

## Generators

- Permanent Magnet
- Separately Excited
- Shunt
- Series
- Compound

# DC Machines

## Motors

- Permanent Magnet
  - Separately Excited
  - Shunt
  - Series
  - Compound
- 
- The diagrams illustrate the electrical connections for different DC machine types. Each diagram shows a DC voltage source  $E_a$  (positive terminal on the left) and a series resistor  $R_s$  connected to the field winding  $R_A$ . The field current is denoted as  $I_f$ . The armature circuit is connected to a load resistor  $R_A$  and a terminal voltage  $V_t$  (positive terminal on the right). The armature current is denoted as  $I_a$ . In the 'Separately Excited' diagram, the field winding is connected to a separate DC source  $V_f$  through a rheostat  $R_{adj}$  and a resistor  $R_f$ . In the 'Compound' diagram, the field winding is connected in series with the armature circuit.

# Chapter 1 Formulas

$$f_m = \frac{\omega_m}{2\pi} \quad \omega_m = 60 f_m$$

$$H = \frac{Ni}{lc} \quad H: \text{intensity [A.N/m]}$$

$$B = \mu H \quad B: \text{density [T]}$$

$$\mu_r = \frac{\mu}{\mu_0} \quad \mu_0 = 4\pi \times 10^{-7} \text{ for Air}$$

$$\mu_r = 2000 - 6000 \text{ for Metal}$$

$$\Phi = \frac{\mu Ni}{lc} A = BA = \frac{F}{R} \quad [\text{weber}]$$

$$F = Ni \quad [\text{mmf}]$$

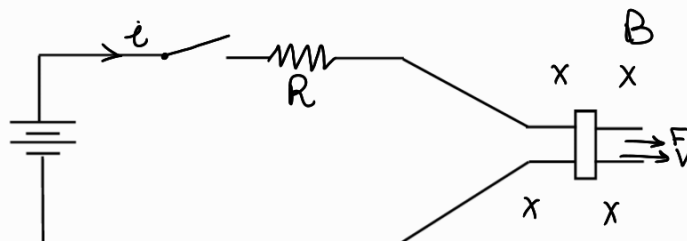
$$R = \frac{lc}{\mu A} \quad [\text{A.N/weber}]$$

Faraday's law:  $e_{ind} = -N \frac{d\Phi}{dt}$

## Linear DC Machine

$$i = \frac{V_B - e_{ind}}{R}$$

$$F = i (l \times B)$$



If a load is introduced

$$e_{ind} = V_B - iR \quad (\text{opposite Direction})$$

$$e_{ind} = V_B + iR \quad (\text{Same Direction})$$

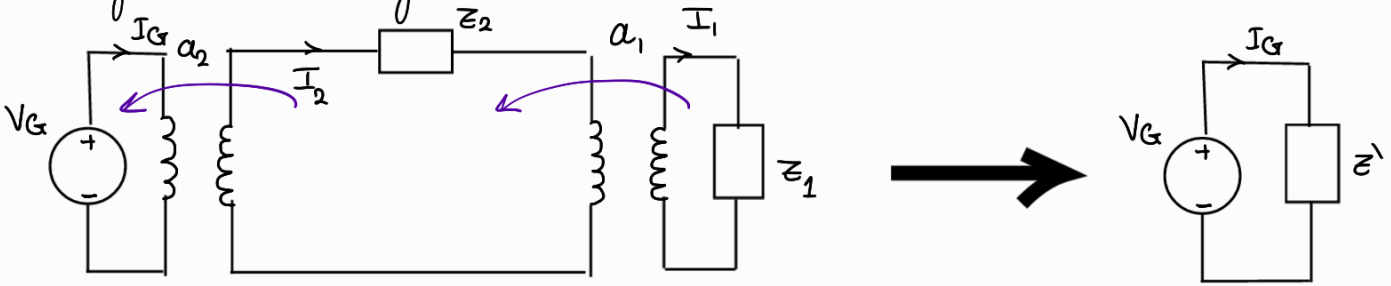
$$\text{where } i = \frac{F}{lB}$$

$$V_{\text{steady state}} = \frac{e_{ind}}{lB}$$

At no load  
 $e_{ind} = V_B$

# Chapter 2 Formulas (Transformers)

Reflection in general



Equations:

$$Z'_1 = a_1^2 Z_1$$

$$Z_{eq} = Z_2 + Z'_1 \rightarrow \text{Reflecting this}$$

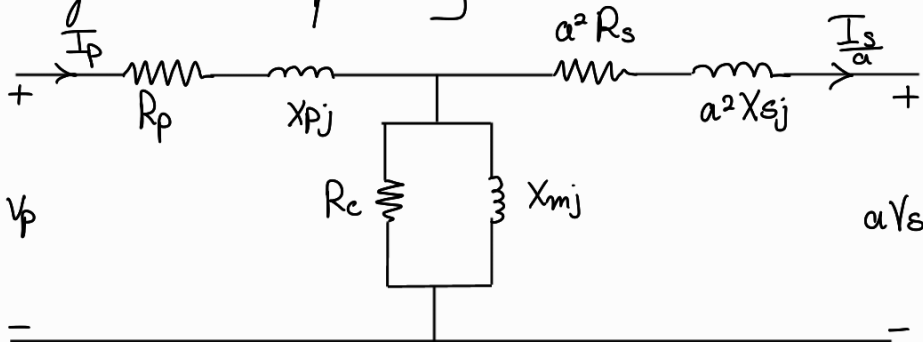
$$Z' = a_2^2 Z_{eq}$$

$$I_G = \frac{V_G}{Z'} \rightarrow \text{Reflecting this Back}$$

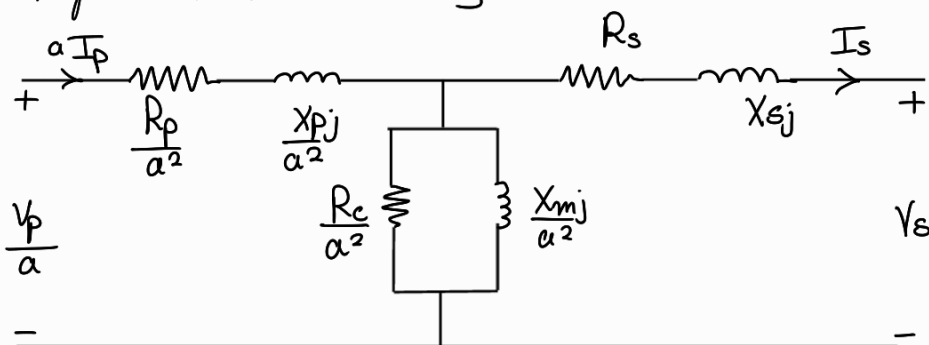
$$I_2 = \frac{1}{a_2} I_G, \quad I_1 = \frac{1}{a_1} I_2$$

## One transformer reflection

Referred to primary

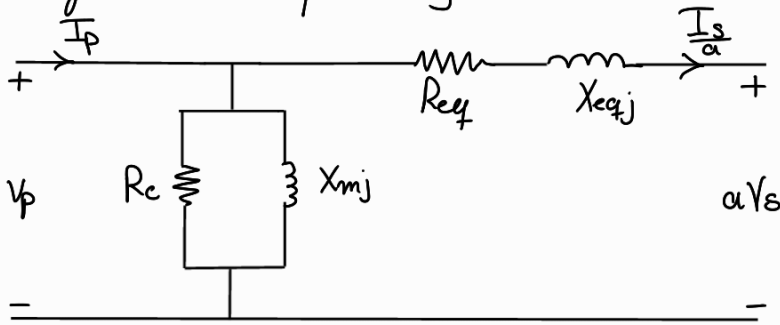


Referred to secondary



## Short of these circuits

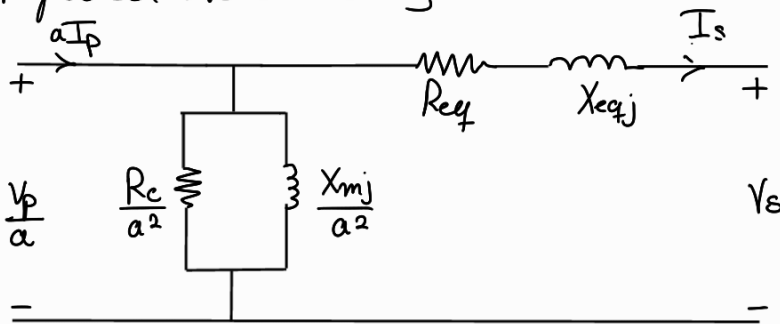
Referred to primary



$$R_{eq} = R_p + a^2 R_s$$

$$X_{eqj} = X_p + a^2 X_s$$

Referred to secondary



$$R_{eq} = \frac{R_p}{a^2} + R_s$$

$$X_{eqj} = \frac{X_p}{a^2} + X_s$$

## Open Circuit test

$$Y = \frac{1}{R_c} + \frac{1}{X_{mj}} = Y \angle -\theta$$

$$Y = \frac{I_{o.c}}{V_{o.c}}, \quad \theta = \cos^{-1} \frac{P_{o.c}}{V_{o.c} I_{o.c}}$$

↓  
Phases

## Short circuit test

$$Z = R_{eq} + X_{eqj} = \frac{V_{s.c}}{I_{s.c}} \angle \phi$$

$$\phi = \cos^{-1} \frac{P_{s.c}}{I_{s.c} V_{s.c}}$$

## Per unit system

$$\text{Quantity per unit} = \frac{\text{Actual value}}{\text{Base value of Quantity}}$$

$$P_{base} = Q_{base} = S_{base}$$

$$I_{base} = \frac{S_{base}}{V_{base}}$$

$$Z_{base} = R_{base} = X_{base} = \frac{V_{base}^2}{S_{base}} = \frac{(V_{base})^2}{S_{base}}$$

## Voltage Regulation

$$V_r = \frac{V_{s,nl} - V_{sfl}}{V_{sfl}} \times 100\%$$

$$V_{s,nl} = \frac{V_p}{a} = V_s + I_s (Z_{eq})$$

$$\left( \text{if rated} = \frac{S_{rated}}{V_{rated}} \right)$$

## Transformer efficiency

$$\eta = \frac{P_{out}}{P_{in}} \times 100\%$$

$$P_{out} = 3 PF = V_s I_s \cos \phi \quad \text{if Given} \quad = (I_s)^2 R_{eq} \quad \text{only } R \text{ from } Z_{eq}$$

$$P_{in} = P_{out} + P_{cu} + P_{core}$$

$$\frac{(V_p/a)^2}{(R_c/a^2)} = \frac{V_p}{R_c}$$

## $\Delta$ and $Y$ connection

$$\text{For } \Delta \rightarrow V_{\phi P} = V_L, \quad I_{\phi P} = \frac{I_L}{\sqrt{3}}, \quad S_{\phi P} = \frac{S}{3}$$

$$\text{For } Y \rightarrow V_{\phi P} = \frac{V_L}{\sqrt{3}}, \quad I_{\phi P} = I_L, \quad S_{\phi P} = \frac{S}{3}$$

Turns ratio  $a$

- $\Delta-\Delta, Y-Y \rightarrow a$
- $\Delta-Y \rightarrow \frac{V_{LP}}{V_{LS}} = \frac{V_{\phi P}}{\sqrt{3}V_{\phi S}} = \frac{1}{\sqrt{3}} a$
- $Y-\Delta \rightarrow \frac{V_{LP}}{V_{LS}} = \frac{\sqrt{3}V_{\phi P}}{V_{\phi S}} = \sqrt{3} a$

# Chapter 4 Formulas (Synchronous Generators)

$$n_{m} = \frac{120 f_e}{P} = n_{sync}$$

$$E_A = \sqrt{2} \pi N_c \Phi f = K \Phi \omega$$

↳ induced voltage

**Note**  
 $S = \sqrt{3} I_L V_L$   
 No cos $\phi$ , sin $\phi$  ↗

## General equation

$$E_A = V_\phi + I_A (R_A + X_s j)$$

## Power calculations

$$P_{in} = T_{app} \omega_m$$

$$P_{conv} = T_{ind} \omega_m$$

$\theta$ : Angle Between  $V_\phi$  &  $I_A$

$\delta$ : Angle between  $E_A$ ,  $V_\phi$

$$P_{out} = \sqrt{3} V_L I_L \cos \theta \text{ or } P_{out} = S \times PF \text{ for 3 phase}$$

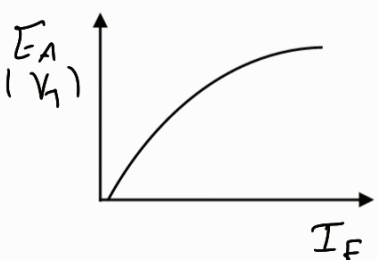
$$P_{copper \text{ losses}} = 3 R_A (I_A)^2$$

$$T_{ind} = \frac{3 V_\phi E_A \sin \delta}{X_s \omega_m} \text{ consider } R_A = 0$$

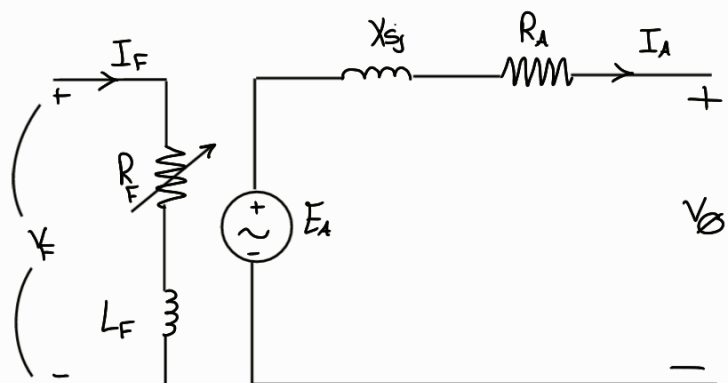
## Voltage Regulation

$$V_R = \frac{V_{no} - V_{fl}}{V_{fl}}$$

## OCC curve



$E_A$  is multiplied by  $\sqrt{3}$  if Y before using curve



# Chapter 5 Formulas (Synchronous Motors)

At coupling  $n_m = \frac{120 f_e}{P}$

General equation

$$V_\phi = E_A + I_A (R_A + X_s j)$$

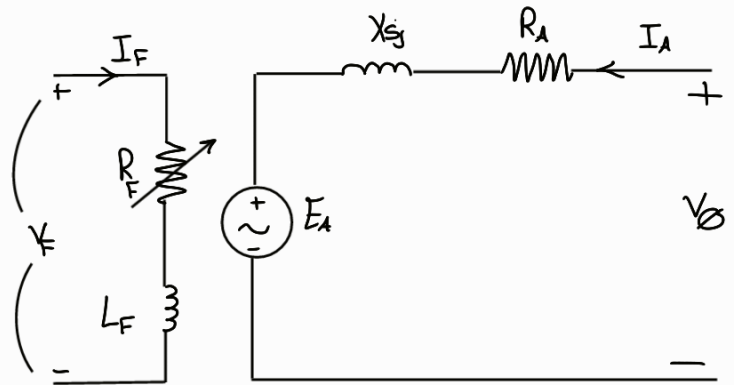
$$P = \frac{3 E_A V_\phi \sin \delta}{X_s} \quad \text{Assuming } R_A = 0$$

$$T_{\text{pull out}} = 3 T_{\text{rated}} \text{ (full load)}$$

$$E_A \sin \delta \propto P = \text{constant}$$

$$(E_A \sin \delta)_1 = (E_A \sin \delta)_2$$

$$P_{in} = \sqrt{3} V_L I_L \cos \theta$$



Static stability power limit

$$P_{\text{max}} = \frac{3 V_\phi E_A}{X_s}$$

$$P_{\text{conv}} = P_{IN} - P_{cu}$$

$$P_{\text{conv}} - P_{\text{out}} = P_{\text{mech}} + P_{\text{core}} + P_{\text{stray}}$$

Note

- If  $E_A$  is leading  $V_\phi$   
 $\delta > 0 \rightarrow$  Generator
- If  $E_A$  is lagging  $V_\phi$   
 $\delta < 0 \rightarrow$  Motor

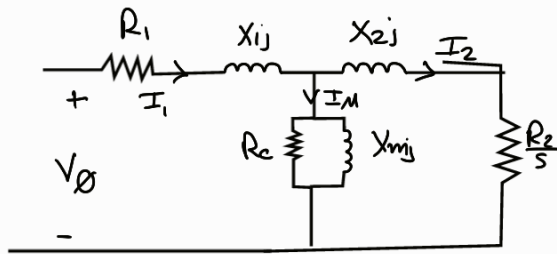
# Chapter 6 Formulas (Induction Motors)

$$n_{slip} = n_{sync} - n_m \quad \rightarrow n_m = \text{at full load}$$

$$n_{sync} = \frac{120 f_e}{P}$$

$$n_m = (1-s) n_{sync}$$

$$f_r = s f_e = \frac{P}{120} (n_{sync} - n_m)$$



Note

if load is increased  
in ratio X

$$s_{new} = X S$$

↳ This is used in Speed

$$Z_{eq} = R_1 + X_{ij} + \left( X_{2j} + \frac{R_2}{s} \parallel X_{mj} \right)$$

$$I_2 = a_{eff} I_1$$

## Power calculations

$$P_{in} = \sqrt{3} V_L I_L \text{ PF}$$

$$P_{scl} = 3 \underbrace{I_1^2 R_1}_{\text{Stator side}}$$

$$P_{RCL} = 3 I_2^2 R_2 = s P_{AG}$$

$$P_{AG} = P_{in} - P_{scl} - P_{core} = 3 I_2^2 \frac{R_2}{s}$$

$$P_{conv} = (1-s) P_{AG}$$

$$\tau_{ind} = \frac{P_{conv}}{\omega_{sync}}$$

$$\tau_{load} = \frac{P_{out}}{\omega_m}$$

$$P_{conv} = P_{in} - P_{scl} - P_{core} - P_{RCL} - P_{F\&W}$$

$$P_{out} = P_{conv} - P_{stray}$$

↳  $P_{mech}, P_{core}, P_{misc}$



$$P_{out} = P_{conv} - P_{mech} - P_{core} - P_{misc}$$

## Rotor power factor

$$G_R = \tan^{-1} \left( \frac{X_2}{R_2/s} \right)$$

Note

$$3I_A^2 R_F = 3I_2^2 \frac{R_2}{s}$$

↳ parallel of  $R_2 + X_{2j}$  and  $X_{mj}$

## Pullout torque

$$|V_{Th}| = \frac{V \phi X_m}{\sqrt{R_1^2 + (X_1 + X_m)^2}}$$

$$Z_{Th} = Z_{eq} = R_{Th} + jX_{Thj}$$

$$\text{Where } Z_{eq} = (R_1 + X_{1j}) \parallel (X_{mj}) = \frac{(R_1 + X_{1j}) X_{mj}}{(R_1 + X_{1j}) + X_{mj}}$$

$$S_{max} = \frac{R_2}{\sqrt{R_{Th}^2 + (X_{Th} + X_2)^2}}$$

$$T_{max} = \frac{3 V_{Th}^2}{2 \omega_{sync} \left[ R_{Th} + \sqrt{R_{Th}^2 + (X_{Th} + X_2)^2} \right]}$$

Note:

• Changing Frequency will change reactances and  $V_{rated}$

reducing  $f \rightarrow$  increases by factor  $f_{new}/f_{old} \rightarrow X_{new} = \frac{f_{new}}{f_{old}} X_{old}$

increasing  $f \rightarrow$  decreases by factor  $f_{new}/f_{old} \leftarrow$  same  $f_{old}$

$$V_{rated} = \frac{f_{new}}{f_{old}} V_{old}$$

# Chapter 8 Formulas (DC Machines)

At no load  $I_A = 0 \rightarrow E_A = V_T$

$$\frac{E_A}{E_{A0}} = \frac{n}{n_0} \rightarrow \text{Speed}$$

241

$$\frac{E_{A1}}{E_{A2}} = \frac{n_1}{n_2}$$

At full load  $\rightarrow I_A = I_L - I_F$   
rated

- ▶ If we have magnetization curve & only Speed of the curve
  - We find new  $I_f$
  - We use it to obtain  $E_A$  from curve  $\rightarrow$  This  $E_A$  is at curve speed
  - We use KVL to obtain  $E_A$  at  $I_f$  found  $\rightarrow$  This  $E_A$  is at the speed we want to find

- ▶ If we have magnetization curve, but rated speed is different from curve

- We find new  $I_f$  ( $I_A$ )
- We  $\sim$  at  $\sim$   $I_f \rightarrow E_{A1} \rightarrow$  new velocity
- We use old  $I_f$  to find  $E_{A1} \rightarrow$  old velocity

$$\frac{E_{A1}}{E_{A2}} = \frac{\phi_1}{\phi_2} \cdot \frac{n_1}{n_2}$$

$n_1 =$  rated But not from curve  
 The one we want to find

we use

$$\frac{E_{A10}}{E_{A20}} = \frac{\phi_1}{\phi_2} \left. \vphantom{\frac{E_{A10}}{E_{A20}}} \right\} \text{at curve speed}$$

$I_{f \text{ old}}$   $\leftarrow$   $I_{f \text{ new}}$

## Speed Regulation

$$SR = \frac{n_{m, n.l} - n_{m, fl}}{n_{m, fl}}$$

## Series DC motor

$$\omega = \frac{V_T}{\sqrt{I_{inl} K_C}} - \frac{R_A + R_S}{K_C}$$

## Shunt DC motor

$$\omega = \frac{V_T}{K\Phi} - \frac{R_A I_{inl}}{(K\Phi)^2}$$

## Converted Power

$$P_{conv} = E_A I_A = T_{inl} \omega_m$$

$$E_A = I_A X_s j + V_\phi$$

$$\frac{480}{\sqrt{3}} \angle \delta = \underline{60 \angle 53.3} + V_\phi \angle 0^\circ$$

$$V_\phi \cos \theta + V_\phi \sin \theta j$$

$$\underline{277 \cos \delta} + \underline{277 \sin \delta j} = \underline{60 \cos 53.3} + \underline{60 \sin 53.3 j} + \underline{V_\phi}$$

$$277 \cos \delta = 60 \cos 53.3 + V_\phi \rightarrow \text{eq (1)}$$

$$277 \sin \delta = 60 \sin 53.3$$

10