Solution – Assignment 4:

Problem 1:

$${}_{3}^{0}T = \begin{bmatrix} C_{1}C_{23} & -C_{1}S_{23} & S_{1} & L_{1}C_{1} + L_{2}C_{1}C_{2} \\ S_{1}C_{23} & -S_{1}S_{23} & -C_{1} & L_{1}S_{1} + L_{2}S_{1}C_{2} \\ S_{23} & C_{23} & 0 & L_{2}S_{2} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

and:

$${}_{4}^{3}T = \begin{bmatrix} 1 & 0 & 0 & L_{3} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad {}_{4}^{0}T = {}_{3}^{0}T {}_{4}^{3}T$$

we could then find ${}^0J(\underline{\theta})$ quite easily by differentiating ${}^0P_{\rm YORG}$. Finally, ${}^4J(\underline{\theta})$ can be calculated as ${}^4_0R^0J(\underline{\theta})$. This might be tedious, so lets try "standard" velocity propagation as done in the text:

$${}^{1}W_{1} = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{1} \end{bmatrix} {}^{1}V_{1} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$${}^{2}W_{2} = {}^{2}_{1}R^{1}W_{1} + \begin{bmatrix} 0\\0\\\dot{\theta}_{2} \end{bmatrix} = \begin{bmatrix} C_{2} & 0 & S_{2}\\-S_{2} & 0 & C_{2}\\0 & -1 & 0 \end{bmatrix} \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0\\0\\\dot{\theta}_{2} \end{bmatrix}$$

$${}^{2}W_{2} = \begin{bmatrix} S_{2}\dot{\theta}_{1} \\ C_{2}\dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} {}^{2}V_{2} = {}^{2}_{1}R({}^{1}V_{1} + {}^{1}W_{1} \times {}^{1}P_{2})$$

$${}^{2}V_{2} = \begin{bmatrix} C_{2} & 0 & S_{2} \\ -S_{2} & 0 & C_{2} \\ 0 & -1 & 0 \end{bmatrix} \begin{pmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ L_{1}\dot{\theta}_{1} \\ 0 \end{bmatrix} \end{pmatrix} = \begin{bmatrix} 0 \\ 0 \\ -L_{1}\dot{\theta}_{1} \end{bmatrix}$$

$${}^{3}W_{3} = {}^{3}_{2}R^{2}W_{2} + \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{3} \end{bmatrix} = \begin{bmatrix} C_{3} & S_{3} & 0 \\ -S_{3} & C_{3} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} S_{2}\dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{3} \end{bmatrix}$$

$${}^{3}W_{3} = \begin{bmatrix} S_{23}\dot{\theta}_{1} \\ C_{23}\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix}^{3}V_{3} = {}^{3}_{2}R({}^{2}V_{2} + {}^{2}W_{2} \times {}^{2}P_{3})$$

$${}^{3}V_{3} = \begin{bmatrix} C_{3} & S_{3} & 0 \\ -S_{3} & C_{3} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{pmatrix} \begin{bmatrix} 0 \\ 0 \\ -L_{1}\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0 \\ L_{2}\dot{\theta}_{2} \\ -L_{2}C_{2}\dot{\theta}_{1} \end{bmatrix}$$

$${}^{3}V_{3} = \begin{bmatrix} S_{3}L_{2}\dot{\theta}_{2} \\ C_{3}L_{2}\dot{\theta}_{2} \\ -L_{1}\dot{\theta}_{1} - L_{2}C_{2}\dot{\theta}_{1} \end{bmatrix}^{4}W_{4} = {}^{3}W_{3}$$

$${}^{4}V_{4} = {}^{4}_{3}R({}^{3}V_{3} + {}^{3}W_{3} \times {}^{3}P_{y}) = {}^{3}V_{3} + {}^{3}W_{3} \times {}^{3}P_{4}$$

$$= \begin{bmatrix} S_{2}L_{2}\dot{\theta}_{2} \\ C_{3}L_{2}\dot{\theta}_{2} \\ -L_{1}\dot{\theta}_{1} - L_{2}C_{2}\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0 \\ L_{3}(\dot{\theta}_{2} + \dot{\theta}_{3}) \\ -L_{3}\dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix}$$

$$= \begin{bmatrix} S_{3}L_{2}\dot{\theta}_{2} \\ C_{3}L_{2}\dot{\theta}_{2} - L_{3}(\dot{\theta}_{2} + \dot{\theta}_{3}) \\ -L_{1}\dot{\theta}_{1} - L_{2}C_{2}\dot{\theta}_{1} - L_{3}C_{23}\dot{\theta}_{1} \end{bmatrix}$$

$$\therefore {}^{4}J(\underline{\theta}) = \begin{bmatrix} 0 & S_{3}L_{2} & 0 \\ 0 & C_{3}L_{2} + L_{3} & L_{3} \\ (-L_{1} - L_{2}C_{2} - L_{3}C_{23}) & 0 & 0 \end{bmatrix}$$

Problem 2:

The mapping which potentially can be singular is: $Y = J(\theta)\dot{\theta}$ for the "position domain", and $\underline{\tau} = J^T(\theta)F$ for the "force domain". Now since transposition has nothing to do with the rank of a (square) matrix, its clear that the singularities of $J(\underline{\theta})$ are the same as those of $J^T(\underline{\theta})$.

Problem 3:

$$\underline{\tau} = {}^{3}J^{T} {}^{3}\underline{F} \quad : {}^{3}\underline{F} = {}^{3}J^{-T}\underline{\tau}$$

$${}^{3}J = \begin{bmatrix} L_{1}S_{2} & 0 \\ L_{1}C_{2} + L_{2} & L_{2} \end{bmatrix}$$

$${}^{3}J^{T} = \begin{bmatrix} L_{1}S_{2} & L_{1}C_{2} + L_{2} \\ 0 & L_{2} \end{bmatrix}$$
so,
$${}^{3}J^{-T} = \frac{1}{L_{1}L_{2}S_{2}} \begin{bmatrix} L_{2} & -L_{1}C_{2} - L_{2} \\ 0 & L_{1}S_{2} \end{bmatrix}$$

Problem 4:

From (5.103):

$$B_{\nu} = \begin{bmatrix} B_{A}R & -B_{A}R^{A}PX \\ 0 & B_{A}R \end{bmatrix}^{A_{\nu}}$$

$$B_{A}R^{A}PX = \begin{bmatrix} 0.86 & 0.5 & 0 \\ -0.5 & 0.86 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & -5 & 0 \\ 5 & 0 & -10 \\ 0 & 10 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} 2.5 & -4.3 & -5.0 \\ 4.3 & 2.5 & -8.6 \\ 0 & 10 & 0 \end{bmatrix}$$

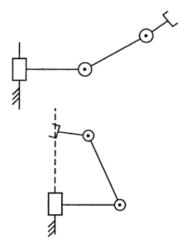
$$B_{\nu} = \begin{bmatrix} 0.86 & 0.5 & 0 & -2.5 & 4.3 & 5.0 \\ -0.5 & 0.86 & 0 & -4.3 & -2.5 & 8.6 \\ 0 & 0 & 1 & 0 & -10 & 0 \\ 0 & 0 & 0 & 0.86 & 0.5 & 0 \\ 0 & 0 & 0 & 0.86 & 0.5 & 0 \\ 0 & 0 & 0 & 0 & 0.86 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 2 \\ -3 \\ 1.41 \\ 1.41 \\ 0 \end{bmatrix}$$

$$^{B}\nu = [3.52 - 7.80 - 17.1 \ 1.91 \ 0.51 \ 0]^{T}$$

Problem 5:

"Workspace boundary" any angle set: $\{\theta_1, \theta_2, 0\}$

"Workspace interior" any angle set such that: $L_1 + L_2C_2 + L_3C_{23} = 0$ (θ_1 is arbitrary)



Problem 6:

$$\underline{\tau} = {}^{O}J^{T}(\underline{\theta}){}^{O}\underline{F}$$

$$\underline{\tau} = \begin{bmatrix} -L_1 S_1 - L_2 S_{12} & L_1 C_1 + L_2 C_{12} \\ -L_2 S_{12} & L_2 C_{12} \end{bmatrix} \begin{bmatrix} 10 \\ 0 \end{bmatrix}$$

$$\tau_1 = -10S_1L_1 - 10L_2S_{12}$$

$$\tau_2 = -10L_2S_{12}$$