0.014 - 0.009 = 0.005.$$

$$q_{infiltration} = 1.23 * \dot{V}_{vent} * \Delta T + 3000 * \dot{V}_{vent} * \Delta\omega = 1.23 * 30.3 * 11 + 3000 * 30.3 * 0.005 = \boxed{865 \text{ W.}}$$

4) Internal load:

▪ Lights:

$$q_{lights} = \text{lamp rating} * Fu * Fb * CLF$$

$$\text{lamp rating} = 25 \left(\frac{\text{watt}}{\text{m}^2} \right) * \text{area} = 25 \left(\frac{\text{watt}}{\text{m}^2} \right) * 27.3 \text{ m}^2 = 683 \text{ W}$$

$$q_{lights} = \text{lamp rating} * Fu * Fb * CLF = 683 * .97 * 1 * 1.2 = \boxed{795 \text{ W}}$$

▪ People:

$$q_{s_{people}} = \text{sensible heat gain} * CLF * \# \text{ of people}$$

$$q_{l_{people}} = \text{latent heat gain} * CLF * (\# \text{ of people})$$

$$(\# \text{ people}) = \underline{6 \text{ people.}}$$

$$q_{s_{people}} = \text{sensible heat gain} * CLF * \# \text{ of people} = 92.5 * 1 * 6 = \underline{555 \text{ W.}}$$

$$q_{l_{people}} = \text{latent heat gain} * CLF * (\# \text{ of people}) = 92.5 * 1 * 6 = \underline{555 \text{ W.}}$$

$$q_{people} = 555 + 555 = \boxed{1110 \text{ W.}}$$

$$q_{TOTAL \text{ of Shop 2}} = q_{Transmission} + q_{Internal} + q_{infiltration}$$

$$= \boxed{3775 \text{ W}}$$

$$q_{Sensible \text{ of Shop 2}} = \boxed{2765 \text{ W}}$$

$$q_{TOTAL \text{ of Gym+Shops}} = q_{Transmission} + q_{Internal} + q_{infiltration}$$

$$= \boxed{81875 \text{ W}}$$

$$q_{Sensible \text{ of Gym+Shops}} = 2765 + 2765 + 48620 = \boxed{54150 \text{ W}}$$

✚ **Main Duct # 2 (2 shops & gym):**

$$SHR_2 = \frac{54150}{81875} = 0.660$$

$$h_{S2} = 31 \text{ Kj/Kg}$$

$$h_i = 47.5 \text{ Kj/Kg}$$

$$q_{TOTAL \text{ of Gym+Shops}} = \dot{m}_{S2} \times (h_i - h_{S2})$$

$$\dot{m}_{S2} = \frac{q_{TOTAL \text{ of Gym+Shops}}}{(h_i - h_{S1})} = \frac{81.875 \text{ KW}}{(47.5 - 31)} = 4.96 \text{ Kg/s.}$$

$$v_{S2} = 0.82 \text{ m}^3/\text{Kg}$$

$$\dot{V}_{S2} = \dot{m}_{S2} \times v_{S2} = 4.96 \times 0.82 = 4.0 \text{ m}^3/\text{s} = 8622 \text{ CFM}$$

✚ **Flow rate for the shops:**

$$\dot{m}_S \text{ For each shop} = \frac{q_{TOTAL \text{ of Shop}}}{(h_i - h_{S1})} = \frac{3.775 \text{ KW}}{(47.5 - 31)} = 0.228 \text{ Kg/s}$$

$$\dot{V}_S \text{ For each shop} = \dot{m}_S \times v_{S2} = 0.228 \times 0.82 = 0.187 \text{ m}^3/\text{s} = 396 \text{ CFM}$$

✚ **Flow rate for the gym:**

$$\dot{m}_S \text{ For the Gym} = \dot{m}_{S2} - (2 \times \dot{m}_S \text{ For each shop}) = 4.5 \text{ Kg/s}$$

$$\dot{V}_S \text{ For the gym} = \dot{V}_{S2} - (2 \times \dot{V}_S \text{ For each shop}) = 4.0 - 2 \times 0.187 = 3.63 \text{ m}^3/\text{s}$$

$$= 8622 - 2 \times 396 = 7830 \text{ CFM}$$

$$\dot{V}_{grill} = \frac{\dot{V}_{S1}}{8}$$

$$\dot{V}_{grill} = \frac{4.0}{8} = 0.5 \text{ m}^3/\text{s}.$$

$$\text{Throw}_{\text{horizontal}} = \frac{L}{2 * n}$$

n=

$$\text{Throw}_{\text{horizontal}} =$$

$$\text{Throw}_{\text{vertical}} = \frac{L}{2 * n}$$

n=

$$\text{Throw}_{\text{vertical}} =$$

Longest run =

Let $V_{\text{main}} = 10 \text{ m/s}$

$$\dot{V}_{ab} = 4000 \text{ l/s}$$

$$\frac{\Delta p}{L} = 1.3$$

$$D_{ab} = 715 \text{ mm}$$

a =

b =

$$\dot{V}_{bc} = 3815 \text{ l/s}$$

$$D_{bc} = 690 \text{ mm}$$

a = mm

b = mm

$$\dot{V}_{cd} = 3625 \text{ l/s}$$

$$D_{cd} = 670 \text{ mm}$$

$$a = \text{mm}$$

$$b = \text{mm}$$

$$B - 1 = C - 1 = D - 1 = \text{mm}$$

$$a = \text{mm}$$

$$b = \text{mm}$$

For the cafeteria:

1) Skylight transmission with solar load:

$$A_{\text{Sky lights}} = 613.739 \text{ m}^2 \text{ From previous heating calculations.}$$

$$U_{\text{skylight}} = 3.3 \text{ W/m}^2\text{C}$$

$SHGF = 870 \text{ W/m}^2$ From Table (4-10) for horizontal glass (Skylight).

$S.C = 0.9$ For a regular sheet double glass (no internal shading) from Table (4-11).

$CLF = 0.85$ From Table (4-12) for horizontal glass at noon.

$$q_{\text{skylight}} = U_{\text{skylight}} * A_{\text{skylight}} * \Delta T_{\text{skylight}} + A_{\text{skylight}} * (SHGF) * (S.C) * (CLF)$$

$$\begin{aligned} q_{\text{skylight}} &= 3.3 * 613.739 * 11 + 613.739 * (870) * (0.2) * (0.85) \\ &= \boxed{113051 \text{ W}} \end{aligned}$$

2) Floor transmission:

$$q_{\text{floor}} = U_{\text{floor}} * A_{\text{floor}} * \Delta T_{\text{floor}}$$

$$\begin{aligned} A_{\text{floor}} &= 613.739 \text{ m}^2 \\ U_{\text{floor}} &= 0.757 \text{ W/m}^2\text{C}. \end{aligned}$$

$$q_{\text{floor}} = 0.757 * 613.739 * 11 = \boxed{5111 \text{ W}}$$

3) Ventilation load:

$$q_{\text{ventilation}} = 1.23 * \dot{V}_{\text{vent}} * \Delta T + 3000 * \dot{V}_{\text{vent}} * \Delta \omega$$

people = 15 people

$$\dot{V}_{\text{vent}} = (\text{air requirements/person}) * (\# \text{ people}) = 5 \text{ (L/s)} * 15 = 75 \text{ L/s}$$

$$q_{\text{ventilation}} = 1.23 * 75 * 11 + 3000 * 75 * 0.005 = \boxed{2140 \text{ W}}$$

4) Infiltration load:

$$q_{\text{infiltration}} = 1.23 * \dot{V}_{\text{infil}} * \Delta T + 3000 * \dot{V}_{\text{infil}} * \Delta \omega$$

$$\dot{V}_{\text{infil}} = V * (\text{air changes per second}) = 75.7 * 4 * (1/3600) = 84 \text{ L/s}$$

$$q_{\text{infiltration}} = 1.23 * 84 * 11 + 3000 * 84 * 0.005 = \boxed{2396 \text{ W}}$$

$$Q_{\text{TOTAL room load of the cafeteria}} = Q_{\text{Transmission}} + Q_{\text{Internal}} + Q_{\text{infiltration}}$$

$$= \boxed{120558 \text{ W}}$$

$$q_{\text{Sensible of cafeteria}} = \boxed{119298 \text{ W}}$$