

Experiment 3

Extended Surface heat transfer

Apparatus

- Manual mode operated
- Long horizontal rod heated at one end with a heater
- Thermocouples are distributed at equal intervals (5 cm) which allow the surface temperature to be measured
- heat transfer is assumed to be one dimensional and heat loss at tip is ignored

Components of the system are:

1. heated rod
 - Solid brass
 - Coated with black paint \rightarrow Consistent emissivity close to 1
2. Heater
 - Electrical heater, inserted coaxially
 - Power supplied to heater can be changed ($P = VI$)
3. Thermocouple
 - K-type thermocouple

OBJECTIVE :

- Verify Fourier law of conduction.
- Measure conductivity of metals
- Measure temperature profile along a rod.
- Apply fin theory
- Calculate heat losses from fin rod
- Calculate efficiency of fin
- Apply basic extended surface heat transfer.

Calculations

$$\left. \begin{aligned} h_{\text{conv}} &= 1.32 \left(\frac{T_s - T_\infty}{D} \right)^{0.25} \quad \leftarrow \text{in K} \\ h_{\text{rad}} &= \epsilon \sigma \left(\frac{T_s^4 - T_\infty^4}{T_s - T_\infty} \right) \quad \leftarrow \text{Constant} \end{aligned} \right\} h_{\text{tot}} = h_{\text{rad}} + h_{\text{conv}}$$

Roel diameter

Electrical power supplied = $q = VI$

$$\text{Conduction heat transfer} = q_{\text{cond}} = KA_c \left(\frac{T_1 - T_2}{X} \right)$$

Cross sectional area
Distance Between T_1 and T_2

$$\text{Convection heat transfer} = q_{\text{conv}} = h_{\text{conv}} A_s (T_s - T_\infty)$$

Surface area = TDL

$$\text{Fin Constant} \longrightarrow m_{\text{th}} = \sqrt{\frac{h_{\text{tot}} P}{A_c K}} \quad \leftarrow \text{TTD}$$

$$\longrightarrow m_{\text{Exp}} = \left| \frac{\ln \left(\frac{T_x - T_\infty}{T_b - T_\infty} \right)}{X} \right|$$

Distance at which T_x is taken

$$\text{Fin efficiency} = \frac{q_{\text{fin}}}{q_{\text{max}}} = \frac{h A_f G_b}{h A_f G_b}$$

$$\begin{aligned} q_{\text{fin}} &\longrightarrow \sqrt{h P K A_c} G_b \tanh mL && \text{(Case B: insulated tip)} \\ &\longrightarrow \sqrt{h P K A_c} G_b && \text{(Case D: very long fin)} \end{aligned}$$

$$\eta_{fin} \longrightarrow \frac{\tanh mL}{mL}$$

$$\longrightarrow \frac{q_{fin}}{hA_f \theta_b} \quad \theta_b = T_b - T_\infty$$

TTDL

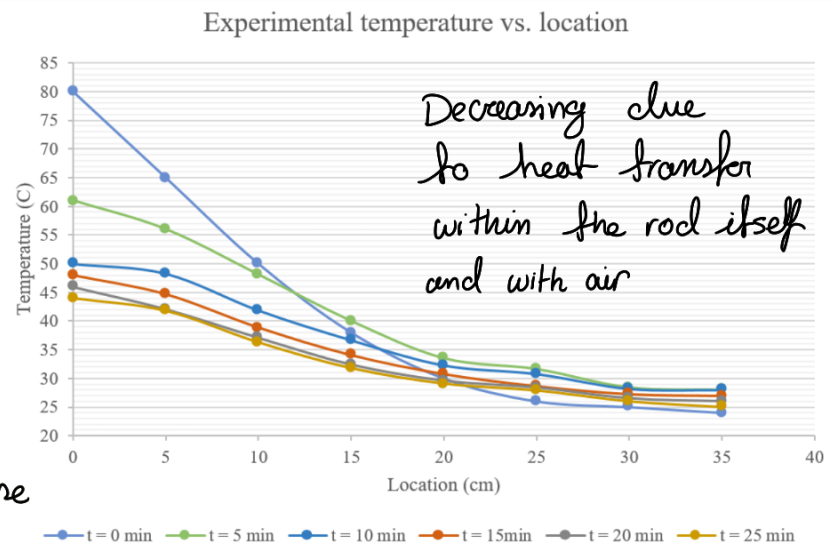
(Case B: insulated tip)
(Case D: very long fin)

Corrected length: $L_c = L + \frac{D}{4}$

Temperature distribution (case B): $\frac{T_x - T_\infty}{T_1 - T_\infty} = \frac{\cosh m(L_c - x)}{\cosh mL_c}$

Discussion of Results

- Average temperature of Rod \downarrow as $t \uparrow$
 \rightarrow That's because voltage provided by the heater is fixed and so power is fixed and so T_1 to decrease
 h_{conv}, h_{rad} to decrease



- Since $T_1 \downarrow \rightarrow$ heat dissipated $\downarrow \rightarrow$ Difference between T_1 & T_∞ decreases \rightarrow heat transfer decrease
- h_{conv} decreases with time since temp of rod is decreasing and so difference between it and air decrease
- Theoretical distribution has lower values than actual since fin provides less heat transfer than expected \rightarrow (Actual temp of the rod is higher and so heat dissipated is less)